

## Gases in PFRs (& batch reactors)



Fogler  
defines  
 $\delta = \frac{d}{a} + \frac{c}{a} - \frac{b}{a} - 1$

$$\Delta = (c+d) - (a+b) \dots \text{stoichiometric change}$$

① Case 1: Temp. & volume constant  
 $\Delta \neq 0$

$$P_{A0} = n_{A0} \frac{RT}{\dot{V}} \dots \underline{\dot{V} \text{ or } V}$$

$$P_A = n_A \frac{RT}{\dot{V}}$$

$$\therefore P_{A0} - P_A = (n_{A0} - n_A) \frac{RT}{\dot{V}}$$

From stoichiometry:

For every a moles of A that reacts, the change of moles is  $\Delta$

$\therefore$  For  $(n_{A0} - n_A)$ , the change is  $\frac{\Delta}{a} (n_{A0} - n_A)$

For the whole system:

$$\Delta P = \frac{\Delta n RT}{V}$$

$$\& \Delta n = \frac{\Delta}{a} (n_{A0} - n_A)$$

$$\therefore (-\pi_0 + \pi) = \frac{\Delta}{a} (n_{A0} - n_A) \frac{RT}{V}$$

final-initial

$$\therefore \pi - \pi_0 = \frac{\Delta}{a} (P_{A0} - P_A)$$

$$\therefore P_{A0} - P_A = \frac{a}{\Delta} (\pi - \pi_0)$$

$$\therefore P_A = P_{A0} + \frac{a}{\Delta} (\pi_0 - \pi)$$

For products:

$$P_C = P_{C0} - \frac{c}{\Delta} (\pi_0 - \pi)$$

..... derive using stoichiometry

What happens if  $\Delta = 0$  &  $T$  &  $V$  are constant?  
 $P = \text{constant!}$

② Case 2: T & P constant, V & n change  
i.e.  $\Delta \neq 0$

$$\text{Definition} \equiv \varepsilon = \frac{U_{X_A=1} - U_{X_A=0}}{U_{X_A=0}}$$

For  $X_A=1$ , moles of A reacted =  $n_{A0}$

$$\therefore \text{total change in moles} = \frac{\Delta \cdot n_{A0}}{\alpha}$$

$$\therefore \Delta V = \Delta n \left( \frac{RT}{P} \right)$$

$$\therefore V - V_0 = \frac{\Delta n_{A0}}{\alpha} \left( \frac{RT}{P} \right) \quad \text{--- for } \underline{\underline{\varepsilon}}$$

$$\therefore U = U_0 + \frac{RT}{P} \left( \frac{\Delta \cdot n_{A0}}{\alpha} \right) \quad \text{all moles of A have reacted}$$

$U_{X_A=1}$        $U_{X_A=0}$

$$\varepsilon = \frac{U - U_0}{U_0} = \frac{RT}{P U_0} \left( \frac{\Delta \cdot n_{A0}}{\alpha} \right)$$

$$\therefore \epsilon = \frac{RT}{Pv_0} \left( \frac{\Delta \cdot n_{A0}}{a} \right)$$

fn. of mole fraction & stoichiometry

$$\epsilon = (\text{initial mole frac.}) \times \frac{\Delta}{a}$$

$$\therefore \epsilon = \frac{n_0^{-1} n_{A0} \Delta}{a}$$

basis for problem (can be any species)

But,  $v - v_0 = \frac{\Delta}{a} (n_{A0} - n_A) \frac{RT}{P}$

general case

$$\therefore v - v_0 = \frac{\Delta}{a} n_{A0} \left( \frac{n_{A0} - n_A}{n_{A0}} \right) \frac{RT}{P}$$

