



Module 2
Supplemental Materials

Example:

A Multimode Fiber



QUESTION

Calculate the number of allowed modes in a multimode step index fiber which has a core of refractive index of 1.468 and diameter $100\ \mu\text{m}$, and a cladding of refractive index of 1.447 if the source wavelength is $850\ \text{nm}$.

SOLUTION

Substitute, $a = 50 \mu\text{m}$, $\lambda = 0.850 \mu\text{m}$, $n_1 = 1.468$, $n_2 = 1.447$ into the expression for the V -number,

$$V = (2\pi a/\lambda)(n_1^2 - n_2^2)^{1/2} = (2\pi 50/0.850)(1.468^2 - 1.447^2)^{1/2} \\ = 91.44.$$

Since $V \gg 2.405$, the number of modes is

$$M \approx V^2/2 = (91.44)^2/2 = 4181$$

which is large.

Example:

A Single Mode Fiber



QUESTION

What should be the core radius of a single mode fiber which has a core of $n_1 = 1.4680$, cladding of $n_2 = 1.447$ and it is to be used with a source wavelength of $1.3 \mu\text{m}$?

SOLUTION

For single mode propagation, $V \leq 2.405$. We need,

$$V = (2\pi a/\lambda)(n_1^2 - n_2^2)^{1/2} \leq 2.405$$

or

$$[2\pi a/(1.3 \mu\text{m})](1.468^2 - 1.447^2)^{1/2} \leq 2.405$$

which gives **$a \leq 2.01 \mu\text{m}$** .

Rather thin for easy coupling of the fiber to a light source or to another fiber; a is comparable to λ which means that the geometric ray picture, strictly, cannot be used to describe light propagation.

Example:

Single Mode Cut-off Wavelength



QUESTION

Calculate the cut-off wavelength for single mode operation for a fiber that has a core with diameter of $8.2 \mu\text{m}$, a refractive index of 1.4532, and a cladding of refractive index of 1.4485. What is the V -number and the mode field diameter (MFD) for operation at $\lambda = 1.31 \mu\text{m}$?

SOLUTION

For single mode operation,

$$V = (2\pi a/\lambda)(n_1^2 - n_2^2)^{1/2} \leq 2.405$$

Substituting for a , n_1 and n_2 and rearranging we get,

$$\lambda > [2\pi(4.1 \mu\text{m})(1.4532^2 - 1.4485^2)^{1/2}]/2.405 = 1.251 \mu\text{m}$$

Wavelengths shorter than 1.251 μm give multimode propagation.

At $\lambda = 1.31 \mu\text{m}$,

$$V = 2\pi [(4.1 \mu\text{m})/(1.31 \mu\text{m})](1.4532^2 - 1.4485^2)^{1/2} = 2.30$$

Mode field diameter MFD

SOLUTION (CONT'D)

Mode field diameter MFD from the Marcuse Equation is

$$\begin{aligned}2w &= 2a(0.65 + 1.619V^{-3/2} + 2.879V^{-6}) \\ &= 2(4.1)[0.65 + 1.62(2.30)^{-3/2} + 2.88(2.30)^{-6}]\end{aligned}$$

$$2w = 9.30 \mu\text{m} \quad 86\% \text{ of total power is within this diameter.}$$

$$2w = (2a)(2.6/V) = 2(4.1)(2.6/2.30) = 9.28 \mu\text{m}$$

$$2w = 2a[(V+1)/V] = 11.8 \mu\text{m} \quad \text{This is for a planar waveguide, and the definition is different than that for an optical fiber.}$$

Example:

A Multimode Fiber and Total Acceptance Angle



QUESTION

A step index fiber has a core diameter of 100 μm and a refractive index of 1.480. The cladding has a refractive index of 1.460. Calculate the numerical aperture of the fiber, acceptance angle from air, and the number of modes sustained when the source wavelength is 850 nm.

$$\text{Normalized refractive index} \\ \Delta = (n_1 - n_2) / n_1 = \mathbf{0.0135 \text{ or } 1.35\%}$$

SOLUTION

The numerical aperture is

$$NA = (n_1^2 - n_2^2)^{1/2} = (1.480^2 - 1.460^2)^{1/2} = \mathbf{0.2425 \text{ or } 24.3\%}$$

$$\text{From, } \sin \alpha_{\max} = NA/n_o = 0.2425/1$$

$$\text{Acceptance angle } \alpha_{\max} = \mathbf{14^\circ}$$

$$\text{Total acceptance angle } 2\alpha_{\max} = \mathbf{28^\circ}$$

V-number in terms of the numerical aperture can be written as,

$$V = (2\pi a/\lambda)NA = [(2\pi 50 \mu\text{m})/(0.85 \mu\text{m})](0.2425) = 89.62$$

$$\text{The number of modes, } M \approx V^2/2 = \mathbf{4016}$$

Example:

A Single Mode Fiber and Cut-off Wavelength



QUESTION

A typical single mode optical fiber has a core of diameter $8\ \mu\text{m}$ and a refractive index of 1.460. The normalized index difference is 0.3%. The cladding diameter is $125\ \mu\text{m}$. Calculate the numerical aperture and the total acceptance angle of the fiber. What is the single mode cut-off frequency λ_c of the fiber?

