

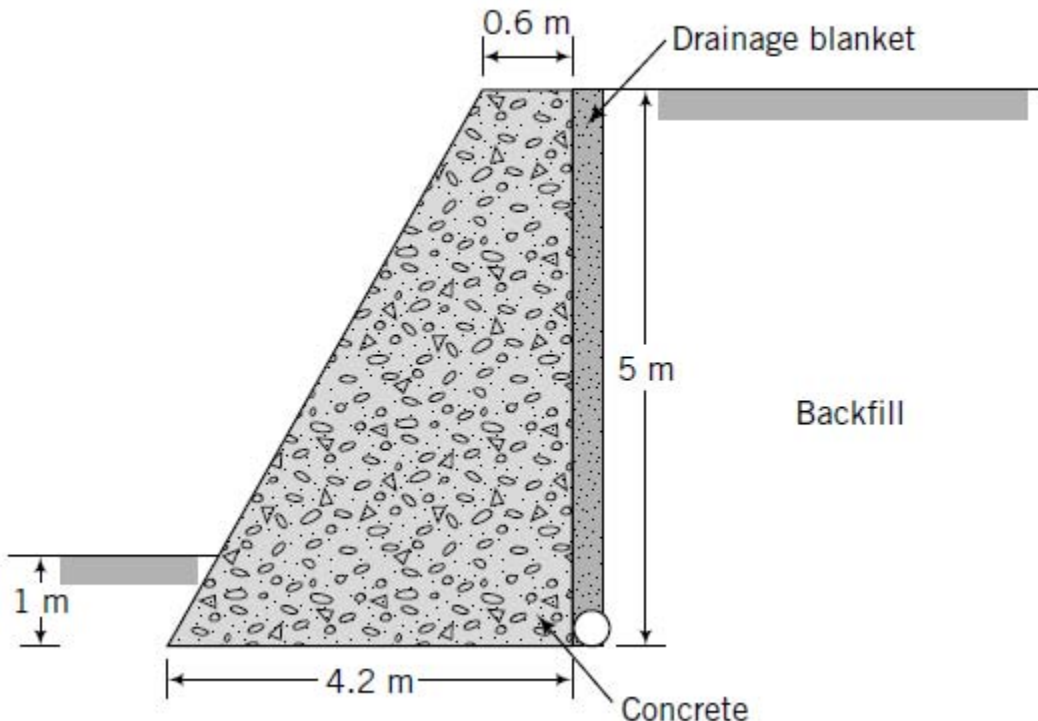
Assignment 4 - Retaining Walls

Question 1

A gravity retaining wall, shown in the figure below, is required to retain 5 m of soil. The backfill is a coarse-grained soil with $\gamma = 18 \text{ kN/m}^3$, $\gamma_{sat} = 19 \text{ kN/m}^3$, $\phi' = 30^\circ$ and $c' = 0$. The existing soil (below the base) has the following properties: $\gamma = 19 \text{ kN/m}^3$, $\gamma_{sat} = 20 \text{ kN/m}^3$, $\phi' = 36^\circ$ and $c' = 0$. The wall is embedded 1 m into the existing soil and a drainage system is provided, as shown. The groundwater level is 4.5 m below the base of the wall. Determine the stability of the wall for the following conditions (assume $k_f = 2/3$ for both base and wall friction):

- Wall friction is zero.
- Wall friction is $\delta' = 2/3\phi'$.
- The drainage system becomes clogged during several days of a rainstorm and the groundwater rises to the surface. Neglect wall friction.

Neglect the passive resistance of the 1.0 m soil above the toe for all cases. The unit weight of concrete is $\gamma_{concr.} = 23.58 \text{ kN/m}^3$.



CVG 3106: Assignment #4

Solution:

a) For zero wall friction, use Rankine's method

$$\phi_1' \text{ (backfill)} = 30^\circ$$

$$K_a = \tan^2 \left(45^\circ - \frac{\phi_1'}{2} \right) = \tan^2 \left(45^\circ - \frac{30^\circ}{2} \right) = 0.33$$

$$P_a = \frac{1}{2} K_a \gamma H^2 = \frac{1}{2} (0.33) (18) (5.0)^2 = 75 \text{ kN/m}$$

P_a is horizontal as the backfill is horizontal and acts at $\frac{H}{3} = \frac{5.0}{3} = 1.67 \text{ m}$ from the base of wall.

