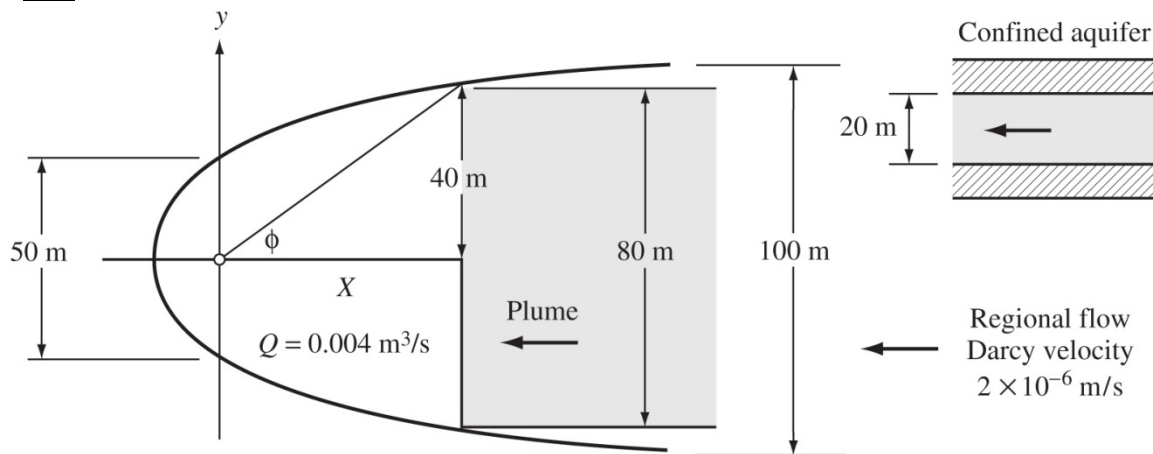


CVG 2132 Final Exam Review Problems

Groundwater Example

- Consider a confined aquifer having a thickness of 20 m, a hydraulic conductivity of 1.0×10^{-3} m/s and a regional hydraulic gradient equal to 0.002. The maximum pumping rate has been determined to be $0.004 \text{ m}^3/\text{s}$. The aquifer has been contaminated and, for simplicity, consider the plume to be rectangular, with a width of 80 m. Locate a single extraction well so that it can totally remove the plume.

ANS:



Given:

$$B = 20 \text{ m}$$

$$K = 1.0 \times 10^{-3} \text{ m/s (seems like clay)}$$

$$dh/dL = 0.002$$

$$Q_{\text{max}} = 0.004 \text{ m}^3/\text{s}$$

$$w_{\text{plume}} = 80 \text{ m}$$

First determine Darcy velocity of the aquifer:

$$q = K(dh/dL) = 1.0 \times 10^{-3} \times 0.002 = 2.0 \times 10^{-6} \text{ m/s}$$

Second determine the width of the capture zone at well:

$$W_{\text{capture zone at well}} = Q/(2qB) = 0.004 \text{ m}^3/\text{s} / [2 \times 20 \text{ m} \times 2.0 \times 10^{-6} \text{ m/s}] = 50 \text{ m}$$

Now determine the maximum width of the capture zone:

$$W_{\text{max of capture zone}} = Q/(qB) = 0.004 \text{ m}^3/\text{s} / [20 \text{ m} \times 2.0 \times 10^{-6} \text{ m/s}] = 100 \text{ m}$$

Therefore an 80m wide plume will fit in the capture zone if the well is located an appropriate distance downgradient of the front of the plume.

Let $Y = 40 \text{ m}$ (see diagram above).

Calculate ϕ and use this value to calculate X .

$$Y = \frac{Q}{2qB} \left(1 - \frac{\phi}{\pi}\right) = 40 = 50 \left(1 - \frac{\phi}{\pi}\right)$$

$$\phi = 0.2\pi \text{ rad}$$

Now use ϕ to calculate X .

$$X = Y/(\tan \phi) = 55 \text{ m}$$

The extraction well should be placed 55 m ahead of the oncoming plume at the time of installation and the well should be directly in the middle of the plume.

Stream DO Example

- A stream with $k_r = 0.31 \text{ d}^{-1}$ (base 10), temperature of 28°C , and minimum river flow of $23.0 \text{ m}^3/\text{s}$ receives $3.80 \times 10^4 \text{ m}^3/\text{d}$ of sewage from a city. The oxygen demand of the river before it intersects with the discharge pipe is negligible. What is the maximum permissible BOD of the sewage if the DO content of the stream is never to fall below 4.0 mg/L and the DO content of the sewage is assumed to be zero and the temperature of the sewage is also 28°C . ? The river is saturated with DO (7.83 mg/L) before the sewage outfall. Assume $k_d = 0.17 \text{ d}^{-1}$ (base 10). NOTE: both rate constants are base 10 and are given for a temperature of 28°C .

