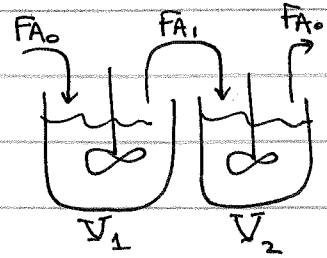
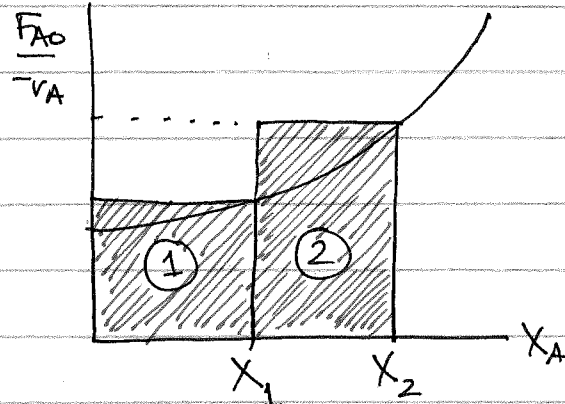


Let's look @ a general CSTR-in-series case:

Recollect:



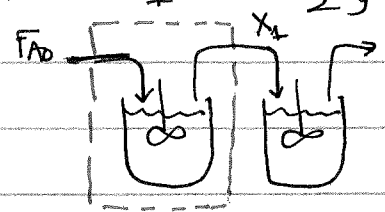
what does  
this mean?

and this?

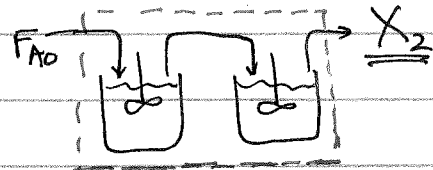
The  $X$  refers to conversion until that point.

∴ If reactor volumes are  $V_1$  &  $V_2$ ,

$$X_{A1} = \frac{F_{A0} - F_{A1}}{F_{A0}}$$



$$X_{A2} = \frac{F_{A0} - F_{A2}}{F_{A0}}$$



$$∴ F_{A1} = F_{A0} (1 - X_{A1})$$

$$F_{A2} = F_{A0} (1 - X_{A2})$$

Design eqns:

\* Don't panic, just write them out systematically

$$F_{A0} - F_{A1} = (-r_A)_1 V_1$$

$$F_{A1} - F_{A2} = \underbrace{(-r_A)_2}_{\text{why did we subscript } -r_A?} V_2$$

The conditions could be different (e.g. T)

If isothermal (which is what we have been assuming):

$$F_{A0} - F_{A1} = (-r_A) V_1$$

$$F_{A1} - F_{A2} = (-r_A) V_2$$

$$\therefore F_{A0} X_{A1} = (-r_A) V_1$$

$$\& F_{A0} (1 - X_{A1}) - F_{A0} (1 - X_{A2}) = (-r_A) V_2$$

$$\therefore F_{A0} X_{A1} = (-r_A) V_1$$

$$F_{A0} (X_{A2} - X_{A1}) = (-r_A) V_2$$

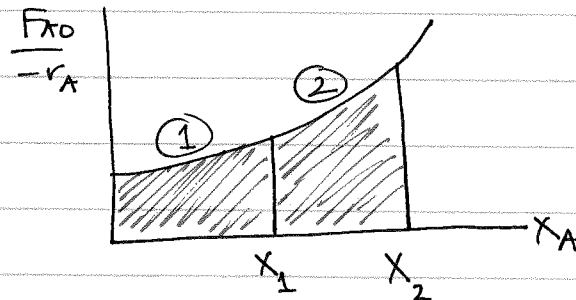
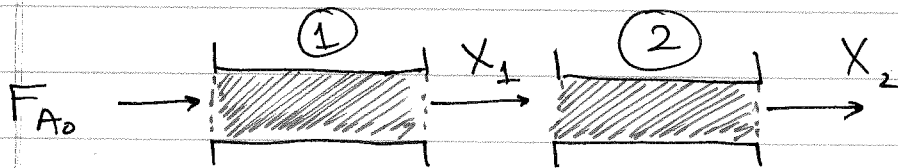
$$\therefore \frac{C_{A1} V_1}{C_{A2} V_2} = \frac{X_{A1}}{X_{A2} - X_{A1}} \quad \dots \text{isothermal case}$$

