

1. For the translational mechanical system shown below where $x_3(t)$ and $x_4(t)$ are known displacements, sketch the free body diagram for **A**: M_1 **B**: M_2 and write the corresponding D'Alembert's law.

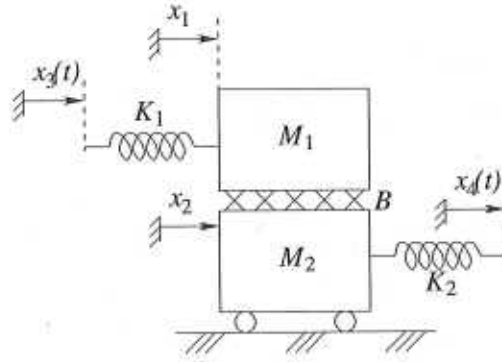


Figure 1: Translational mechanical system for question 1.

A:

$$M_1 \ddot{x}_1 + B \dot{x}_1 + K_1 x_1 - B \dot{x}_2 = K_1 x_3(t)$$

B:

$$M_2 \ddot{x}_2 + B \dot{x}_2 + K_2 x_2 - B \dot{x}_1 = K_2 x_4(t)$$

2. For the translational mechanical system shown below, sketch the free body diagram for **A**: M_1 **B**: M_2 and write the corresponding D'Alembert's law.

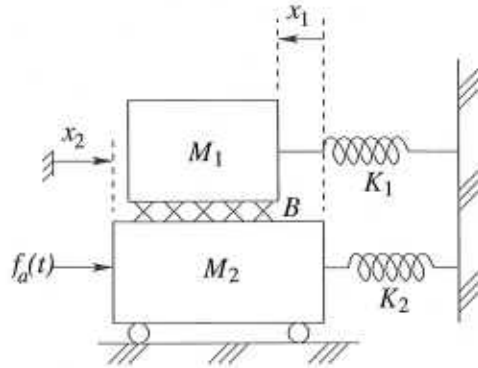
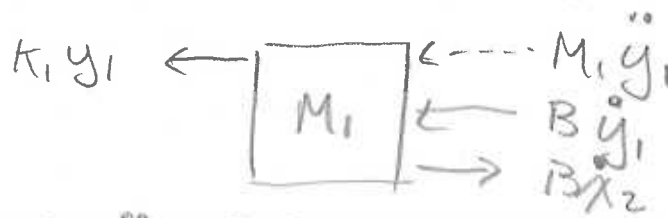


Figure 2: Translational mechanical system for question 2.

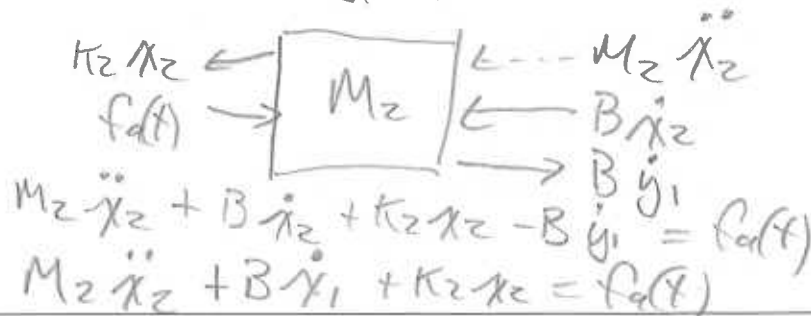
A: Define y_1 as absolute motion of m_1 +ve \rightarrow
 s.t. $y_1 = x_2 - x_1$



$$M_1 \ddot{y}_1 + B \dot{y}_1 + K_1 y_1 - B \ddot{x}_2 = 0$$

$$M_1 (\ddot{x}_2 - \ddot{x}_1) - B (\dot{x}_2 - \dot{x}_1) + K_1 (x_2 - x_1) = 0$$

B: Define y_1 as absolute motion of m_1 +ve \rightarrow
 s.t. $y_1 = x_2 - x_1$



$$M_2 \ddot{x}_2 + B \dot{x}_2 + K_2 x_2 - B \dot{y}_1 = f_d(t)$$

$$M_2 \ddot{x}_2 + B \dot{x}_1 + K_2 x_2 = f_d(t)$$

3. For the rotational mechanical system shown below, where $\tau_a(t)$ is a known torque, sketch the free body diagram for **A**: J_1 **B**: J_2 and write the corresponding D'Alembert's law.