ANS:

NOTE: in the solution below k_d is denoted as k_1' and k_r is denoted as k_2' since they are base 10 coefficients.

Given:

$$Q_w = 3.80 \times 10^4 \text{ m}^3/\text{d}, T = 28^\circ\text{C}, \text{DO} = \text{zero}$$

$$Q_r = 23.0 \text{ m}^3/\text{s}, T = 28^\circ\text{C}, \text{DO} = \text{Saturated}$$

$$L_r = \text{zero}$$

$$\text{At } 28^\circ\text{C}, \text{Saturated} = 7.83 \text{ mg/L}$$

The primed coefficients refer to the fact that they are base 10:

$$k_1' = 0.17 \text{ d}^{-1}; k_2' = 0.31 \text{ d}^{-1}$$

Use the conservative assumption that the sewage DO is 0.

$$D_w = 7.83 - 0.0 = 7.83 \text{ mg/L}$$

The critical deficit is

$$D_c = 7.83 - 4.0 = 3.83 \text{ mg/L}$$

Now calculate known values:

$$Q_w = \left(3.80 \times 10^4 \frac{\text{m}^3}{\text{d}} \right) \left(\frac{1 \text{ d}}{86400 \text{ s}} \right) = 0.44 \text{ m}^3/\text{s} \quad (1)$$

$$D_0 = \frac{Q_w D_w + Q_r D_r}{Q_w + Q_r} = \frac{\left(0.44 \frac{\text{m}^3}{\text{s}}\right) \left(7.83 \frac{\text{mg}}{\text{L}}\right) + \left(23.0 \frac{\text{m}^3}{\text{s}}\right) (0)}{23.0 \frac{\text{m}^3}{\text{s}} + 0.44 \frac{\text{m}^3}{\text{s}}} = 0.15 \text{mg/L} \quad (2)$$

$$L_0 = \frac{Q_w L_w + Q_r L_r}{Q_w + Q_r} = \frac{\left(0.44 \frac{\text{m}^3}{\text{s}}\right) (L_w) + \left(23.0 \frac{\text{m}^3}{\text{s}}\right) (0)}{23.0 \frac{\text{m}^3}{\text{s}} + 0.44 \frac{\text{m}^3}{\text{s}}} \quad (3)$$

At this point we need to determine L_0 ; once L_0 is determined, L_w is easily found.

D_c occurs at t_c . D_c & D_0 & k_1' & k_2' are known. We need equations that involve L_0 .

$$\frac{dD}{dt} = k_1' L_c - k_2' D_c = 0 \quad \dots dD/dt = 0 \text{ at } D_c \quad (4)$$

$$k_1' L_c - k_2' D_c = 0 \quad (5)$$

$$L_c = L_0 10^{-k_1' t_c} \quad \dots \text{from class, now in base 10} \quad (6)$$

$$k_1' L_0 10^{-k_1' t_c} = k_2' D_c \quad (\text{Using 6 in 5}) \quad (7)$$

$$L_0 = \frac{k_2'}{k_1'} D_c 10^{k_1' t_c} \quad (8)$$

$$t_c = \left(\frac{1}{k_2' - k_1'} \right) \log \left[\frac{k_2'}{k_1'} \left(1 - D_0 \frac{k_2' - k_1'}{k_1' L_0} \right) \right] \quad (9a)$$

$$= \left(\frac{1}{0.31 \text{d}^{-1} - 0.17 \text{d}^{-1}} \right) \log \left\{ \frac{0.31 \text{d}^{-1}}{0.17 \text{d}^{-1}} \left[1 - (0.15 \text{mg/L}) \frac{0.31 \text{d}^{-1} - 0.17 \text{d}^{-1}}{(0.17 \text{d}^{-1}) L_0} \right] \right\}$$

$$= 7.14 \left\{ \log \left[1.82 \left(1 - \frac{0.12}{L_0} \right) \right] \right\} \quad (9b)$$

Using (9b) in (8):

$$L_0 = \left(\frac{0.31 \text{ d}^{-1}}{0.17 \text{ d}^{-1}} \right) (3.83 \text{ mg/L}) 10^{0.17 [7.14 \log(1.82 - 0.22/L_0)]} = 6.98 \left(1.82 - \frac{0.22}{L_0} \right)^{1.21} \quad (10)$$

Solving the above equation by trial and error (which also could be done by using the solver routine in a spreadsheet):

$$L_0 = 14.5 \text{ mg/L}$$

$$t_c = 6.98 \log \left[1.82 - \frac{0.22}{14.5} \right] = 1.79 \text{ d}$$

Now (3) can be used to find L_w :

$$L_0 = \frac{Q_r L_r + Q_w L_w}{Q}$$

$$L_w = \frac{L_0(Q_r + Q_w) - Q_r L_r}{Q_w} = \frac{(14.5 \text{ mg/L})(23.44 \text{ m}^3/\text{s}) - 0}{0.44 \text{ m}^3/\text{s}} = 772 \text{ mg/L}$$