

**ELG3175**  
**Introduction to Communication**  
**Systems**

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**Solutions**

**Assignment #6**

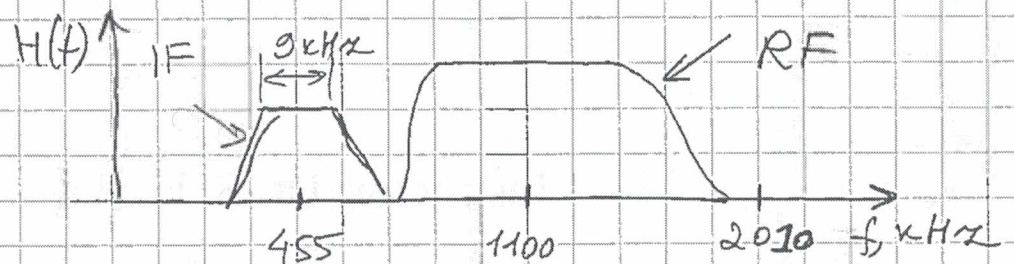
#1 Find  $f_{LO}$  first:

b+c)  $f_{LO} = f_c + f_{IF} = 1.1 \text{ MHz} + 455 \text{ kHz} = 1555 \text{ kHz}$

where  $f_c = 1.1 \text{ MHz}$  - AM signal carrier frequency.

Image frequency  $f_{im} = f_c + 2f_{IF} = 1.1 \text{ MHz} + 910 \text{ kHz} = 2010 \text{ kHz}$ .

IF filter bandwidth is  $\Delta f_{IF} = \Delta f_s = 9 \text{ kHz}$ .



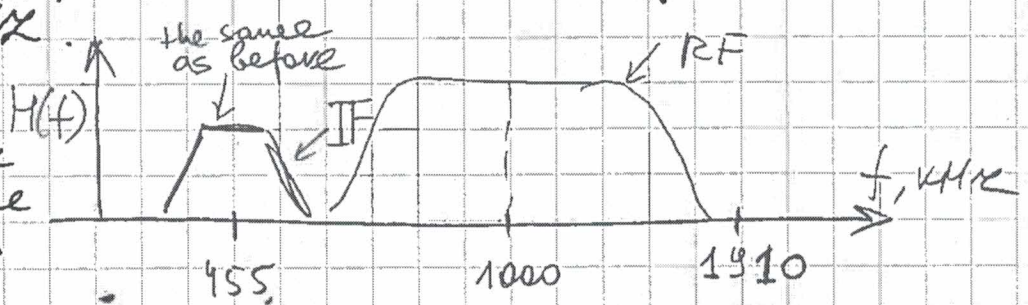
Normally, RF filter bandwidth is larger than IF one. However, RF filter must reject the image frequency that cannot be filtered out by the IF filter.

c)  $f_c = 1 \text{ MHz}$ ;  $f_{LO} = 1 \text{ MHz} + 455 \text{ kHz} = 1455 \text{ kHz}$

$f_{im} = f_c + 2f_{IF} = 1 \text{ MHz} + 910 \text{ kHz} = 1910 \text{ kHz}$

IF and RF filter bandwidth stay the same:

$\Delta f_{IF} = 9 \text{ kHz}$



RF filter response may stay the same or may shift to around 1 MHz.

IF filter response always stay the same.

#2

(a) The center frequency of BPF

$$f_{\text{BPF}} = \frac{f_c}{8} = \frac{103.7}{8} = 12.96 \text{ MHz}$$

Peak deviation

$$\Delta f_{\text{BPF}} = \frac{\Delta f}{8} = \frac{75}{8} = 9.375 \text{ kHz}$$

Bandwidth

$$\begin{aligned} \text{BW}_{\text{BPF}} &= 2(\Delta f_{\text{BPF}} + F_m) = 2(9.375 + 15) \\ &= 48.75 \text{ kHz} \end{aligned}$$

$$\begin{aligned} \text{(b)} \quad f_{\text{BPF}} &= f_c + f_{\text{os}} \rightarrow f_{\text{os}} = f_{\text{BPF}} - f_c = \\ &= 12.96 - 5 = 7.96 \text{ MHz} \end{aligned}$$

Another possibility:

$$f_{\text{BPF}} = f_{\text{os}} - f_c \rightarrow f_{\text{os}} = f_{\text{BPF}} + f_c = 17.96 \text{ MHz}$$

$$\text{(c)} \quad \Delta f_{\text{FM}} = \frac{\Delta f}{8} = \Delta f_{\text{BPF}} = 9.375 \text{ kHz}$$

where  $\Delta f = 75 \text{ kHz}$  peak deviation.

