

Assignment 2

(Due: 10 October, 2017 by 17:00)

- Q1.** In the system illustrated in Figure 1, a pump is installed in pipe *BC* to provide a flow of 40 L/s to reservoir *C*. Neglecting the velocity head at the junction and the local losses in the pipes, calculate the total head to be generated by pump and the input power assuming an overall efficiency of 60 percent. Also determine the flow rates in pipes *AB* and *BD*. Assume $\nu = 1 \times 10^{-6} \text{ m}^2/\text{s}$.

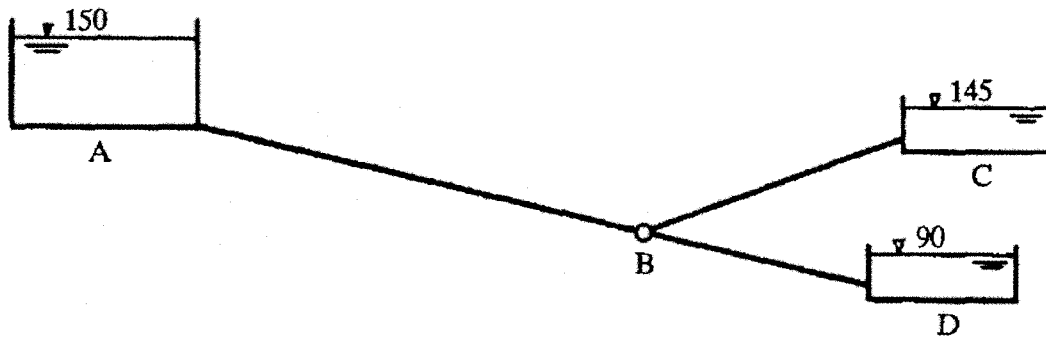


Figure 1

| Pipe | AB | BC | BD |
|----------------|-------|------|------|
| Roughness (mm) | 0.06 | 0.06 | 0.06 |
| Length (m) | 10000 | 4000 | 5000 |
| Diameter (mm) | 400 | 250 | 250 |

Solution:

The flow in pipe *BC* is treated as external outflow of 40 L/s at junction *B*. For the first iteration assume pressure head elevation at junction *B* and calculate flow rates in pipes *AB* and *BD* so that: $q_{AB} - q_{BC} - q_{BD} = 0$ where $q_{BC} = 40 \text{ L/s}$. Continue iterations (with $q_{BC} = 40 \text{ L/s}$) until $\sum_{i=1}^3 q_i = 0$.

Assume: $H_B = 130.00$ m

| Pipe | L (m) | D (m) | ks/D (-) | ΔZ (m) | Initial λ (-) | V (m/s) | Re (-) | Revised λ (-) | Revised V (m/s) | New Re (-) | New λ (-) | q (m ³ /s) | $H_A = 150.00$ m |
|------|----------|----------|-------------|-------------------|--------------------------|------------|-----------|--------------------------|--------------------|---------------|----------------------|--------------------------|--------------------------------|
| AB | 10000 | 0.40 | 1.5E-04 | 20.00 | 0.0130 | 1.101 | 4.40E+05 | 0.0151 | 1.020 | 4.08E+05 | 0.0152 | 0.1282 | $H_C = 145.00$ m |
| BC | 4000 | 0.25 | 2.4E-04 | -15.00 | | | | | | | | -0.0400 | $H_D = 90.00$ m |
| BD | 5000 | 0.25 | 2.4E-04 | -40.00 | 0.0143 | 1.659 | 4.15E+05 | 0.0161 | 1.560 | 3.90E+05 | 0.0162 | -0.0766 | ks = 6.00E-05 m |
| | | | | | | | | | | | | | v = 1.00E-06 m ² /s |
| | | | | | | | | | | | | | $\delta q = 0.0117$ |

Assume: $H_B = 132.00$ m

| Pipe | L (m) | D (m) | ks/D (-) | ΔZ (m) | Initial λ (-) | V (m/s) | Re (-) | Revised λ (-) | Revised V (m/s) | New Re (-) | New λ (-) | q (m ³ /s) | $H_A = 150.00$ m |
|------|----------|----------|-------------|-------------------|--------------------------|------------|-----------|--------------------------|--------------------|---------------|----------------------|--------------------------|--------------------------------|
| AB | 10000 | 0.40 | 1.5E-04 | 18.00 | 0.0130 | 1.044 | 4.18E+05 | 0.0151 | 0.966 | 3.86E+05 | 0.0153 | 0.1214 | $H_C = 145.00$ m |
| BC | 4000 | 0.25 | 2.4E-04 | -13.00 | | | | | | | | -0.0400 | $H_D = 90.00$ m |
| BD | 5000 | 0.25 | 2.4E-04 | -42.00 | 0.0143 | 1.700 | 4.25E+05 | 0.0161 | 1.600 | 4.00E+05 | 0.0162 | -0.0785 | ks = 6.00E-05 m |
| | | | | | | | | | | | | | v = 1.00E-06 m ² /s |
| | | | | | | | | | | | | | $\delta q = 0.002827$ |

