

Solution Assignment #4

Summer 2016

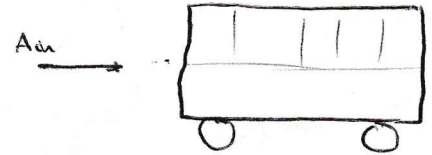
①

9,112 / # 9,125 / # 9,165 / x fact

9,112

A bus travel at 80 km/hr in Standard air.

$$A_{\text{frontal}} = 7,5 \text{ m}^2 \quad C_D = 0,92$$



a) Power to overcome drag ?

b) Maximum speed of bus if engine is rated at 465 hp

Add fairings on Front and rear of bus to reduce drag $\Rightarrow C_D$ reduces to 0,86 without changing ~~A~~ ~~frontal~~ frontal.

c) Required Power at 80 km/hr and at new top speed

d) if fuel cost is \$300/day \Rightarrow \$4800 to install. How long it would take for the modifications to pay for itself

a) We know $V = 80 \text{ km/hr} = 22,2 \text{ m/s}$

Let's estimate the drag force based on $C_D \Rightarrow C_D = \frac{F_D}{\frac{1}{2} \rho V^2 A}$

$$\Rightarrow F_D = \frac{1}{2} C_D \rho V^2 A$$

at standard air conditions: $\rho = 1,23 \text{ kg/m}^3$

$$\Rightarrow F_D = 0,5 \times 0,92 \times 1,23 \times (22,2)^2 \times 7,5 = 2091,36 \text{ N}$$

$$\Rightarrow \text{Power to overcome drag} \Rightarrow P = F_D \times V = 2091,36 \times 22,2 \Rightarrow \boxed{P = 46,42 \text{ kW}}$$

b) $P_{\text{max}} = 465 \text{ Hp} \times 745,7 \frac{\text{W}}{\text{Hp}} = 346,75 \text{ kW}$

$$\Rightarrow P_{\text{max}} = F_{D_{\text{max}}} \times V_{\text{max}} = \frac{1}{2} C_D \rho V_{\text{max}}^2 A \times V_{\text{max}} = \frac{1}{2} C_D \rho A V_{\text{max}}^3$$

$$\Rightarrow V_{\text{max}} = \sqrt[3]{\frac{P_{\text{max}}}{\frac{1}{2} C_D \rho A}} \Rightarrow V_{\text{max}} = \sqrt[3]{\frac{346,75 \cdot 10^3}{0,5 \times 0,92 \times 1,23 \times 7,5}} \Rightarrow \boxed{V_{\text{max}} = 43,39 \text{ m/s}}$$

c) Now $C_{D_{new}} = 0,86$ without changing $A_{frontal}$

$$F_{D_{new}} = \frac{1}{2} C_{D_{new}} \rho V^2 A = 0,5 \times 0,86 \times 1,23 \times (22,2)^2 \times 7,5$$

$$\Rightarrow F_{D_{new}} = 1954,97 \text{ N}$$

$$\Rightarrow \text{Power}_{new} = F_{D_{new}} \times V = 1954,97 \times 22,2 \Rightarrow \boxed{\text{Power}_{new} = 43,4 \text{ kW}}$$

$$\text{Power}_{Max} = F_{D_{Max}} \times V_{Max} = 0,5 \times C_{D_{new}} \times \rho \times V_{Max}^2 \times A \times V_{Max}$$
$$= 0,5 \times C_{D_{new}} \times \rho \times V_{Max}^3 \times A$$

$$\Rightarrow V_{Max_{new}} = \sqrt[3]{\frac{\text{Power}_{Max}}{0,5 \times C_{D_{new}} \times \rho \times A}} = \sqrt[3]{\frac{346,4 \times 10^3}{0,5 \times 0,86 \times 1,23 \times 7,5}} = 44,38 \text{ m/s}$$

$$\boxed{V_{Max_{new}} = 44,38 \text{ m/s}}$$

d) The fairings cost \$4800 to install and Fuel cost = $\frac{\$300}{\text{day}}$

