

Solution for Assignment on Design of Compression members

Problem 1:

A compression member has an L152x102x16 cross-section and a 300W material. The member span is 3,960mm and its effective length factors are $K_x = K_y = K_z = 1.0$. It is required to calculate the compressive resistance of the member.

Solution

(a) Properties

From the handbook, the relevant section properties are:

$$A = 3780\text{mm}^2$$

$$r'_x = 51.6\text{mm}, r'_y = 22.0\text{mm}, x_0 = 34.4\text{mm}, y_0 = 32.3\text{mm}, r_0 = 73.3\text{mm}$$

$$J = 319,000\text{mm}^4, C_w = 0.427 \times 10^9 \text{mm}^6$$

(b) Class 3 Check

For the long leg

$$\frac{b}{t} = \frac{152}{16} = 9.5 < \left(\frac{b}{t}\right)_{\text{lim}} = \frac{250}{\sqrt{F_y}} = \frac{250}{\sqrt{300}} = 14.4$$

Long leg meets Class 3 requirements

Since Class 3 requirements are met for the long leg, they must be met for the short leg

$$\frac{b}{t} = \frac{102}{16} = 6.4 < \left(\frac{b}{t}\right)_{\text{lim}} = \frac{250}{\sqrt{F_y}} = \frac{250}{\sqrt{300}} = 14.4$$

Thus, the section meets Class 3 requirements

(b) Check Slenderness

$$\left(\frac{K_x L}{r'_x}\right) = \frac{1 \times 3,960}{51.6} = 76.7 < 200$$

$$\left(\frac{K_y L}{r'_y}\right) = \frac{1 \times 3,960}{22.0} = 180 < 200$$

Slenderness requirements are met

(c) Buckling Stresses

$$F_{ex} = \frac{\pi^2 E}{\left(\frac{K_x L}{r_x}\right)^2} = \frac{\pi^2 (200,000)}{(76.7)^2} = 336 \text{MPa}$$

$$F_{ey} = \frac{\pi^2 E}{\left(\frac{K_y L}{r_y}\right)^2} = \frac{\pi^2 (200,000)}{(180)^2} = 60.9 \text{MPa}$$

$$F_{ez} = \left[\frac{\pi^2 EC_w}{(K_z L_z)^2} + GJ \right] \frac{1}{Ar_0^2}$$

$$\left[\frac{\pi^2 (200,000)(0.427 \times 10^9)}{(3,960)^2} + (77,000)(319,000) \right] \frac{1}{3,780 \times 73.3^2} = 1,212 \text{MPa}$$

Since the Section is asymmetric, the above stresses are not the buckling stresses.

The buckling stresses are obtained by solving the following cubic equation.

$$(F_e - F_{ex})(F_e - F_{ey})(F_e - F_{ez}) - F_e^2 (F_e - F_{ey}) \left(x_0/\bar{r}_0\right)^2 - F_e^2 (F_e - F_{ex}) \left(y_0/\bar{r}_0\right)^2 = 0$$

Substituting

$$(F_e - 336)(F_e - 60.9)(F_e - 1,212)$$

$$- F_e^2 (F_e - 60.9) \left(\frac{34.4}{73.3}\right)^2 - F_e^2 (F_e - 336) \left(\frac{32.3}{73.3}\right)^2 = 0$$

Solving (using the Solver or the Goal Seek utility, both in excel), obtain the three solution of the above cubic equations. The smallest root is the elastic buckling stress sought

$$F_e = 60.3 \text{MPa}$$

(d) Factored compressive resistance

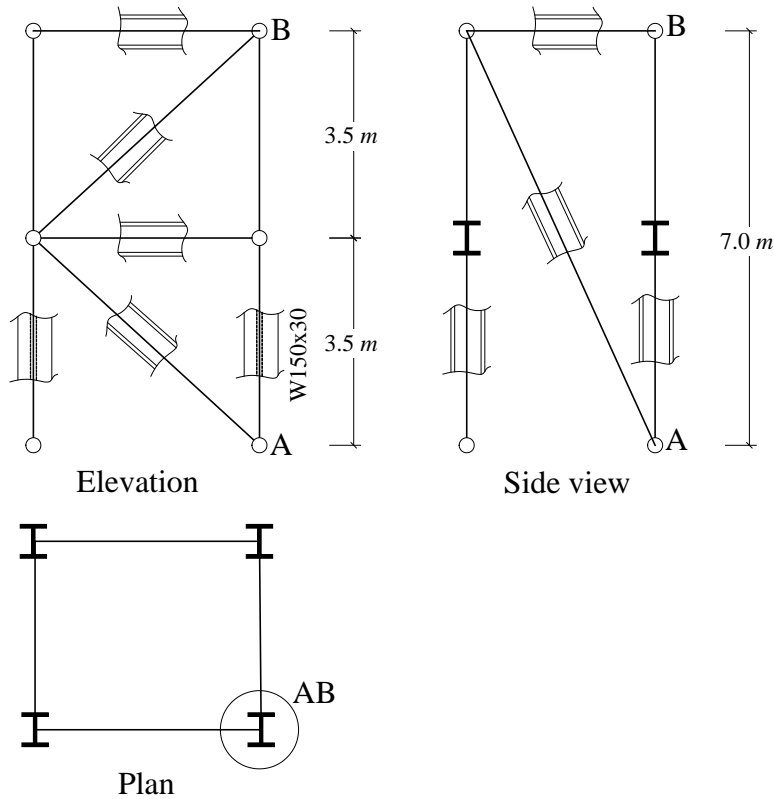
$$\lambda = \sqrt{\frac{F_y}{F_e}} = \sqrt{\frac{300}{60.3}} = 2.23$$

