

CVG 3116 Fall 2017

Hydraulics – Tutorial 7
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Lecture 10: RVFs - Momentum

- Froude Number

$$Fr = \frac{V}{\sqrt{gL}}$$

Where L is a length scale and **depends on application**. For **general open channels**, we may take the mean depth $D_m = A/B$ (the ratio of area to the surface width):

- For rectangular channels $L=y$

$$Fr = \frac{V}{\sqrt{gy}}$$

We have seen that the water velocity in a **rectangular** channel for the **critical ($y=y_c$) flow** is given by

$$V_c = \sqrt{gy_c}$$

Let's calculate the Froude number for this flow:

$$Fr = \frac{V}{\sqrt{gy}} = \frac{\sqrt{gy_c}}{\sqrt{gy_c}} = 1$$

Subcritical flow: $y > y_c$ and $V < V_c \Rightarrow Fr < 1$

Supercritical flow: $y < y_c$ and $V > V_c \Rightarrow Fr > 1$

Lecture 10: Hydraulic Jump

- Occurs when a **supercritical** flow meets a **subcritical** flow.
- A large **energy loss** exists due to turbulence.

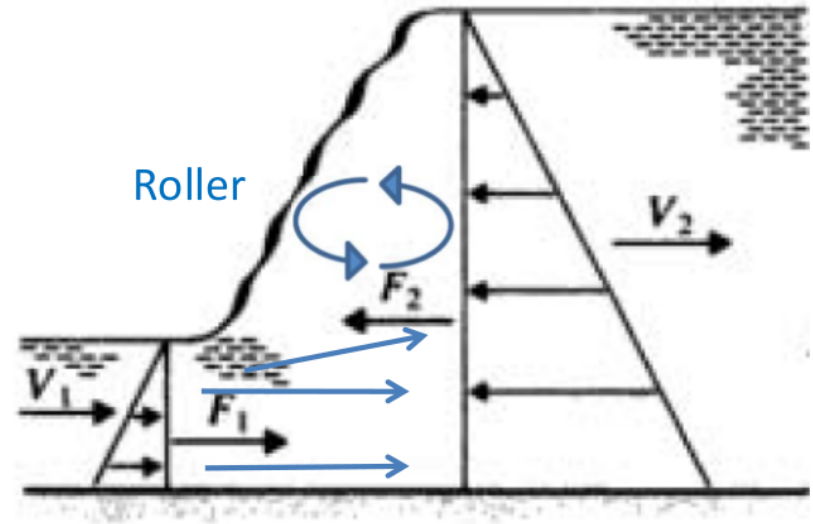
In a **rectangular** channel, the upstream and downstream depths are related via:

$$y_2 = (y_1 / 2) \left(\sqrt{1 + 8Fr_1^2} - 1 \right)$$

$$y_1 = (y_2 / 2) \left(\sqrt{1 + 8Fr_2^2} - 1 \right)$$

and the **energy loss** is given by:

$$\Delta E = \frac{(y_2 - y_1)^3}{4y_1y_2}$$



Lecture 11: Gradually varied non-uniform flow

➤ **Normal depth y_n (for a given discharge):**

- Is the depth of **uniform flow**.
- Can be calculated using the **Manning Equation**

$$Q = \frac{1}{n} \frac{A^{5/3}}{P^{2/3}} S_0^{1/2}$$

The **bed friction** is ignored in **rapidly varied flows** e.g., in hydraulic jump, because the changes happen over a short distance. But in **gradually varied flows**, the bed friction becomes important.

The normal depth can be calculated using the Manning formula with $S=S_0$

The critical slope S_c :

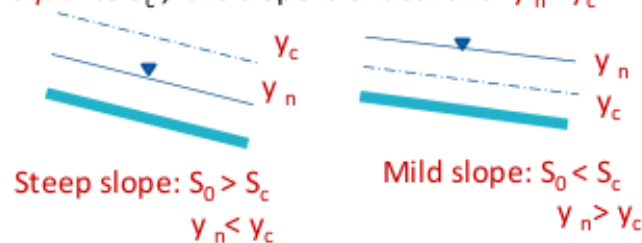
For a given discharge Q , S_c is the slope for which, the normal depth is equal to the critical depth.

i.e. Setting $y=y_c$ in the Manning formula leads to $S=S_c$.

If the channel slope S_0 is **steeper** than S_c , the slope is called **steep** slope and $y_n < y_c$

If the channel slope S_0 is **milder** than S_c , the slope is called **mild** slope and $y_n > y_c$

If the channel slope S_0 is **equal** to S_c , the slope is critical and $y_n = y_c$



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Lecture 11: Critical Slope, S_c

Manning formula:

$$Q = \frac{1}{n} \frac{A^{5/3}}{P^{2/3}} S_0^{1/2}$$

For **critical flow**, (assuming $\alpha=1$), we already know that:

$$\frac{Q^2 B}{g A^3} = 1$$

Eliminating Q:

$$\frac{1}{n} \frac{A^{5/3}}{P^{2/3}} S_c^{1/2} = \sqrt{\frac{g A^3}{B}}$$

$$S_c = \left(\frac{n Q P^{2/3}}{A^{5/3}} \right)^2$$

Where A and P are calculated based on the critical depth.