Let's see how much saving we have because of the fairings

$$\text{Power gain} = \frac{\text{Power}_{new}}{P} = \frac{43,4 \times 10^3}{46,42 \times 10^3} = 93,49 \approx 93,5\%$$

$$\Rightarrow \text{The new cost per day} \Rightarrow \text{New cost/day} = \text{Power gain} \times \text{Fuel cost} = 0,935 \times 300$$

$$\text{New cost/day} = \frac{\$280,5}{\text{day}}$$

$$\Rightarrow \text{Savings} = \text{Fuel cost} - \frac{\text{New cost}}{\text{day}} = 300 - 280,5 = \$19,5/\text{day}$$

$$\text{time} = \frac{\text{Initial cost}}{\text{savings}} = \frac{\$4800}{\$19,5/\text{day}} = \boxed{246,153 \text{ days} = \text{time}} \approx 8,2 \text{ months}$$

9.12T

(3)

Runner maintains a speed of 7.5 mph during a 4 mile run

2 miles straight then turn around and return home for 2 miles.

$C_D A = 9 \text{ ft}^2$ for the runner

a) on a windless day, how many calories in kcal will the runner burn overcoming drag

b) if wind is blowing 5 mph directly along the runner's route, how many calories burn to overcome drag.

a) $V_{\text{wind}} = 0 \text{ mph}$

$V_{\text{runner}} = 7.5 \text{ mph}$, Runner in air $\Rightarrow \rho_{\text{air}} = 0.002377 \text{ slug/ft}^3$

Calories burned = Energy \approx Energy = Power \times time

$$V = \frac{\text{distance}}{\text{time}} \Rightarrow \text{time} = \frac{\text{distance}}{V} = \frac{4 \text{ miles}}{7.5 \text{ mph}} = 0.533 \text{ h} = 0.533 \times \frac{3600 \text{ s}}{\text{h}} = 1920 \text{ s}$$

$$\text{Power} = F_D \times V$$

$$C_D = \frac{F_D}{\frac{1}{2} \rho V^2 A} \Rightarrow F_D = \frac{1}{2} \rho V^2 A \times C_D \quad \text{given}$$

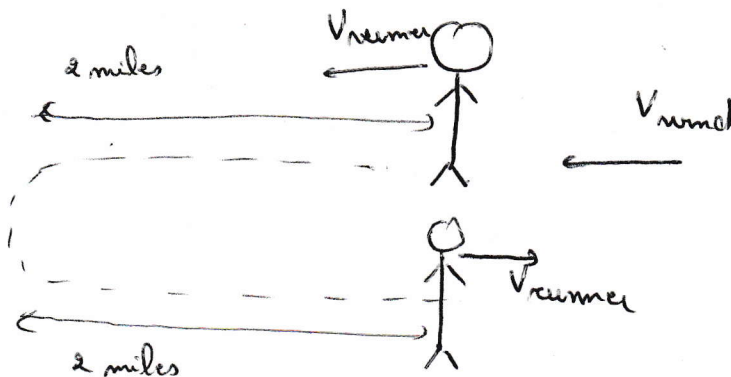
$$\Rightarrow F_D = 1,294 \text{ lbf}$$

$$\Rightarrow \text{Power} = 1,294 \times 11 = 14,237 \frac{\text{lbf} \cdot \text{ft}}{\text{s}}$$

$$\Rightarrow \text{Energy (in kcal)} = \text{Power} \times \text{time} = 14,237 \times 1920 \frac{\text{lbf} \cdot \text{ft}}{\text{s}} \times \frac{1}{5} \times \frac{0.0003238 \text{ kcal}}{\text{ft} \cdot \text{lbf}}$$

$$\Rightarrow \boxed{\text{Energy (kcal)} = 8,86 \text{ kcal}}$$

b) $V_{\text{wind}} = 5 \text{ mph}$



① For the first 2 miles \Rightarrow the relative velocity $V_{rel} = V_{runner} + V_{wind} =$
 $\Rightarrow V_{rel} = 7.5 + 5 = 12.5 \text{ mph} = 18.33 \text{ ft/s}$

② For the next 2 miles $\Rightarrow V_{rel} = 7.5 - 5 = 2.5 \text{ mph} = 3.667 \text{ ft/s}$