Final: $H_B = 132.62$ m

| Pipe | L (m) | D (m) | ks/D (-) | ΔZ (m) | Initial λ (-) | V (m/s) | Re (-) | Revised λ (-) | Revised V (m/s) | New Re (-) | New λ (-) | q (m ³ /s) | $H_A = 150.00$ m |
|------|----------|----------|-------------|-------------------|--------------------------|------------|-----------|--------------------------|--------------------|---------------|----------------------|--------------------------|--------------------------------|
| AB | 10000 | 0.40 | 1.5E-04 | 17.38 | 0.0130 | 1.026 | 4.10E+05 | 0.0152 | 0.948 | 3.79E+05 | 0.0153 | 0.1192 | $H_C = 145.00$ m |
| BC | 4000 | 0.25 | 2.4E-04 | -12.38 | | | | | 0.815 | 2.04E+05 | 0.0172 | -0.0400 | $H_D = 90.00$ m |
| BD | 5000 | 0.25 | 2.4E-04 | -42.62 | 0.0143 | 1.713 | 4.28E+05 | 0.0161 | 1.612 | 4.03E+05 | 0.0162 | -0.0791 | ks = 6.00E-05 m |
| | | | | | | | | | | | | | v = 1.00E-06 m ² /s |
| | | | | | | | | | | | | | $\delta q = 0.000021$ |

∴ The final result is: $H_B = 132.62$ m and flow rates: $q_{AB} = 119.2$ L/s; $q_{BC} = 40$ L/s; $q_{BD} = 79.1$ L/s
 The pump in pipe BC is required to overcome the difference in pressure head elevation between junction B and reservoir C ($\Delta z_{BC} = 12.38$ m) in addition to the frictional head loss along pipe BC.

$$V_{BC} = \frac{q_{BC}}{A_{BC}} = \frac{0.04}{\frac{\pi \times 0.25^2}{4}} = 0.815 \text{ m/s}$$

$$Re(BC) = \frac{V_{BC} \times D_{BC}}{\nu} = \frac{0.815 \times 0.25}{1.0 \times 10^{-6}} = 2.04 \times 10^5$$

From Moody diagram: $\lambda_{BC} = 0.0172$

$$D-W: h_f(BC) = \frac{\lambda_{BC} L_{BC} V_{BC}^2}{2g D_{BC}} = \frac{0.0172 \times 4000 \times 0.815^2}{2 \times 9.81 \times 0.25} = 9.32 \text{ m}$$

$$\text{Required } K_p = A Z_{BC} + h_f(BC) = 12.38 + 9.32 = 21.70 \text{ m}$$

$$P_{out} = \rho g K_p Q_{BC} = 1000 \times 9.81 \times 21.70 \times 0.04 = 8515.08 \text{ W}$$

If overall efficiency is 60%, then $\eta_f = 0.6$

$$P_{in}^{total} = \frac{P_{out}}{\eta_f} = \frac{8515.08}{0.6} = 14191.8 \text{ W} = \underline{\underline{14.19 \text{ kW}}}$$

Q2. Determine the flow rate in the pipes (initial estimated flow rates are provided) and the pressure head elevations at the junctions of the closed-loop pipe network illustrated in Figure 2, neglecting local losses. Water enters the system at junction A from a storage tank (surface elevation of 60.0 m). All pipes have the same roughness size ($k_s = 0.03$ mm) with lengths and diameters provided in the table below. The outflows at the junctions are shown in L/s.

Hint: the solution is iterative. Continue iterations until $\sum h_f < 0.01$ m for each loop.