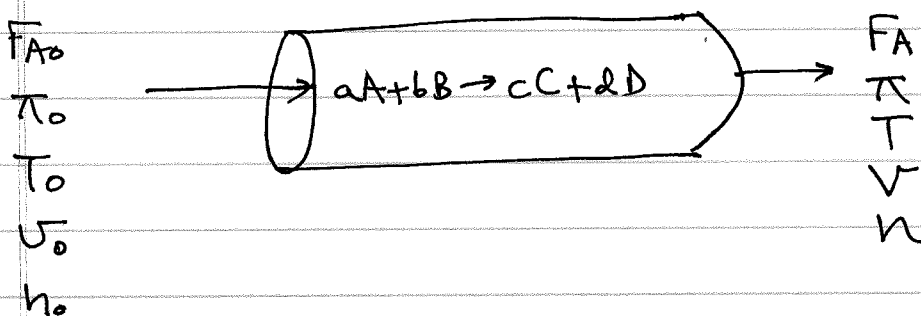
$$\therefore v - v_0 = \left( \frac{\Delta n_{A0}}{a} \right) \sum_A \left( \frac{RT}{Pv_0} \right) v_0$$

$$\therefore v - v_0 = \left( \frac{n_0^{-1} \Delta n_{A0}}{a} \right) \sum_A v_0 \dots \epsilon = \frac{n_{A0} \Delta}{n_0 a}$$

$$\therefore v = v_0 + v_0 \epsilon \sum_A$$

$$\therefore v = v_0 (1 + \epsilon \sum_A)$$

Case 3: Generalized flow case  
( $T, P, V, n$  changing)



As before,  $\Delta = d + c - b - a$

Fogler uses:  $\delta = \frac{d}{a} + \frac{c}{a} - \frac{b}{a} - 1$

$$\therefore \frac{\Delta}{a} = \delta$$

Let us start from the ideal gas law,

$$PV = nRT$$

For our system:

$$\pi_0 V_0 = n_0 R T_0$$

$$\& \pi V = n R T$$

Dividing these equations, we get:

$$\frac{\pi_0 v_0}{\pi v} = \frac{h_0 T_0}{h T}$$

$$\therefore \frac{\pi_0 v_0 h T}{\pi h_0 T_0} = v$$

$$\therefore v = v_0 \left\{ \frac{\pi_0 \cdot h \cdot T}{\pi \cdot h_0 \cdot T_0} \right\}$$

In case of non-ideality:

$$PV = z n R T$$

compressibility  
factor

FYI: when does the ideal gas law start to fail?

High P, low T (HPLT!)  
→ instead of HPLC 😊

\* What happens when you pressurise a gas  
↳ becomes liquid!

Recollect from thermodynamics:

$$Z = f(T, P, V)$$

Example: Virial Equations of State

The virial equation in pressure:

$$Z = 1 + B'P + C'P^2 + D'P^3 + \dots$$

$$B' = \frac{B}{RT}, \quad C' = \frac{C - B^2}{(RT)^2} \text{ \& so on}$$

$$B = \sum_i \sum_j y_i y_j B_{ij}$$

depends on composition  $\rightarrow$   $B$   $\leftarrow$  mole fractions  $\leftarrow$  interaction parameter

$$C = \sum_i \sum_j \sum_k y_i y_j y_k C_{ij}$$

Nevertheless,

$$P_0 V_0 = n_0 Z_0 R T_0$$

$$P V = n Z R T$$

$$\therefore \frac{P_0 V_0}{P V} = \left( \frac{n_0}{n} \right) \left( \frac{Z_0}{Z} \right) \left( \frac{T_0}{T} \right)$$

$$\therefore V = V_0 \left\{ \frac{\pi_0 \cdot n \cdot T}{\pi \cdot n_0 \cdot T_0} \frac{Z}{Z_0} \right\}$$

Recollect

$$\Delta n = n - n_0 \quad \dots \text{change in moles}$$

can be related  
to conversion

$$\text{If } a \text{ moles} \longrightarrow \Delta \text{ moles (from stoich.)}$$

$$n_{A0} - n_A \longrightarrow \Delta n$$

$$\therefore \Delta n = (n_{A0} - n_A) \frac{\Delta}{a} \quad \text{stoch. coeff.}$$

change

$$\therefore \Delta n = \left( \frac{n_{A0} - n_A}{n_{A0}} \right) \frac{\Delta n_{A0}}{a}$$

$$\therefore \Delta n = \frac{\sum_A (\Delta) n_{A0}}{a}$$

$$\therefore \Delta n = \sum_A \underbrace{\left( \frac{\Delta}{a} \right)}_{\epsilon} \frac{n_{A0}}{n_0} \cdot n_0$$