Determine the resisting moment:

$$\gamma_{\text{concr.}} = 23.58 \text{ kN/m}^3$$

Section #	Area (m ²)	Weight (kN/m)	Moment arm vs C	Moment (kN.m/m)
1	8.00	70.74	3.9	275.89
2	9.00	212.22	2.4	509.33

$$\Sigma V = 282.96 \text{ kN/m}$$

$$\Sigma M_R = 785.22 \text{ kN.m/m}$$

The overturning moment is:

$$M_o = P_a \left(\frac{H}{3} \right) = 75 \left(\frac{5.0}{3} \right) = 125 \text{ kN.m/m}$$

$$FS \text{ (overturning)} = \frac{\Sigma M_R}{M_o} = \frac{785.22}{125.0} = 6.28 > 2.0, \text{ OK}$$

The passive resistance of the soil above toe is ignored!

$$\delta_{\text{base}}' = k_1 \phi_2' = \frac{2}{3} \times 36 = 24^\circ$$

$$FS \text{ (sliding)} = \frac{(\Sigma V) \tan \delta_{\text{base}}' + B k_2 c_2' + P_p}{P_a}$$

$$FS(\text{sliding}) = \frac{282.96 \tan 24^\circ}{75} = 1.68 > 1.5, \text{ OK}$$

$$M_{\text{net}} = \sum M_R - M_o = 785.22 - 125.0 = 660.22 \text{ kN}\cdot\text{m/m}$$

$$\bar{x} = \frac{M_{\text{net}}}{\sum V} = \frac{660.22}{282.96} = 2.33 \text{ m}$$

$$e = \left| \frac{B}{2} - \bar{x} \right| = \left| \frac{4.2}{2} - 2.33 \right| = 0.23 \text{ m} < \frac{B}{6} = \frac{4.2}{6} = 0.70 \text{ m}$$

The maximum stress occurs at the heel rather than at the toe:

$$q_{\text{max}} = q_{\text{heel}} = \frac{\sum V}{B} \left(1 + \frac{6e}{B} \right) = \frac{282.96}{4.2} \left(1 + \frac{6 \times 0.23}{4.2} \right) = 89.51 \text{ kN/m}^2$$

$$q_{\text{min}} = q_{\text{toe}} = \frac{\sum V}{B} \left(1 - \frac{6e}{B} \right) = \frac{282.96}{4.2} \left(1 - \frac{6 \times 0.23}{4.2} \right) = 45.24 \text{ kN/m}^2$$

$$q_u = c_2' N_o F_{ci} + q N_q F_{qd} F_{qi} + \frac{1}{2} \gamma_2 B' N_\gamma F_{yd} F_{yi}$$

$$q = \gamma_2 D = 19 \times 1.0 = 19 \text{ kN/m}^2$$

GWT @ 4.5m > B = 4.2m → GW has no effect on BC!

$$B' = B - 2e = 4.2 - 2(0.23) = \underline{3.74 \text{ m}}$$

$$\text{for } \phi_2' = 36^\circ \rightarrow N_q = 37.75 \quad N_\gamma = 56.31$$

$$\frac{D_f}{B} = \frac{1.0}{4.2} = 0.24 < 1 \text{ and } \phi_2' = 36^\circ > 0$$

$$F_{qd} = 1 + 2 \tan \phi_2' (1 - \sin \phi_2')^2 \left(\frac{D_f}{B} \right)$$

$$F_{qd} = 1 + 2 \tan 36^\circ (1 - \sin 36^\circ)^2 \left(\frac{1.0}{4.2} \right) = 1.06$$

$$F_{yd} = 1.0$$

$$\psi^o = \tan^{-1} \left(\frac{P_a}{\sum V} \right) = \tan^{-1} \left(\frac{75}{282.96} \right) = 14.8^\circ$$

$$F_{qi} = \left(1 - \frac{\psi^\circ}{90^\circ}\right)^2 = \left(1 - \frac{14.8}{90}\right)^2 = 0.70$$

$$F_{ji} = \left(1 - \frac{\psi^\circ}{\phi_2'}\right)^2 = \left(1 - \frac{14.8}{36^\circ}\right)^2 = 0.35$$

$$q_u = (19)(37.75)(1.06)(0.70) + \frac{1}{2}(19)(3.74)(56.31)(1.0)(0.35) = 1232.44 \text{ kN/m}^2$$

$$FS_{(BC)} = \frac{q_u}{q_{max}} = \frac{1232.44}{89.57} = 13.8 > 3, \text{ OK}$$

b) For wall friction $\delta'_{wall} = \frac{2}{3}\phi_1'$, use Coulomb's method:

For $\alpha = 0^\circ$ (horizontal backfill), $\beta = 90^\circ$ (vertical back face) and $\phi_1' = 30^\circ$ from Table on p. 12 (Lecture notes)

$$K_a = 0.2973 \approx \underline{0.30}$$

$$P_a = \frac{1}{2} K_a \gamma H^2 = \frac{1}{2} (0.30)(18)(5.0)^2 = 67.5 \text{ kN/m}$$

P_a is inclined at an angle $\delta'_{wall} = \frac{2}{3}\phi_1'$ to the horizontal!

$$P_h = P_a \cos\left(\frac{2}{3}\phi_1'\right) = 67.5 \cos\left(\frac{2}{3} \times 30\right) = 63.43 \text{ kN/m}$$

$$P_v = P_a \sin\left(\frac{2}{3}\phi_1'\right) = 67.5 \sin\left(\frac{2}{3} \times 30\right) = 23.09 \text{ kN/m}$$

Determine the resisting moment:

Section #	Area (m ²)	Weight (kN/m)	Moment arm vs C	Moment (kN.m/m)
1	3.00	70.74	3.9	275.89
2	9.00	212.22	2.4	509.33
		$P_v = 23.09$	4.2	96.98

$$\sum V = 306.05 \text{ kN/m}$$

$$\sum M_P = 882.20 \text{ kN.m/m}$$

The overturning moment is:

$$M_o = Ph \left(\frac{H}{3} \right) = 63.43 \left(\frac{5}{3} \right) = 105.72 \text{ kN}\cdot\text{m/m}$$

$$FS (\text{overturning}) = \frac{\sum M_R}{M_o} = \frac{882.20}{105.72} = 8.34 > 2.0, \text{ OK}$$

$$\phi'_{\text{base}} = \kappa_1 \phi_2' = \frac{2}{3} \times 36 = 24^\circ$$

$$FS (\text{sliding}) = \frac{\sum V + \tan \phi'_{\text{base}}}{Ph} = \frac{306.05 + \tan 24^\circ}{63.43} = 2.14 > 1.5, \text{ OK}$$

$$M_{\text{net}} = \sum M_R - M_o = 882.20 - 105.72 = 776.48 \text{ kN}\cdot\text{m/m}$$

$$\bar{x} = \frac{M_{\text{net}}}{\sum V} = \frac{776.48}{306.05} = 2.54 \text{ m}$$

$$e = \left| \frac{B}{2} - \bar{x} \right| = \left| \frac{4.2}{2} - 2.54 \right| = 0.44 \text{ m} < \frac{B}{6} = 0.70 \text{ m}$$

The maximum stress is at the heel!

$$q_{\text{max}} = q_{\text{heel}} = \frac{\sum V}{B} \left(1 + \frac{6e}{B} \right) = \frac{306.05}{4.2} \left(1 + \frac{6 \times 0.44}{4.2} \right) = 118.67 \text{ kN/m}^2$$

$$q_{\text{min}} = q_{\text{toe}} = \frac{\sum V}{B} \left(1 - \frac{6e}{B} \right) = \frac{306.05}{4.2} \left(1 - \frac{6 \times 0.44}{4.2} \right) = 27.07 \text{ kN/m}^2$$

$$q_u = q_r N_q F_{qd} F_{qi} + \frac{1}{2} f_2 B' N_y F_{yd} F_{yi}$$

$$q_r = 19 \text{ kN/m}^2 \text{ (see a.)}$$

$$B' = B - 2e = 4.2 - 2(0.44) = 3.32 \text{ m}$$

$$\left. \begin{array}{l} N_q = 37.75 \\ F_{qd} = 1.06 \end{array} \right\} \begin{array}{l} N_y = 56.31 \\ F_{yd} = 1.0 \end{array} \quad \left\{ \begin{array}{l} \text{From a)} \end{array} \right.$$

$$\psi^\circ = \tan^{-1} \left(\frac{Ph}{\sum V} \right) = \tan^{-1} \left(\frac{63.43}{306.05} \right) = 11.7^\circ$$

$$F_{qi} = \left(1 - \frac{11.7^\circ}{90^\circ} \right)^2 = 0.76$$

$$F_{ji} = \left(1 - \frac{11.7^\circ}{36^\circ}\right)^2 = 0.46$$

$$q_u = (19)(37.75)(1.06)(0.76) + \frac{1}{2}(19)(3.32)(56.31)(1.0)(0.46) = 1394.78 \text{ kN/m}^2$$

$$FS(\text{BC}) = \frac{q_u}{q_{\max}} = \frac{1394.78}{118.67} = 11.75 > 3, \text{ OK}$$

c) GWT @ surface and no wall friction - use Rankine's method!