- Special Case – wide rectangular channel ($b \gg y$)

$$A = by$$

$$P = b + 2y \approx b \quad \text{because } y \ll b$$

$$S_c = g n^2 / y_c^{1/3}$$

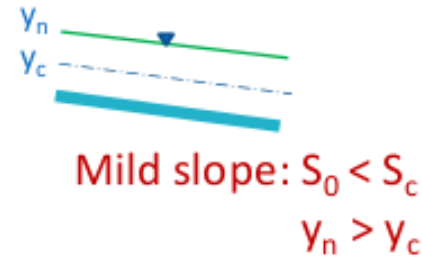
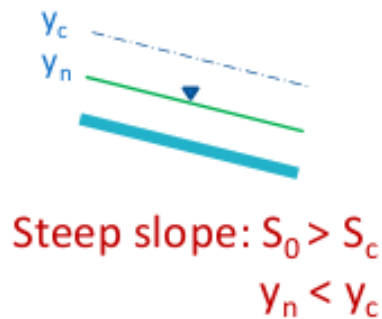
Lecture 11: Summary – mild and steep slope

➤ *Critical slope:*

S_c is the slope for which **normal depth is equal to critical depth**, i.e. if S_c is used in the Manning formula, it gives the **critical depth** ($Y_n = Y_c$).

➤ *Mild slope:* The channel slope is less than the critical slope

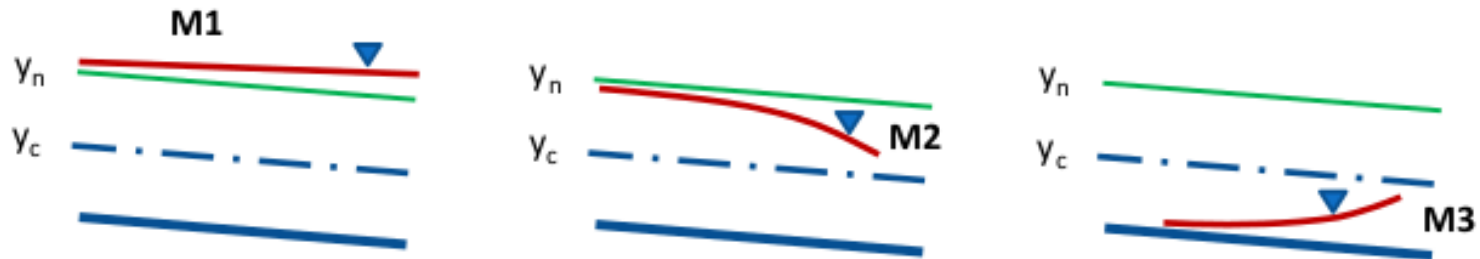
➤ *Steep slope:* The channel slope is greater than the critical slope



Note: A channel may be steep for one discharge and mild for another.

Lecture 11: Summary – mild and steep slope

- Mild Slope ($y_n > y_c$)



Water depth **increases** in region 1
Water depth **decreases** in region 2
Water depth **increases** in region 3

□ Water surface

- is **asymptotic** to $y=y_n$
- has a **large angle** with $y=y_c$

Lecture 11: Summary – mild and steep slope

- Steep Slope ($y_n < y_c$)



Water depth **increases** in region 1
Water depth **decreases** in region 2
Water depth **increases** in region 3

Water surface

- is **asymptotic** to $y=y_n$
- has a **large angle** with $y=y_c$

Lecture 12: Control Points and Non-uniform flow profiles (review)

1 – Control points:

- **Bed** rise (or hump) - if flow becomes critical $\Delta z \geq \Delta z^*$
- **Channel contraction** - if flow becomes critical ($b < b_c$)
- **Change in the slope from mild to steep**
- **Free overfall** (flow becomes critical to maximize the discharge) (Tutorial 7)

2 - **Normal** depth (i.e. flow is controlled by channel friction).

3 - **Sluice gate**: water depth after the gate $\approx 0.6 \times$ gate opening.

We saw that variations of water depth in channels in **gradually varied flows** can be calculated using:

$$\frac{dy}{dx} = \frac{S_0 - S_f}{1 - Fr^2}$$

We can find out if the water depth increases or decreases using the above equation.

Lecture 12: Water depth in channels and rivers

We have already shown that the energy equation leads to:

$$\frac{dy}{dx} = \frac{S_0 - S_f}{1 - Fr^2}$$

We can numerically integrate the above equation to calculate y at each point. The derivative dy / dx is approximated between two points as $\Delta y / \Delta x$.

$$\frac{\Delta y}{\Delta x} = \left(\frac{S_0 - S_f}{1 - Fr^2} \right)_{mean}$$

where “mean” is the average value between the two points.

- **The Direct Step Method:** Δy is assumed, Δx is calculated.
- **The Standard Step Method:** Δx is assumed, Δy is calculated (iteration required).

Lecture 12: Water depth in channels and rivers

The Direct Step Method:

Δy is assumed, Δx is calculated:

$$\Delta x = \Delta y K_{mean} \quad \text{where} \quad K = \frac{1 - Fr^2}{S_0 - S_f}$$

Procedure: (Discharge is given)

- 1- Start from point 1 where you know the water depth y_1 (**control point**).
For **supercritical** flow, we go from upstream to downstream.
For **subcritical** flow, we go from downstream to upstream.
- 2- Assume a value for y_2 **based on the profile type.**
- 3- $\Delta y = y_2 - y_1$
- 4- Calculate $K_{mean} = (K_1 + K_2) / 2$
- 5- Calculate $\Delta x = \Delta y K_{mean}$
- 6- Repeat from step 2.