For most sections (including angles) $n=1.34$. Thus, the compressive resistance for the compression member is

$$C_r = \phi A F_y (1 + \lambda^{2n})^{-1/n} = 0.9 \times 3,780 \times 0.30 \times (1 + 2.23^{2 \times 1.34})^{-1/1.34} = 189 \text{kN}$$

Problem 2:

It is required to calculate the factored resistance for the shown vertical W150x30 member. Material is 350W. Perform all calculations and checks as required in CAN-CSA S16. For torsional buckling, the effective length can be taken as $K_z L = 3,500\text{mm}$

Solution:(a) Section Properties

From the Handbook, the relevant cross-section properties for a W150x30 are extracted:

$$r_x = 67.3 \text{ mm}$$

$$r_y = 38.3 \text{ mm}$$

$$A = 3,790 \text{ mm}^2$$

$$C_w = 30.3 \times 10^9 \text{ mm}^6$$

$$J = 100,000 \text{ mm}^4$$

$$I_x = 17.1 \times 10^6 \text{ mm}^4$$

$$I_y = 5.56 \times 10^6 \text{ mm}^4$$

(b) Class 3 Check

$$\text{Flange: } \frac{b}{t} = 8.22 < \left(\frac{b}{t}\right)_{\text{lim}} = \frac{200}{\sqrt{350}} = 10.7 \text{ Flange meets Class 3 requirements}$$

$$\text{Web: } \frac{b}{t} = 21.0 < \left(\frac{b}{t}\right)_{\text{lim}} = \frac{670}{\sqrt{350}} = 35.8 \text{ Web meets Class 3 requirements}$$

Section meets Class 3 requirements.

(c) Check Slenderness

From the figure, $K_x L = 7,000$, $K_y L = 3,500 \text{ mm}$

$$\frac{K_x L}{r_x} = 104 < 200$$

$$\frac{K_y L}{r_y} = 91.4 < 200 \quad \text{OK}$$

(d) Buckling Stresses

$$F_{ex} = \frac{\pi^2 E}{\left(\frac{K_x L}{r_x}\right)^2} = \frac{\pi^2 (200,000)}{(104)^2} = 182.5 \text{ MPa}$$

$$F_{ey} = \frac{\pi^2 E}{\left(\frac{K_y L}{r_y}\right)^2} = \frac{\pi^2 (200,000)}{(91.4)^2} = 236.3 \text{ MPa}$$

$$F_{ez} = \left[\frac{\pi^2 E C_w}{(K_z L_z)^2} + GJ \right] \frac{1}{I_x + I_y}$$

$$\left[\frac{\pi^2 (200,000)(30.3 \times 10^9)}{(3,500)^2} + (77,000)(100,000) \right] \frac{1}{(17.1 + 5.56) \times 10^6}$$

$$= \left[4.884 \times 10^9 + 7.7 \times 10^9 \right] \frac{1}{(17.1 + 5.56) \times 10^6} = \frac{12.58 \times 10^9}{(17.1 + 5.56) \times 10^6} = 555 \text{ MPa}$$

Since the column cross-section is doubly symmetric, the buckling stress is the smallest of F_{ex} , F_{ey} , F_{ez} , i.e.,

$$F_e = \min(F_{ex}, F_{ey}, F_{ez}) = 182.5 \text{ MPa}$$

(e) The factored compressive resistance for the column is

$$\lambda = \left(\frac{K_x L}{r_x} \right) \sqrt{\frac{F_y}{\pi^2 E}} = 104 \sqrt{\frac{350}{\pi^2 (200000)}} = 1.385$$

$$\text{or} \quad \lambda = \sqrt{\frac{350}{182.5}} = 1.385$$

For rolled wide flange sections $n=1.34$. Thus, the compressive resistance for the column is

$$\begin{aligned} C_r &= \phi A F_y (1 + \lambda^{2n})^{-1/n} = 0.9 \times 3,790 \times 0.350 \times (1 + 1.385^{2 \times 1.34})^{-1/1.34} \\ &= 1194 \times 0.4018 = 479 \text{ kN} \end{aligned}$$