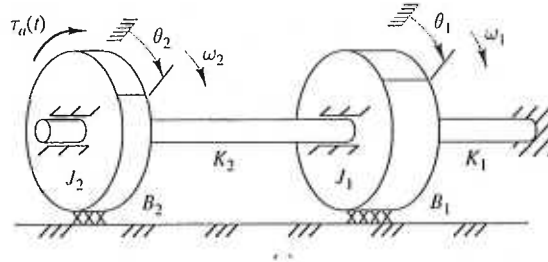
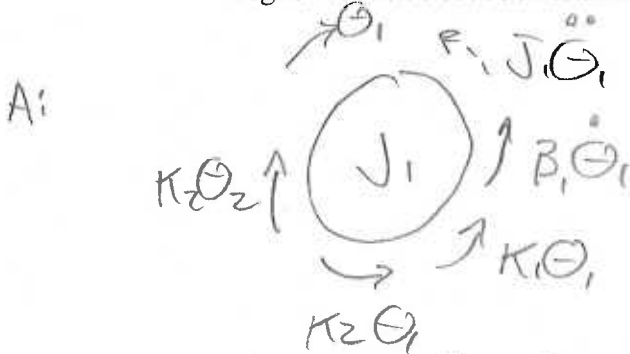
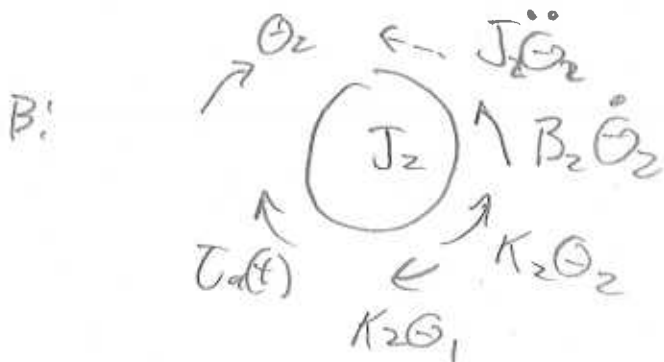


Figure 3: Rotational mechanical system for question 3.



$$J_1 \ddot{\theta}_1 + B_1 \dot{\theta}_1 + (K_1 + K_2) \theta_1 - K_2 \theta_2 = 0$$



$$J_2 \ddot{\theta}_2 + B_2 \dot{\theta}_2 + K_2 \theta_2 - K_2 \theta_1 = \tau_a(t)$$

4. For the mechanical system shown below, where $f_a(t)$ is a known force, sketch the free body diagram for **A: M_1** **B: M_2** and write the corresponding D'Alembert's law using only the variables x_1 , x_2 , and θ as indicated in the figure. Assume that the lever is ideal, i.e., no mass or friction.

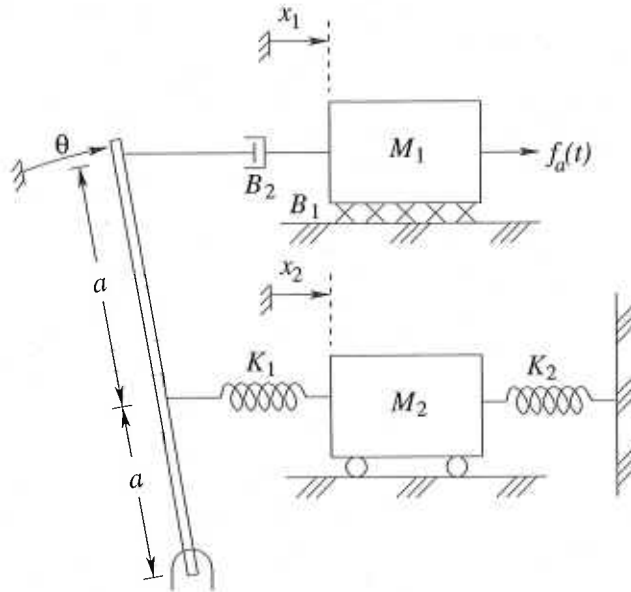


Figure 4: Mechanical system for question 4.