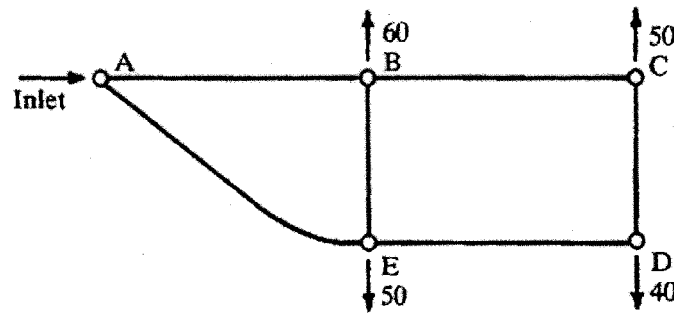
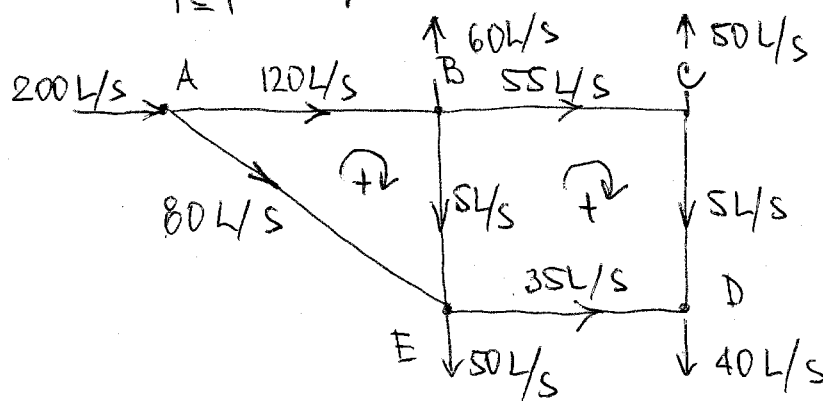


Figure 2

| Pipe | AB | BC | CD | DE | EA | BE |
|---------------|-----|-----|-----|-----|-----|-----|
| Flow (L/s) | 120 | 55 | 5 | 35 | 80 | 5 |
| Length (m) | 500 | 600 | 200 | 600 | 600 | 200 |
| Diameter (mm) | 200 | 150 | 100 | 150 | 200 | 100 |

Solution:

As inflow = outflow for continuity, the inflow at A = $60 + 50 + 50 + 40 = 200$ L/s. Also at each junction, the inflow must be equal to the outflow. With the initial estimated flow rates in the pipes provided and $\sum_{i=1}^n I_i = q$ we obtain:



Analysis is performed by Hardy-Cross method!

* Frictional head losses in pipes calculated from the Darcy-Weisbach equation with friction factor, λ determined from the Moody diagram:

$$D-W: h_f = \frac{\lambda L V^2}{2gD}$$

$$\text{Moody diagram: } \lambda = 0.0055 \left[1 + \left(\frac{20000 k_s}{D} + \frac{10^6}{Re} \right)^{1/3} \right]$$

The first two iterations are given below:

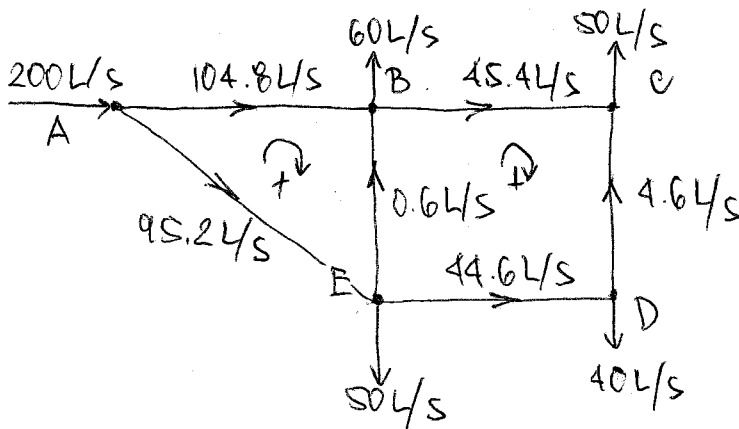
| Pipe | q (m ³ /s) | L (m) | D (m) | ks/D (-) | V (m/s) | Re (-) | λ^* (-) | h_f (m) | h_f/q (-) | new q (m ³ /s) | |
|----------|--------------------------|----------|----------|-------------|------------|-----------|--------------------|--------------|----------------|------------------------------|---|
| AB | 0.120 | 500 | 0.20 | 1.5E-04 | 3.820 | 6.76E+05 | 0.0146 | 27.080 | 225.668 | 0.1089 | ks = 3.00E-05 m v = 1.13E-06 m ² /s |
| BE | 0.005 | 200 | 0.10 | 3.0E-04 | 0.637 | 5.63E+04 | 0.0213 | 0.880 | 176.073 | -0.0061 | |
| EA | -0.080 | 600 | 0.20 | 1.5E-04 | 2.546 | 4.51E+05 | 0.0150 | -14.913 | 186.407 | -0.0911 | |
| Σ | | | | | | | | 13.048 | 588.149 | | |
| | | | | | | | | | | | $\delta q = -0.0111$ |

