

Term Test #2 - Fall 2018

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PROBLEM #1:

- a) From Table 10.3, for a major diameter of 1.25", the number of threads per inch is 5.
 Single thread \Rightarrow lead $L = p = \text{pitch} \Rightarrow L = p = \frac{1}{5} = 0.2'' \therefore$
 mean diameter $d_m = d - \frac{p}{2} = 1.25 - \frac{0.2}{2} = \underline{1.15''} \therefore$

b) $\tan A = \frac{L}{\pi d_m} = \frac{0.2}{1.15\pi} \Rightarrow A = 3.17^\circ$
 $\tan \alpha_n = \tan \alpha \times \tan A = \tan(4.5^\circ) \times \tan(3.17^\circ) \Rightarrow \alpha_n = 14.48^\circ$

Torque required to lift the load W :

$$T_{\text{lift}} = \frac{W d_m}{2} \frac{f \pi d_m + L \cos \alpha_n}{\pi d_m \cos \alpha_n - f L} + \frac{W f_c d_c}{2}$$

$$= \frac{1000 \times 1.15}{2} \frac{\pi \times 0.15 \times 1.15 + 0.2 \cos(14.48^\circ)}{\pi \times 1.15 \times \cos(14.48^\circ)} + \frac{1000 \times 0.15 \times 1.75}{2}$$

$$= \underline{253.2} \text{ lbf-in} \therefore$$

$$T_{\text{lower}} = \frac{W d_m}{2} \frac{f \pi d_m - L \cos \alpha_n}{\pi d_m \cos \alpha_n + f L} + \frac{W f_c d_c}{2} = \underline{188} \text{ lbf-in} \therefore$$

c) efficiency $e = \frac{W L}{2 \pi T_{\text{lift}}} = \frac{1000 \times 0.2}{2 \pi \times 253.2} = 0.125 = 12.5\%$

d) The screw is self-locked if: $f \geq \frac{L \cos \alpha_n}{\pi d_m} = \frac{0.2 \times \cos(14.48^\circ)}{\pi \times 1.15}$
 $= 0.0536$
 So it is self-locked as $f = 0.15 > 0.0536$

\therefore

PROBLEM #2:

Spring constant $k=200 \text{ N/cm}$; $F_{min} = 250 \text{ N}$; $F_{max} = 500 \text{ N}$

Excitation frequency $f = 1000 \text{ rpm}$, Spring index $C=8$

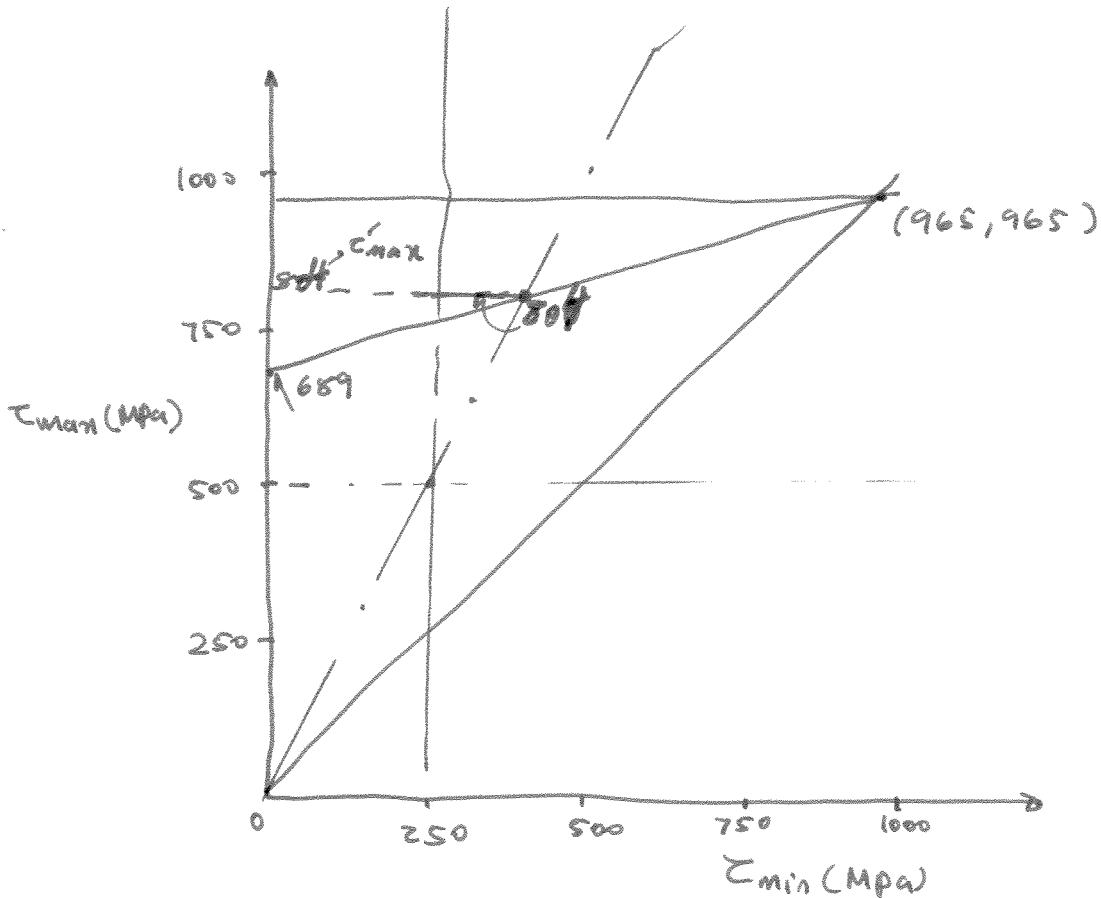
SF = 1.5 against fatigue , density $\rho = 7700 \text{ kg/m}^3$.