$$\therefore \Delta n = \sum_A \epsilon n_0$$

$$\therefore n - n_0 = n_0 \epsilon X_A$$

$$\therefore n = n_0 (1 + \epsilon X_A)$$

$$\therefore \frac{n}{n_0} = 1 + \epsilon X_A \longrightarrow \text{subst. in volume term}$$

$$\therefore v = v_0 \left( \frac{p_0}{p} \right) \left( \frac{T}{T_0} \right) \left( \frac{z}{z_0} \right) (1 + \epsilon X_A)$$

Compare to case when T & P were constant.

Other definitions:

$$Q_i = \frac{F_{i0}}{F_{A_0}}$$

basis species  
(for which we define  $X_A$ )

Also, stoichiometry is key.

Consider  $aA + bB \rightarrow cC + dD$

$$N_A = N_{A0} - N_{A0} X_A$$

$\uparrow$                      $\uparrow$                      $\uparrow$   
 final                  original                  change

& from stoichiometry:

$$\begin{aligned} \text{moles of A reacted} &= N_{A0} X_A \\ \therefore \text{moles of B reacted} &= \left(\frac{b}{a}\right) N_{A0} X_A \\ \therefore \text{moles of C produced} &= \left(\frac{c}{a}\right) N_{A0} X_A \\ \therefore \text{moles of D produced} &= \left(\frac{d}{a}\right) N_{A0} X_A \end{aligned} \quad \left. \vphantom{\begin{aligned} \text{moles of A reacted} \\ \therefore \text{moles of B reacted} \\ \therefore \text{moles of C produced} \\ \therefore \text{moles of D produced} \end{aligned}} \right\} \text{change terms}$$

$$\therefore N_B = N_{B0} - N_{A0} X_A \left(\frac{b}{a}\right)$$

$$N_C = N_{C0} + \left(\frac{c}{a}\right) N_{A0} X_A$$

$$N_D = N_{D0} + \left(\frac{d}{a}\right) N_{A0} X_A$$

$$\text{Also, } N_{B0} = \theta_B N_{A0}$$

$$N_{C0} = \theta_C N_{A0}$$

$$N_{D0} = \theta_D N_{A0}$$

$$\therefore N_A = N_{A0} (1 - X_A)$$

$$N_B = N_{A0} \left( \alpha_B - \frac{b X_A}{a} \right)$$

$$N_C = N_{A0} \left( \alpha_C + \frac{c X_A}{a} \right)$$

$$N_D = N_{A0} \left( \alpha_D + \frac{d X_A}{a} \right)$$

→ all species written in terms of  $N_{A0}, X_A$

Consider  $N_A$  &  $C_A$ :

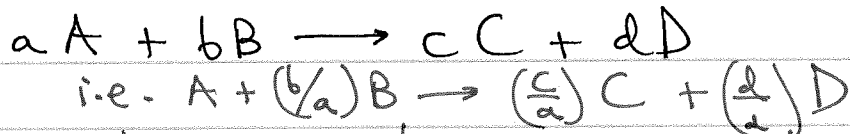
(consider ideal gas)  
(if non-ideal correlation will be given)

$$C_A = \frac{N_A}{V} = \frac{N_{A0} (1 - X_A)}{V_0 \left( \frac{\pi_0 T}{\pi T_0} \right) (1 + \epsilon X_A)}$$

$$\therefore C_A = \left( \frac{N_{A0}}{V_0} \right) \frac{(1 - X_A)}{(1 + \epsilon X_A)} \left( \frac{\pi T_0}{\pi_0 T} \right)$$

$$\therefore C_A = C_{A0} \left( \frac{\pi T_0}{\pi_0 T} \right) \left( \frac{1 - X_A}{1 + \epsilon X_A} \right)$$

What is the protocol for batch & flow reactors?