SOLUTION

The numerical aperture

$$NA = (n_1^2 - n_2^2)^{1/2} = [(n_1 + n_2)(n_1 - n_2)]^{1/2}$$

Substituting $(n_1 - n_2) = n_1\Delta$ and $(n_1 + n_2) \approx 2n_1$, we get

$$NA \approx [(2n_1)(n_1\Delta)]^{1/2} = n_1(2\Delta)^{1/2} = 1.46(2 \times 0.003)^{1/2} = \mathbf{0.113 \text{ or } 11.3 \%}$$

The acceptance angle is given by

$$\sin \alpha_{max} = NA/n_o = 0.113/1 \text{ or } \alpha_{max} = \mathbf{6.5^\circ}, \text{ and } 2\alpha_{max} = \mathbf{13^\circ}$$

SOLUTION (CONT'D)

The condition for single mode propagation is $V \leq 2.405$. At cut-off,

$$V = (2\pi a/\lambda_c)(n_1^2 - n_2^2)^{1/2} = 2.405$$

$$\therefore \lambda_c = [2\pi a \text{NA}]/2.405 = [(2\pi)(4 \mu\text{m})(0.113)]/2.405 = \mathbf{1.18 \mu\text{m}}$$

Wavelengths shorter than $1.18 \mu\text{m}$ will result in multimode operation.

Dispersion = Spread of Information



DISPERSION = SPREAD OF INFORMATION

- Intermode (Intermodal) Dispersion:
Multimode fibers only
- Material Dispersion
 - Group velocity depends on N_g and hence on λ
- Waveguide Dispersion
 - Group velocity depends on waveguide structure
- Chromatic Dispersion
 - Material dispersion + Waveguide Dispersion
- Polarization Dispersion
- Profile Dispersion
 - Like material and waveguide dispersion. Add all 3: Material + Waveguide + Profile
- Self phase modulation dispersion

Example:

Combining Intermodal and Intramodal Dispersions



QUESTION

Consider a graded index fiber with a core diameter of $30\ \mu\text{m}$ and a refractive index of 1.474 at the center of the core and a cladding refractive index of 1.453. Suppose that we use a laser diode emitter with a spectral linewidth of 3 nm to transmit along this fiber at a wavelength of 1300 nm. Calculate, the total dispersion and estimate the bit-rate \times distance product of the fiber. The material dispersion coefficient D_m at 1300 nm is $-7.5\ \text{ps}\ \text{nm}^{-1}\ \text{km}^{-1}$.

SOLUTION

The normalized refractive index difference $\Delta = (n_1 - n_2)/n_1 = (1.474 - 1.453)/1.474 = 0.01425$. Modal dispersion for 1 km is

$$\sigma_{\text{intermode}} = Ln_1\Delta^2/[(20)(3^{1/2})c] = 2.9 \times 10^{-11} \text{ s}^1 \text{ or } 0.029 \text{ ns.}$$

The material dispersion is

$$\Delta\tau_{1/2} = LD_m\Delta\lambda_{1/2} = (1 \text{ km})(7.5 \text{ ps nm}^{-1} \text{ km}^{-1})(3 \text{ nm}) = 0.0225 \text{ ns}$$

Assuming a Gaussian output light pulse shape,

$$\sigma_{\text{intramode}} = 0.425\Delta\tau_{1/2} = (0.425)(0.0225 \text{ ns}) = 0.0096 \text{ ns}$$

SOLUTION (CONT'D)

Total dispersion is

$$\sigma_{\text{rms}} = \sqrt{\sigma_{\text{intermode}}^2 + \sigma_{\text{intramode}}^2} = \sqrt{0.029^2 + 0.0096^2} = 0.030 \text{ ns}$$

Assume $L = 1 \text{ km}$

$$B = 0.25/\Delta\tau_{\text{rms}} = \mathbf{8.2 \text{ Gb}}$$

Example:

Power Attenuation



QUESTION

A 12-km long optical fiber has a loss of 1.5 dB/km. What is the minimum optical power level that must be launched into the fiber to maintain an optical power level of $0.3 \mu\text{W}$ at the receiving end? How about if the loss is 2.5 dB/km.

SOLUTION

$$dB = -10 \log_{10} \frac{P_{out}}{P_{in}}$$

$$P_{in} = P_{out} 10^{\alpha L/10} = (0.3 \mu W) 10^{(1.5)(12)/10} = 18.9 \mu W$$

$$P_{in} = P_{out} 10^{\alpha L/10} = (0.3 \mu W) 10^{(2.5)(12)/10} = 300 \mu W$$