Shear modulus $G = 79000 \text{ MPa}$, HCS steel A232 , shot-peened
No pre-set

a) wire diameter?

$$\frac{\tau_{max}}{\tau_{min}} = \frac{F_{max}}{F_{min}} = \frac{500}{250} = 2 \quad , \quad SF = \frac{\tau'_{max}}{\tau_{max}} = \frac{804}{\tau_{max}} \Rightarrow \tau_{max} = \frac{804}{1.5} = 536 \text{ MPa}$$

A line of this slope is drawn on Figure below, giving an intersection of $\tau'_{max} = 804 \text{ MPa}$



$$k_w = \frac{4C-1}{4C-4} + \frac{0.615}{C}$$

$$C=8 \Rightarrow C k_w \approx 9.5$$

$$\tau_{max} = \frac{8 F_{max}}{\pi d^2} (k_w) = \frac{8 \times 500}{\pi d^2} \times 9.5 \quad , \quad \tau_{max} = 536 \Rightarrow d = \frac{8 \times 500 \times 9.5}{\pi (536)} \Rightarrow d \approx 4.75 \text{ mm}$$

b) mean diameter $\Delta = c d = 8 \times 4.75 = \underline{38 \text{ mm}}$ \therefore (3)

c) $k = \frac{dG}{8N_a C^3} \Rightarrow N_a = \frac{dG}{8k C^3} = \frac{4.75 \times 79000}{8 \times 20 \times 8^3} = \underline{4.5}$

Number of active coils N/mm

ends are squared & grounded $\Rightarrow N_t = N_a + 2 = 4.5 + 2 = \underline{6.5}$

total number of coils

(d) Free length $L_f = L_s + \frac{F_{shot}}{k} + \delta_{clash} = L_s + \delta_{shot}$

δ_{sw}

$\delta_{shot} = \frac{F_{shot}}{k}$ for 10% clash allowance $F_{shot} = 1.1 \times F_{max}$

$\Rightarrow F_{shot} = 1.1 \times 500 = 550 \text{ N}$, $\delta_{shot} = \frac{550}{20 \text{ N/mm}} = \underline{27.5 \text{ mm}}$

$L_s = N_t d = 6.5 \times 4.75 = \underline{30.875 \text{ mm}}$

$\Rightarrow L_f = 30.875 + 27.5 = \underline{58.375 \text{ mm}}$

e) No preset $\Rightarrow \tau_s \leq 0.45 S_{ut} = 0.45 \times 1523 = \underline{685.35 \text{ MPa}}$

$S_{ut} = A d^b = 1909.9 (4.75)^{-0.1453} = \underline{1523 \text{ MPa}}$ or from Fig. 12.7

$\tau_s = \frac{8F_s}{\pi d^2} C k_s$ $\Rightarrow C k_s = 8.5$, $c = 8$

$\Rightarrow \tau_s = \frac{8 \times 550}{\pi \times 4.75^2} \times 8.5 = \underline{527.63 \text{ MPa}}$

$\Rightarrow SF = \frac{685.35}{527.63} = \underline{1.3}$

$$f: \quad \frac{L_f}{D} = \frac{58.375}{38} \approx 1.536, \quad \frac{\delta_{SMI}}{L_f} = \frac{27.5}{58.375} \approx 0.468$$

From Fig 12.10 stable with respect to both end conditions
 No buckling will occur \therefore

$$g) \quad f_n = \frac{353000 d}{N_a D^2} = \frac{353000 \times 4.75}{4.5 \times 38^2} \approx 258 \text{ Hz}$$

$$\text{excitation } f = 1000 \text{ rpm} = \frac{1000}{60} \approx 16.7 \text{ Hz}$$

$$\frac{f_n}{f} = \frac{258}{16.7} = 15.4 > 13 \quad \text{OK}$$

No surging will occur