① $time = \frac{2 \text{ miles}}{7.5 \text{ mph}} = 960 \text{ s}$

$\Rightarrow Energy_{\text{①}} = Power \times time$
 $= F_D \times V \times time$
 $= \frac{1}{2} C_D \times V^2 \times A \times \rho \times V \times time = 0.7 \times 9 \times (18.33)^2 \times 18.33 \times \frac{\text{kcal/ft} \cdot \text{lb}}{0.0003238} \times 960 \times 0.00238$

$\Rightarrow Energy_{\text{①}} = 12.3 \text{ kcal}$

② $time = 960 \text{ s}$

$\Rightarrow Energy_{\text{②}} = \frac{1}{2} C_D V^2 \times A \times \rho \times V \times time = 0.7 \times 9 \times (3.667)^2 \times 0.0003238 \times 960 \times 0.00238$

$\Rightarrow Energy_{\text{②}} = 0.49 \text{ kcal}$

$\Rightarrow Total \ Energy = Energy_{\text{①}} + Energy_{\text{②}} = 12.3 + 0.49 = \boxed{12.79 \text{ kcal} = Energy \ total}$

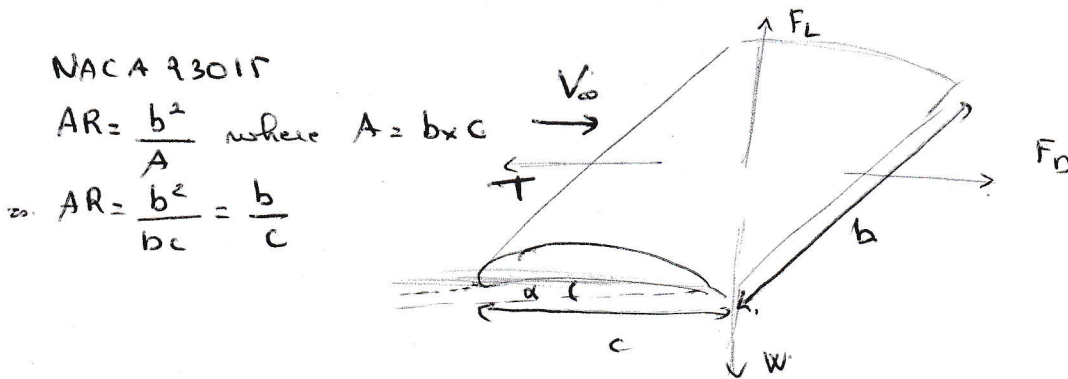
9.165

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Design of airplane

Evaluate the maximum total payload and required power to maintain flight, if sheet of plastic is replaced by NACA 23015 with same AR and angle of attack as in (9.163)

To maintain the flight \Rightarrow Thrust = F_D
Weight = Lift



From 9.163: $b = \sqrt{A_{9.163}} = 7 \text{ ft}$ and $c = L_{9.163} = 5 \text{ ft}$

Angle of attack $\alpha = 10^\circ$, $V = 40 \text{ ft/s}$

* Payload $\Rightarrow M$? since $W = F_L \Rightarrow M \times g = F_L$

we know: $C_L = \frac{F_L}{\frac{1}{2} \rho V^2 A} \Rightarrow F_L = \frac{1}{2} C_L \rho V^2 A$

~~Table~~ Figure 9.17 in the book \Rightarrow for $\alpha = 10^\circ \Rightarrow C_L = 1.2$ and $C_{Di} = 0.01$

Assume standard conditions for air $\Rightarrow \rho_{air} = 0.00234 \frac{\text{slug}}{\text{ft}^3}$

$$\Rightarrow M = \frac{F_L}{g} = \frac{0.5 \times 1.2 \times 0.00234 \times (40)^2 \times 7 \times 5}{32.2} = \frac{78.624}{32.2} = 2.44 \text{ slug} = \boxed{78.624 \text{ lb} = M}$$

