

Solution Assignment #6
Summer 2016

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13.37 / 13.39 / 10.7 / 10.16 / 10.31

13.37

Experimental rocket $M = 25 \text{ kg}$

Tank is tank = $127^\circ\text{C} = T_0$

A converging section with exit area 25 mm^2 is attached to tank, $\dot{m} = 0.05 \text{ kg/s}$

a) $P_{\text{tank}}?$

$A_{\text{ex}} \Rightarrow k = 1.4, R = 287 \text{ J/kgK}$

b) $P_e? T_e? V_e?$

c) Initial acceleration?

a) Since back pressure = 0 \Rightarrow the flow is choked $\Rightarrow P_e = P^*$
 $T_e = T^*$

T_e
 \Rightarrow we know that $\frac{T_0}{T^*} = \frac{k+1}{2} \Rightarrow \boxed{T^* = T_e = 332 \text{ K}}$

V_e
 $\Rightarrow M_e = \frac{V_e}{c_e}$ where $M_e = 1$ since flow choked

$\Rightarrow V_e = c_e = \sqrt{kRT_e} = \sqrt{1.4 \times 287 \times 332} = \boxed{367 \text{ m/s} = V_e}$

P_e
 \Rightarrow we know for ideal gas $\Rightarrow P_e = \rho_e RT_e$

$\rho_e?$ we know $\dot{m} = 0.05 \text{ kg/s} = \rho_e V_e A_e$

$\Rightarrow \rho_e = \frac{\dot{m}}{V_e A_e} = \frac{0.05}{367 \times 25} = 0.0548 \text{ kg/m}^3$

$\Rightarrow P_e = 0.0548 \times 287 \times 332 = \boxed{P_e = 5.21 \text{ kPa}}$

a) $\frac{P_0}{P^*} = \frac{P_0}{P_e} = \left(\frac{k+1}{2}\right)^{\frac{k}{k-1}} = \left(\frac{1.4+1}{2}\right)^{\frac{1.4}{0.4}} \Rightarrow \boxed{9.87 \text{ kPa} = P_0}$

c) $\vec{F} = \int_{\text{surface } P} \vec{a}_{\text{if}} \rho dV = \frac{d}{dt} \int_{\text{CV}} \vec{V}_{xy3} \rho dV + \int_{\text{CS}} \vec{V}_{xy3} \rho \vec{V}_{xy3} \cdot d\vec{A}$ (momentum conservation)

$\Rightarrow P_e A - M a_x = \dot{m} V_e$

$\Rightarrow a_x = \frac{\dot{m} V_e + P_e A}{M} = \boxed{1.25 \text{ m/s}^2 = a_x}$

13.39

(2)

Hydrogen \Rightarrow adiabatically without friction from:

$$P_1 = 100 \text{ psi} \quad \Rightarrow \text{converging-diverging nozzle} \Rightarrow P_2 = 20 \text{ psia}$$

$$T_1 = 540^\circ \text{F}$$

$$V_1 = 0 \quad M_2 = ?$$

For Hydrogen $k = 1.41$

$$T_0 = 540^\circ \text{F} = 1000^\circ \text{R}$$

$$R = 766.7 \frac{\text{ft} \cdot \text{lb}}{\text{lbm} \cdot \text{R}} \Rightarrow \text{convert } T_0$$

$$\Rightarrow \text{we know that } \frac{P_0}{P} = \left(1 + \frac{k-1}{2} M^2\right)^{\frac{k}{k-1}}$$

$$M_2 = \sqrt{\frac{2}{k-1} \left(\frac{P_0}{P_2}\right)^{\frac{k-1}{k}} - 1} \Rightarrow M_2 = 1.71$$

10.7

Dimensions of centrifugal pump impeller:

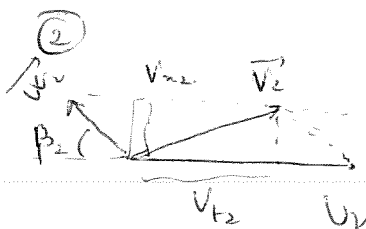
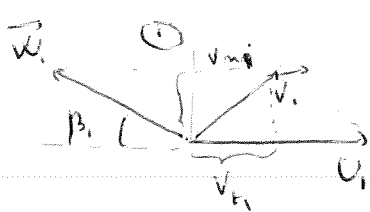
	①	②
r	15 in	45 in
b	4.75 in	3.25 in
β	40°	60°

 $\omega = 575 \text{ rpm}$, watercalculate H? and \dot{W}_m ? if $Q = 80000 \text{ gpm}$

$$\text{we know: } \dot{W}_m = (U_2 V_{t2} - U_1 V_{t1}) \dot{m}$$

$$H = \frac{\dot{W}_m}{\dot{m}g} = \frac{1}{g} (U_2 V_{t2} - U_1 V_{t1})$$

Using the velocity diagrams:



$$V_m = \frac{Q}{2\pi r b} \quad (\text{continuity}) \Rightarrow Q = 2\pi r b \times V_m$$