A:

assuming small theta

$$M_1 \ddot{x}_1 + (B_1 + B_2) \dot{x}_1 - B_2 2a \dot{\theta} = f_a(t)$$

B:

$$M_2 \ddot{x}_2 + (K_1 + K_2) x_2 - K_1 a \theta = 0$$

5. For the mechanical system shown below, sketch the free body diagram for J and write the corresponding D'Alembert's law. Do take into account gravitational force(s).

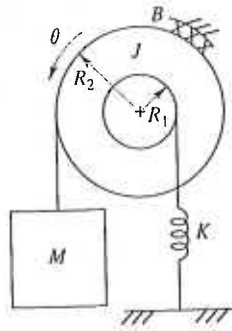


Figure 5: Mechanical system for question 5.

contact force $f_c \downarrow$
 $\tau_c = R_2 f_c$

$f_K = Kx$
 $= KR_1 \theta$
 $\tau_K = R_1 KR_1 \theta$

$$J \ddot{\theta} + B \ddot{\theta} + R_1^2 K \theta - R_2 f_c = 0$$

(can define $f_c \uparrow$)

5. For the mechanical system shown below, sketch the free body diagram for J and write the corresponding D'Alembert's law. Do take into account gravitational force(s).

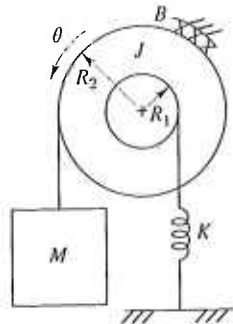


Figure 5: Mechanical system for question 5.

Alternative

Moment of inertia for mass M
 $R_2^2 M$

$$F_k = kx = kR_1 \theta$$

$$\tau_k = R_1 kR_1 \theta$$

$$(J + R_2^2 M) \ddot{\theta} + B \dot{\theta} + R_1^2 k \theta = R_2 M g$$

6. If applying D'Alembert's law to the two free body diagrams of some **A**: translational **B**: rotational mechanical system yields the following two differential equations, write the input-output differential equation where

A: $f_a(t)$ is the input and x_1 is the output.

$$\begin{aligned} \ddot{x}_1 + 5\dot{x}_1 + 2x_1 - \dot{x}_2 - x_2 &= f_a(t) \\ \ddot{x}_2 + \dot{x}_2 + 2x_2 - \dot{x}_1 - x_1 &= 0 \end{aligned}$$

B: $\tau_a(t)$ is the input and θ_1 is the output.

$$\begin{aligned} \ddot{\theta}_1 + 5\dot{\theta}_1 + 2\theta_1 - \dot{\theta}_2 - \theta_2 &= \tau_a(t) \\ \ddot{\theta}_2 + \dot{\theta}_2 + 2\theta_2 - \dot{\theta}_1 - \theta_1 &= 0 \end{aligned}$$

$$\begin{aligned} \text{A:)} \quad (D^2 + 5D + 2)x_1 + (-D - 1)x_2 &= f_a(t) \quad (1) \\ (-D - 1)x_1 + (D^2 + D + 2)x_2 &= 0 \quad (2) \end{aligned}$$

to eliminate x_2 : $(1) \times (D^2 + D + 2) - (2) \times (-D - 1)$

$$\begin{aligned} (D^2 + D + 2)(D^2 + 5D + 2)x_1 &= (D^2 + D + 2)f_a(t) \\ + (D + 1)(-D - 1)x_1 &= 0 \end{aligned}$$

$$\begin{aligned} [D^4 + 5D^3 + 2D^2 + D^3 + 5D^2 + 2D + 2D^2 + 10D + 4 \\ - D^2 - 2D - 1]x_1 &= (D^2 + D + 2)f_a(t) \end{aligned}$$

$$(D^4 + 6D^3 + 8D^2 + 6D + 3)x_1 = (D^2 + D + 2)f_a(t)$$

$$D^4 x_1 + 6D^3 x_1 + 8D^2 x_1 + 6D x_1 + 3x_1 = D^2 f_a(t) + D f_a(t) + 2f_a(t)$$

B) Similarly for θ_1

$$D^4 \theta_1 + 6D^3 \theta_1 + 8D^2 \theta_1 + 6D \theta_1 + 3\theta_1 = D^2 \tau_a(t) + D \tau_a(t) + 2\tau_a(t)$$

7. If applying D'Alembert's law to the two free body diagrams of the **A**: rotational **B**: translational mechanical system as shown below yields the following two differential equations, express the system in state variable form by

- Defining an appropriate set of state variables
- Writing the state variable equations in matrix form.