$$f'_i = \gamma_{\text{sat},1} - \gamma_w = 19 - 9.81 = 9.19 \text{ kN/m}^3$$

$$K_a = 0.33 - \text{From a)}$$

$$P_a = \frac{1}{2} K_a f'_i H^2 + \frac{1}{2} \gamma_w H^2 = \frac{1}{2} (0.33)(9.19)(5.0)^2 + \frac{1}{2} (9.81)(5.0)^2 = 160.53 \text{ kN/m}^2$$

P_a is horizontal and acts at $\frac{H}{3} = 1.67 \text{ m}$ from the base.

$$\Sigma V = 282.96 \text{ kN/m} \quad \left\{ \text{From a)} \right.$$

$$\Sigma M_R = 785.22 \text{ kN}\cdot\text{m/m}$$

The overturning moment is:

$$M_o = P_a \left(\frac{H}{3}\right) = 160.53 \left(\frac{5.0}{3}\right) = 267.55 \text{ kN}\cdot\text{m/m}$$

$$FS(\text{overturning}) = \frac{\Sigma M_R}{M_o} = \frac{785.22}{267.55} = 2.93 > 2.0, \text{ OK}$$

$$\delta'_{\text{base}} = 24^\circ$$

$$FS(\text{sliding}) = \frac{\Sigma V \tan \delta'_{\text{base}}}{P_a} = \frac{282.96 \tan 24^\circ}{160.53} = 0.78 < 1.5 \quad \underline{\text{NOT OK}}$$

$$M_{\text{net}} = \Sigma M_R - M_o = 785.22 - 267.55 = 517.67 \text{ kN}\cdot\text{m/m}$$

$$\bar{x} = \frac{M_{\text{net}}}{\Sigma V} = \frac{517.67}{282.96} = 1.83 \text{ m}$$

$$e = \left| \frac{B}{2} - \bar{x} \right| = \left| \frac{4.2}{2} - 1.83 \right| = 0.27 \text{ m} < \frac{B}{6} = 0.70 \text{ m}$$

The maximum stress occurs at the toe!

$$q_{\max} = q_{\text{toe}} = \frac{\Sigma V}{B} \left(1 + \frac{6e}{B} \right) = \frac{282.96}{4.2} \left(1 + \frac{6 \times 0.27}{4.2} \right) = 93.36 \text{ kN/m}^2$$

$$q_{\min} = q_{\text{heel}} = \frac{\Sigma V}{B} \left(1 - \frac{6e}{B} \right) = \frac{282.96}{4.2} \left(1 - \frac{6 \times 0.27}{4.2} \right) = 41.39 \text{ kN/m}^2$$

$$q_u = q_r N_q F_{qd} F_{qi} + \frac{1}{2} f_2' B' N_f F_{qd} F_{ji}$$

$$q_r = f_2' D = 10.19 \times 1.0 = 10.19 \text{ kN/m}^2$$

$$f_2' = f_{\text{sat},2} - f_w = 20 - 9.81 = 10.19 \text{ kN/m}^3$$

$$B' = B - 2e = 4.2 - 2(0.27) = 3.66 \text{ m}$$

$$\left. \begin{array}{l} N_q = 37.75 \\ F_{qd} = 1.06 \end{array} \right\} \begin{array}{l} N_f = 56.31 \\ F_{jd} = 1.0 \end{array} \quad \left\{ \begin{array}{l} \text{From a)} \end{array} \right.$$

$$\psi^\circ = \tan^{-1} \left(\frac{P_a}{\Sigma V} \right) = \tan^{-1} \left(\frac{160.53}{282.96} \right) = 29.6^\circ$$

$$F_{qi} = \left(1 - \frac{\psi^\circ}{90^\circ} \right)^2 = \left(1 - \frac{29.6}{90} \right)^2 = 0.45$$

$$F_{ji} = \left(1 - \frac{\psi^\circ}{\phi_2'} \right)^2 = \left(1 - \frac{29.6}{36} \right)^2 = 0.03$$

$$q_u = (10.19)(37.75)(1.06)(0.45) + \frac{1}{2} (10.19)(3.66)(56.31)(1.0)(0.03) = 214.99 \text{ kN/m}^2$$

$$FS(BC) = \frac{q_u}{q_{\max}} = \frac{214.99}{93.36} = 2.3 < 3.0, \quad \underline{\text{NOT OK}}$$