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geometry: $\vec{W} = \vec{V} + \vec{U}$

$$\left. \begin{aligned} U - V_E &= W \cos \beta \\ V_m &= W \sin \beta \end{aligned} \right\} \Rightarrow \frac{U - V_E}{V_m} = \cot \beta$$

$$\Rightarrow V_E = -\cot \beta \times V_m + U$$

$$V_E = -\frac{Q}{2\pi r b} \cot \beta + U$$

we know $U = r\omega \Rightarrow$ when $\omega = 575 \text{ rpm} = 60.21 \text{ rad/s}$

$$U_1 = 77.3 \text{ ft/s} \quad U_2 = 226 \text{ ft/s}$$

$$Q = 178 \text{ ft}^3/\text{s} \Rightarrow \text{flow} (80000 \text{ gpm})$$

$$\Rightarrow V_{E1} = 6.94 \text{ ft/s}$$

$$V_{E2} = 210 \text{ ft/s}$$

$$\Rightarrow \dot{W}_m = (U_2 V_{E2} - U_1 V_{E1}) \rho Q \approx P_{water} = 1.94 \text{ slug/ft}^3$$

$$\Rightarrow \dot{W}_m = 1.62 \cdot 10^4 \frac{\text{ft} \cdot \text{lb} \cdot \text{ft}}{\text{s}} = 2.94 \cdot 10^4 \text{ hp}$$

$$H = \frac{\dot{W}_m}{\dot{m} g} = 1455 \text{ ft}$$

10.16.

$\omega = 1200 \text{ rpm}$ centrifugal pump

①

②

radius	90 mm	170 mm
h	10 mm	7.5 mm
β	25°	45°

a) Q ? when $V_E = 0$

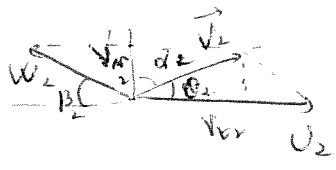
b) Draw outlet velocity diagram? outlet absolute flow angle?

c) \dot{W}_R if $\eta = 0.7$? and H ?

$$\dot{W}_m = (U_2 V_{t2} - U_1 V_{t1}) \dot{m}$$

$$H = \frac{\dot{W}_m}{\dot{m} g} = \frac{1}{g} (U_2 V_{t2} - U_1 V_{t1})$$

a) ②



continuity: $Q = V_m \times 2\pi r b = V_m = \frac{Q}{2\pi r b}$

$$\left. \begin{aligned} U - V_t &= W \cos \beta \\ V_m &= W \sin \beta \end{aligned} \right\} \Rightarrow V_t = U - V_m \cot \beta$$

For ① $\Rightarrow V_{t1} = 0 \Rightarrow U_1 - V_{m1} \cot \beta_1 = 0$

$$\Rightarrow U_1 = \frac{Q}{2\pi r_1 b_1} \cot \beta_1 = 0 \Rightarrow Q = 2\pi r_1 b_1 U_1 \tan \beta_1$$

$$Q = \frac{U_1 \times 2\pi r_1 b_1}{\cot(\beta_1)} = r_1 \omega \times 2\pi r_1 b_1 \tan(\beta_1)$$

$\omega = 1200 \text{ rpm} = 125,66 \text{ rad/s}$

$$\Rightarrow Q = 29810^{-2} \text{ m}^3/\text{s}$$

b) $\alpha_2 = \text{tg}^{-1} \left(\frac{V_{t2}}{V_{m2}} \right)$

$$V_{m2} = \frac{Q}{2\pi r_2 b_2} = 4,22 \text{ m/s}$$

$$V_{t2} = U_2 - V_{m2} \cot(\beta_2) = r_2 \omega - V_{m2} \cot(\beta_2) = 14,6 \text{ m/s}$$

$$\Rightarrow \alpha_2 = \text{tg}^{-1} \left(\frac{14,6}{4,22} \right) = \boxed{73,9^\circ = \alpha_2}$$

$$\dot{W}_m = (U_2 V_{t_2} - U_1 V_{t_1}) \rho Q = U_2 V_{t_2} \rho Q \quad \frac{1}{m^3} \text{ water}$$

$$\Rightarrow \dot{W}_m = 8,22 \cdot 10^3 \text{ W}$$

we know $\frac{\dot{W}_R}{\dot{W}_m} = \eta \Rightarrow \dot{W}_R = \eta \dot{W}_m = 0,7 \times 8,22 \cdot 10^3 = 5,75 \cdot 10^3 \text{ W} = \dot{W}_R$

$$H = \frac{1}{g} (U_2 V_{t_2}) = 28,1 \text{ m}$$

$$\eta = \frac{H_p}{H} \Rightarrow H_p = H \times \eta = 28,1 \times 0,7 = H_p = 19,7 \text{ m}$$

10.31

small centrifugal pump $N = 2875 \text{ rpm} \Rightarrow \omega = \text{rad/s}$ with water

$Q = 0,016 \text{ m}^3/\text{s}$ and $H = 40 \text{ m}$ at its best efficiency $\eta = 0,7$

a) N_s ? Sketch?

b) \dot{W}_m ?

a) $N_s = \frac{\omega Q^{1/2}}{g H^{3/4}}$ where $h = g H$ $\omega = 2875 \text{ rpm} = 301,07 \text{ rad/s}$

$$N_s = \frac{\omega Q^{1/2}}{g H^{3/4}} = 0,432 = N_s$$

\therefore impeller will be centrifugal

b) \dot{W}_m ?

$$\eta = \frac{\dot{W}_R}{\dot{W}_m} \Rightarrow \dot{W}_m = \frac{\dot{W}_R}{\eta} = \frac{\rho Q g H}{\eta} \quad \rho_{\text{water}} = 1000 \text{ kg/m}^3$$

$$\Rightarrow \dot{W}_m = 8,97 \cdot 10^3 \text{ W}$$