#3

DSB-SC modulated signal:

$$x(t) = A_c \cdot m(t) \cdot \cos \omega_c t$$

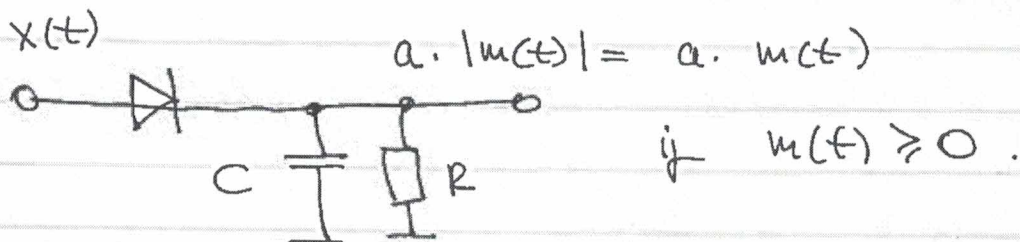
Its envelope  $E(t)$ :

$$E(t) = |A_c m(t)| = A_c |m(t)|$$

If  $m(t) \geq 0$  :  $|m(t)| = m(t)$

$$E(t) = A_c m(t) \sim m(t).$$

i.e. envelope detector can be used:



↑ simplest AM detector.

## FDM Broadcast of FM stations

# 4

FM mod. signal bandwidth (large  $\beta \gg 1$ ):

$$\Delta f \approx 2(F_{\max} + \Delta f) = 2(20 + 75) \text{ kHz} \\ = 190 \text{ kHz}$$

where  $F_{\max} = 20 \text{ kHz} = \text{max. message freq.}$   
 $\Delta f = 75 \text{ kHz} = \text{frequency deviation.}$

Total bandwidth per channel (incl. safety margin  $\delta f = 10 \text{ kHz}$ ):

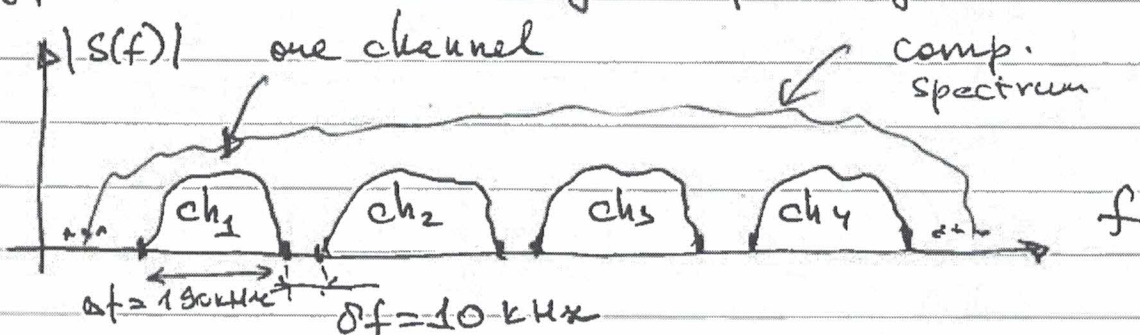
$$\Delta f' = \Delta f + \delta f = 200 \text{ kHz}$$

Number  $N$  of stations:

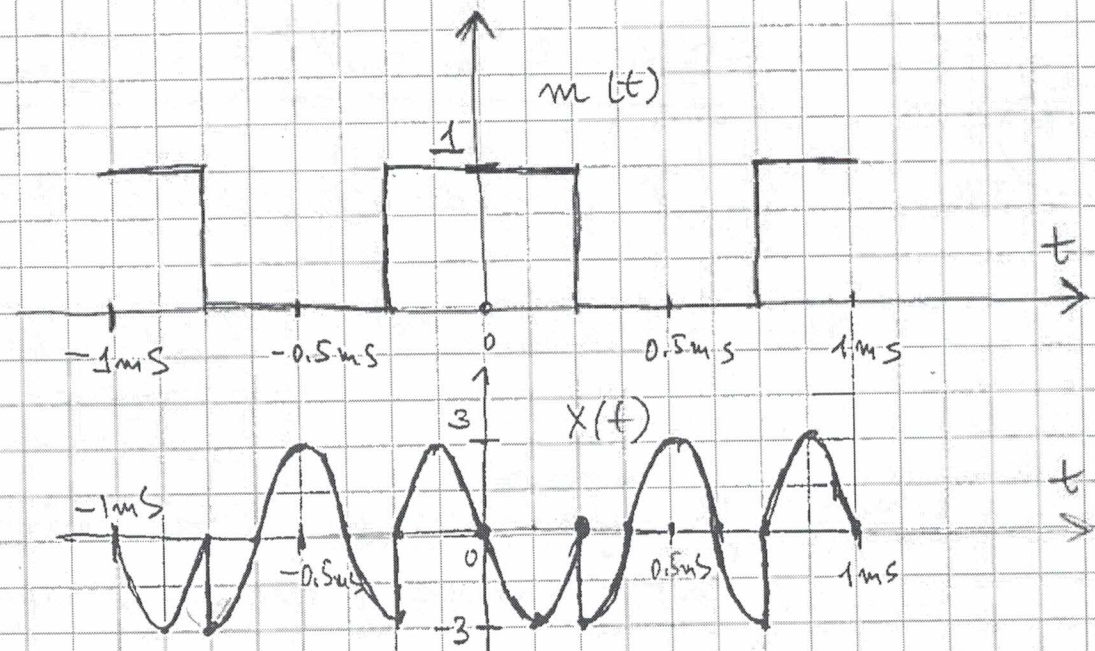
$$N = \frac{F_2 - F_1}{\Delta f'} = \frac{(110 - 80) \text{ MHz}}{200 \text{ kHz}} \\ = \frac{30 \text{ MHz}}{200 \text{ kHz}} = 150$$