For non-isothermal case (i.e.  $T_1 \neq T_2$ ):

$$\frac{k_1 V_1 C_{A1}}{k_2 V_2 C_{A2}} = \frac{X_{A1}}{X_{A2} - X_{A1}}$$

other cases such as  $V_1 = V_2$   
etc. can be derived  
appropriately

What about PFRs in series?



$$\frac{dF_A}{dV} = r_A \quad \dots \text{start with the design equation}$$

$$F_{A0} \frac{dX_A}{dV} = -r_A$$

$$dV = \left( \frac{F_{A0}}{-r_A} \right) dX_A$$

For reactor 1  $dV|_1 = \left( \frac{F_{A0}}{-r_{A1}} \right) dX_A$

$$\therefore \int dV_1 = \int_0^{X_{A1}} \left( \frac{F_{A0}}{-r_A} \right) dX_A$$

$$\therefore V_1 = \int_0^{X_{A1}} \left( \frac{F_{A0}}{-r_A} \right) dX_A$$

$$V_2 = \int_{X_{A1}}^{X_{A2}} \left( \frac{F_{A0}}{-r_A} \right) dX_A$$

.....  $F_{A0}$  const.  
throughout

$$\therefore V_1 + V_2 = \int_0^{X_{A2}} \left( \frac{F_{A0}}{-r_A} \right) dX_A$$

just 'doubling'  
the pipe  
(or elongating it)

if  $V_1 = V_2$

$$\int_0^{X_{A1}} \left( \frac{F_{A0}}{-r_A} \right) dX_A = \int_{X_{A1}}^{X_{A2}} \left( \frac{F_{A0}}{-r_A} \right) dX_A$$

→ give  $X_{A2}$ , find  $X_{A1}$ .

## Residence time & space velocity

$$v \equiv \frac{\text{volume}}{s}$$

$$V \equiv \text{volume}$$

$$\frac{V}{v} \equiv \text{seconds}$$

time spent by a molecule  
or unit reacting element in  
the reactor

$$\left\{ \begin{array}{l} \text{residence} \\ \text{time} \end{array} \right\} = \frac{V}{v} = \tau$$

$$\frac{F_{A0}}{-r_A} = \frac{C_{A0} v}{k f(C_A)} \implies F_{A0} X_A = (-r_A) V$$

$$\therefore X_A = \frac{(-r_A) \cdot V}{F_{A0}}$$

$$\therefore X_A = \frac{k f(C_A) V}{C_{A0} v}$$

$$\therefore X_A = \frac{k \tau f(C_A)}{C_{A0}}$$

$$\underbrace{X_A}_{\text{dimensionless}} = \frac{(k\tau)}{C_{A0}} \underbrace{f(C_A)}_{\text{dimensionless}}$$

$k \equiv$  units depend on order

$$k \equiv \frac{1}{(\text{conc.})^{n-1} \times \text{time}}$$

order of the rxn.

$\therefore$  For a first order rxn.,  $k = \frac{1}{\text{time}}$  & so on.

In reactor design, we introduce another dimensionless quantity

$\rightarrow$  Damköhler Number  $\equiv Da$

1<sup>st</sup> order  $\quad \underline{Da = k\tau}$

2<sup>nd</sup> order  $\quad \underline{Da = k\tau C_{A0}}$  & so on....

Space velocity  $\equiv \frac{1}{\tau}$  ..... rarely used