| Pipe | q (m ³ /s) | L (m) | D (m) | ks/D (-) | V (m/s) | Re (-) | λ^* (-) | h_f (m) | h_f/q (-) | new q (m ³ /s) | |
|----------|--------------------------|----------|----------|-------------|------------|-----------|--------------------|--------------|----------------|------------------------------|---|
| BC | 0.0550 | 600 | 0.15 | 2.0E-04 | 3.112 | 4.13E+05 | 0.0157 | 31.050 | 564.543 | 0.0474 | ks = 3.00E-05 m v = 1.13E-06 m ² /s |
| CD | 0.0050 | 200 | 0.10 | 3.0E-04 | 0.637 | 5.63E+04 | 0.0213 | 0.880 | 176.073 | -0.0026 | |
| DE | -0.0350 | 600 | 0.15 | 2.0E-04 | 1.981 | 2.63E+05 | 0.0164 | -13.123 | 374.949 | -0.0426 | |
| BE | 0.0061 | 200 | 0.10 | 3.0E-04 | 0.776 | 6.86E+04 | 0.0206 | 1.262 | 207.09 | -0.0015 | |
| Σ | | | | | | | | 20.069 | 1322.655 | | |
| | | | | | | | | | | | $\delta q = -0.0076$ |

| Pipe | q (m ³ /s) | L (m) | D (m) | ks/D (-) | V (m/s) | Re (-) | λ^* (-) | h_f (m) | h_f/q (-) | new q (m ³ /s) | |
|----------|--------------------------|----------|----------|-------------|------------|-----------|--------------------|--------------|----------------|------------------------------|---|
| AB | 0.1089 | 500 | 0.20 | 1.5E-04 | 3.467 | 6.14E+05 | 0.0147 | 22.459 | 206.222 | 0.1054 | ks = 3.00E-05 m v = 1.13E-06 m ² /s |
| BE | 0.0015 | 200 | 0.10 | 3.0E-04 | 0.190 | 1.68E+04 | 0.0277 | 0.102 | 68.2915 | -0.0021 | |
| EA | -0.0911 | 600 | 0.20 | 1.5E-04 | 2.900 | 5.13E+05 | 0.0149 | -19.119 | 209.889 | -0.0946 | |
| Σ | | | | | | | | 3.442 | 484.402 | | |
| | | | | | | | | | | | $\delta q = -0.0036$ |

| Pipe | q (m ³ /s) | L (m) | D (m) | ks/D (-) | V (m/s) | Re (-) | λ* (-) | h _f (m) | h _f /q (-) | new q (m ³ /s) | |
|------|--------------------------|----------|----------|-------------|------------|-----------|-----------|-----------------------|--------------------------|------------------------------|---|
| BC | 0.0474 | 600 | 0.15 | 2.0E-04 | 2.683 | 3.56E+05 | 0.0159 | 23.371 | 492.91 | 0.0455 | ks = 3.00E-05 m v = 1.13E-06 m ² /s |
| CD | -0.0026 | 200 | 0.10 | 3.0E-04 | 0.329 | 2.91E+04 | 0.0244 | -0.269 | 104.116 | -0.0045 | |
| DE | -0.0426 | 600 | 0.15 | 2.0E-04 | 2.410 | 3.20E+05 | 0.0161 | -19.044 | 447.176 | -0.0445 | |
| BE | 0.0021 | 200 | 0.10 | 3.0E-04 | 0.262 | 2.32E+04 | 0.0256 | 0.180 | 87.2308 | 0.0002 | |
| Σ | | | | | | | | 4.237 | 1131.433 | | |
| δq = | | | | | | | | -0.0019 | | | |

After further iterations ($\sum h_f < 0.01$ m in any loop), the final flow rates and head losses in the pipes are:



Junction pressure head elevations:

$$H_B = H_A - h_{AB} = 60 - 20.84 = 39.16 \text{ m}$$

$$H_C = H_A - h_{AB} - h_{BC} = 60 - 20.84 - 21.52 = 17.64 \text{ m}$$

$$H_D = H_A - h_{AB} - h_{BC} + h_{CD} = 60 - 20.84 - 21.52 + 0.75 = 18.39 \text{ m}$$

$$H_E = H_A - h_{AE} = 60 - 20.82 = 39.18 \text{ m}$$

Final:

| Pipe | AB | BC | CD | DE | EA | BE |
|--------------------------|--------|--------|--------|--------|--------|--------|
| Flow (m ³ /s) | 0.1048 | 0.0454 | 0.0046 | 0.0446 | 0.0952 | 0.0006 |
| Flow (L/s) | 104.8 | 45.4 | 4.6 | 44.6 | 95.2 | 0.6 |
| Head Loss (m) | 20.84 | 21.52 | 0.75 | 20.79 | 20.82 | 0.02 |

| Junction | A | B | C | D | E |
|------------------------|-------|-------|-------|-------|-------|
| Pr. Head Elevation (m) | 60.00 | 39.16 | 17.64 | 18.39 | 39.18 |