where  $F_1 = 80 \text{ MHz}$ ,  $F_2 = 110 \text{ MHz}$ .

Typical spectrum of comp. signal:



#4



Since  $\beta_D = 1 \Rightarrow \Delta\varphi = \frac{\pi}{2} \cdot \beta_D = \frac{\pi}{2}$

when  $m(t) = 1$ ,  $x(t) = 3 \cos(\omega_c t + \frac{\pi}{2}) = -3 \sin \omega_c t$

when  $m(t) = 0$ ,  $x(t) = 3 \cos(\omega_c t)$ ,  $f_c = 2 \text{ kHz} \rightarrow T_c = 0.5 \text{ ms}$ .

To find the spectrum of  $x(t)$ , we present it as

$$x(t) = \frac{1}{2} (e^{j\omega_c t} e^{j\Delta\varphi m(t)} + e^{-j\omega_c t} e^{-j\Delta\varphi m(t)})$$

and find the spectrum of  $\varphi(t) = e^{j\Delta\varphi m(t)}$  first:

$$\varphi(t) = \sum_{n=-\infty}^{+\infty} C_n e^{jn\Omega t}, \text{ where } \Omega = \frac{2\pi}{T_m}, T_m = 1 \text{ ms}$$

$$C_n = \frac{1}{T_m} \int_{-T_m/4}^{T_m/4} \varphi(t) e^{-jn\Omega t} dt = \frac{1}{T_m} \int_{-T_m/4}^{T_m/4} e^{j\Delta\varphi} e^{-jn\Omega t} dt +$$

$$+ \frac{1}{T_m} \int_{T_m/4}^{3T_m/4} e^{-j\Delta\varphi} e^{-jn\Omega t} dt = \frac{1}{T_m} e^{j\Delta\varphi} \frac{e^{-jn\Omega t}}{-jn\Omega} \Big|_{-T_m/4}^{T_m/4} + \frac{1}{T_m} \frac{e^{-jn\Omega t}}{-jn\Omega} \Big|_{T_m/4}^{3T_m/4}$$

$$= \frac{\sin(\frac{\pi}{2}n)}{\pi n} [e^{j\pi/2} - 1] = \frac{1}{2} \text{sinc}(\frac{n}{2})(j-1);$$

#4 Using this result, we present  $x(t)$  as

$$x(t) = \frac{1}{2} \sum_{n=-\infty}^{+\infty} c_n e^{j(\omega_c + n\omega) t} + \frac{1}{2} \sum_{n=-\infty}^{+\infty} c_n^* e^{-j(\omega_c + n\omega) t}$$

Hence, FT of  $x(t)$  is

$$S_x(f) = \frac{1}{2} \sum_{n=-\infty}^{+\infty} c_n \delta(f - f_c - nF) + \frac{1}{2} \sum_{n=-\infty}^{+\infty} c_n^* \delta(f + f_c + nF).$$

where  $f_c = \omega_c/2\pi$ ,  $F = \omega/2\pi$ .

When  $f_c = 2 \text{ MHz} \gg F = 1 \text{ kHz}$ , positive and negative frequency parts of the spectrum (1st and 2nd terms correspondingly) do not overlap and the null-to-null bandwidth is determined by  $c_n$ :

$$c_n = 0 \Rightarrow \text{sinc}\left(\frac{n}{2}\right) = 0 \Rightarrow n = 2 \text{ (1st null)}.$$

Hence,  $\Delta f = 2 \cdot n \cdot F = 2 \cdot 2 \cdot 1 \text{ kHz} = 4 \text{ kHz}$ .

To compare with the random message case, find

$R$  first:  $R = 2F = 2 \text{ kHz}$ , hence

$\Delta f_{\text{random}} = 2R = 4 \text{ kHz} \rightarrow$  the same as for deterministic square-wave of the same period.

Hence, deterministic square-wave provides good approximation for a random message (sometimes!).