Species	Initial	Change	Final	Final Conc.
A	$N_{A0}$	$-N_{A0}X_A$	$N_{A0}(1-X_A)$	$\frac{N_A}{V} = C_A$
B	$Q_B N_{A0}$	$-(b/a)N_{A0}X_A$	$N_{A0}\left(Q_B - \frac{bX_A}{a}\right)$	$\frac{N_B}{V} = C_B$
C	$Q_C N_{A0}$	$+(c/a)N_{A0}X_A$	$N_{A0}\left(Q_C + \frac{cX_A}{a}\right)$	$\frac{N_C}{V} = C_C$
D	$Q_D N_{A0}$	$+(d/a)N_{A0}X_A$	$N_{A0}\left(Q_D + \frac{dX_A}{a}\right)$	$\frac{N_D}{V} = C_D$
I	$Q_I N_{A0}$	0	$Q_I N_{A0}$	$\frac{N_I}{V} = C_I$

inert species

$$V = V_0 \left( \frac{\pi_0 T Z}{\pi T_0 Z_0} \right) (1 + \epsilon X_A)$$

Eg.  $\therefore C_A = \frac{N_{A0}(1-X_A)}{V_0 \left( \frac{\pi_0 T Z}{\pi T_0 Z_0} \right) (1 + \epsilon X_A)}$

assume ideal when true

$$\therefore C_A = \frac{N_{A0}}{V_0} \left( \frac{\pi T_0 Z_0}{\pi_0 T Z} \right) \left( \frac{1-X_A}{1+\epsilon X_A} \right)$$

$$\therefore C_A = C_{A0} \left( \frac{\pi T_0 Z_0}{\pi_0 T Z} \right) \left( \frac{1-X_A}{1+\epsilon X_A} \right)$$

Similarly,

$$C_B = C_{A0} \left( \frac{\pi T_0 Z_0}{\pi_0 T Z} \right) \left( \frac{O_B - \frac{b}{a} X_A}{1 + \epsilon X_A} \right)$$

$$C_C = C_{A0} \left( \frac{\pi T_0 Z_0}{\pi_0 T Z} \right) \left( \frac{O_C - \frac{c}{a} X_A}{1 + \epsilon X_A} \right) \text{ \& so on}$$

$$\boxed{\frac{C_{B0}}{C_{C0}} = \frac{O_B}{O_C}}$$

\&

$$\boxed{\frac{C_B}{C_C} = \frac{O_B - \frac{b}{a} X_A}{O_C - \frac{c}{a} X_A}}$$

Now,  $\boxed{dV = \left( \frac{F_{A0}}{-r_A} \right) dX_A}$  ... volume of a PFR

$$\text{If } -r_A = k C_A C_B$$

$$\therefore -r_A = k \left[ C_{A0} \left( \frac{\pi T_0 Z_0}{\pi_0 T Z} \right) \right]^2 \left( \frac{1 - X_A}{1 + \epsilon X_A} \right) \left( \frac{O_B - \frac{b}{a} X_A}{1 + \epsilon X_A} \right)$$

$$\therefore -r_A = k \left( \frac{C_{A0} \pi T_0 Z_0}{\pi_0 T Z} \right)^2 \frac{(1 - X_A) (O_B - \frac{b}{a} X_A)}{(1 + \epsilon X_A)^2}$$

$$\therefore \frac{F_{A0}}{-r_A} = \frac{(1 + \epsilon X_A)^2}{(1 - X_A) (O_B - \frac{b}{a} X_A)} \left( \frac{\pi_0 T Z}{C_{A0} \pi T_0 Z_0} \right)^2 \frac{1}{k} \cdot C_{A0} V_0$$

$$\therefore \frac{F_{A0}}{-v_A} = \frac{(1 + \epsilon X_A)^2}{(1 - X_A) \left( C_B - \frac{b}{a} X_A \right)} \left( \frac{\pi_0 T Z}{\pi T_0 Z_0} \right)^2 \frac{U_0}{k C_{A0}}$$

$$\therefore dV = \left( \frac{\pi_0 T Z}{\pi T_0 Z_0} \right)^2 \frac{U_0}{k C_{A0}} \frac{(1 + \epsilon X_A)^2}{(1 - X_A) \left( C_B - \frac{b}{a} X_A \right)} dX_A$$

↓  
Solve ODE