A:

$$J_1 \ddot{\theta}_1 + B_1 \dot{\theta}_1 + (K_1 + K_2)\theta_1 - K_2 \theta_2 = 0$$

$$J_2 \ddot{\theta}_2 + B_2 \dot{\theta}_2 + K_2 \theta_2 - K_2 \theta_1 = \tau_a(t)$$

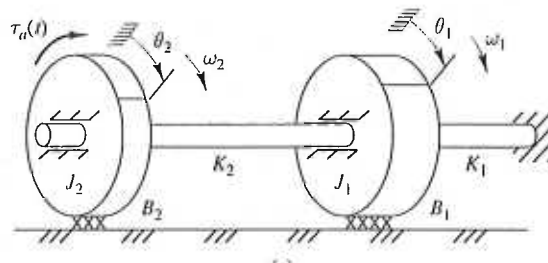


Figure 6: Rotational mechanical system for question 7.

a) Define $\theta_1, \omega_1, \theta_2, \omega_2$ as state variables

b) $\dot{\theta}_1 = \omega_1$

$\dot{\theta}_2 = \omega_2$

$\dot{\omega}_1$: from J_1 FBD

$$J_1 \dot{\omega}_1 + B_1 \omega_1 + (K_1 + K_2)\theta_1 - K_2 \theta_2 = 0$$

$$\dot{\omega}_1 = -\frac{(K_1 + K_2)}{J_1} \theta_1 - \frac{B_1}{J_1} \omega_1 + \frac{K_2}{J_1} \theta_2 + 0 \omega_2 = 0$$

$\dot{\omega}_2$: from J_2 FBD

$$J_2 \dot{\omega}_2 + B_2 \omega_2 + K_2 \theta_2 - K_2 \theta_1 = \tau_a(t)$$

$$\dot{\omega}_2 = \frac{K_2}{J_2} \theta_1 + 0 \omega_1 - \frac{K_2}{J_2} \theta_2 - \frac{B_2}{J_2} \omega_2 + \frac{1}{J_2} \tau_a(t)$$

$$\begin{bmatrix} \dot{\Theta}_1 \\ \dot{\omega}_1 \\ \dot{\Theta}_2 \\ \dot{\omega}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ \frac{-(k_1 k_2)}{J_1} & \frac{-B_1}{J_1} & \frac{k_2}{J_1} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_2}{J_2} & 0 & \frac{-k_2}{J_2} & \frac{-B_2}{J_2} \end{bmatrix} \begin{bmatrix} \Theta_1 \\ \omega_1 \\ \Theta_2 \\ \omega_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ \frac{1}{J_2} \end{bmatrix} \quad \text{Eq(1)}$$

B:

$$M_1 \ddot{x}_1 + B_1 \dot{x}_1 + K_1 x_1 - K_1 x_2 = f_a(t)$$

$$M_2 \ddot{x}_2 + B_2 \dot{x}_2 + (K_1 + K_2)x_2 - K_1 x_1 = 0$$

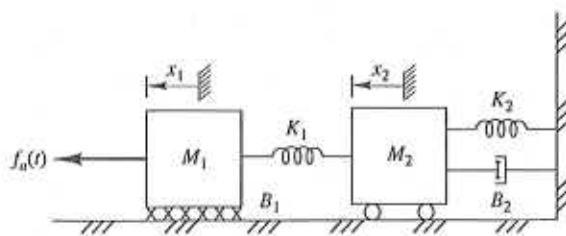


Figure 7: Translational mechanical system for question 7.

Similarly

$$\begin{bmatrix} \ddot{x}_1 \\ \dot{x}_1 \\ x_2 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -\frac{(K_1+K_2)}{M_1} & -\frac{B_1}{M_1} & \frac{K_1}{M_1} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{K_1}{M_2} & 0 & -\frac{K_1}{M_2} & -\frac{B_2}{M_2} \end{bmatrix} \begin{bmatrix} x_1 \\ \dot{x}_1 \\ x_2 \\ \dot{x}_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ \frac{1}{M_2} f_a(t) \end{bmatrix}$$