* Power required $\Rightarrow P = \text{Thrust} \times V$, $C_D = \frac{F_D}{\frac{1}{2} \rho V^2 A}$

we know $T = F_D \Rightarrow T = \frac{1}{2} \rho V^2 A C_D$

For a wing, the drag coefficient can be found using $C_D = C_{Di} + \frac{C_L^2}{\pi AR}$

$$\Rightarrow C_D = 0.01 + \frac{1.2^2}{\pi \times \frac{7}{5}} = 0.337$$

$$T = 0,5 \times 0,00234 \times (40)^2 \times 7 \times 5 \times 0,337 = 22,08 \text{ lbf}$$

$$\text{Power} = T \times V = 22,08 \times 40 = 883,2 \frac{\text{lbf ft}}{\text{s}} = \text{Power} \Rightarrow \text{Power} = 1,605 \text{ hp}$$

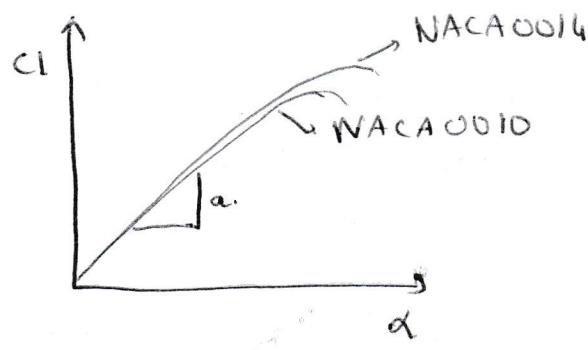
X-foil

C_L was calculated for 3 different NACA airfoils \Rightarrow NACA 0006 \Rightarrow 6% thickness
 \Rightarrow NACA 0010 \Rightarrow 10% "
 \Rightarrow NACA 0014 \Rightarrow 14% thickness

These airfoils are not cambered, they are symmetrical.

* Fig 1. $\Rightarrow C_L$ vs. α . (see page 9)
 angle of attack

- The results were generated for $Re = 10^6$



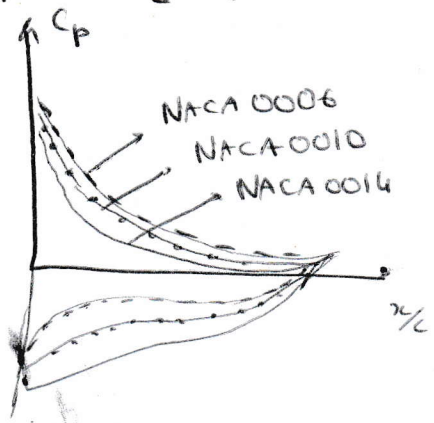
$\Rightarrow \alpha \approx 2\pi$ for all airfoils until reaching a critical angle of attack where C_L decreases.

- we noticed that ~~the~~ for the same angle of attack the airfoils with higher thicknesses ~~have~~ have higher lift coefficients.

- The same analysis can be performed with cambered airfoils with comparable thicknesses (NACA 2406, NACA 2410 and NACA 2414) \Rightarrow Max camber 2% at 40% of chord.

- it was found that cambered airfoils have higher lift coefficients for the same angles of attack \Rightarrow this shows the importance of the airfoil camber.

* Fig 2. $\Rightarrow C_p$ vs. $\frac{x}{c}$ (using the same Re) for angle of attack at $2^\circ = \alpha$

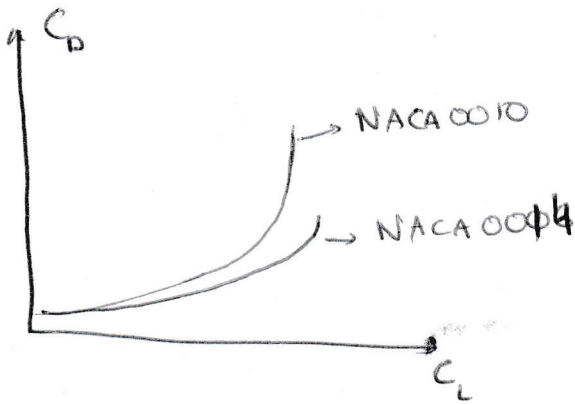


$$C_p = \frac{P - P_\infty}{\frac{1}{2} \rho V_\infty^2}$$

- We noticed that the pressure coefficient tend to decrease on the top of the airfoil ~~the~~ for larger thicknesses, which explains the higher C_L

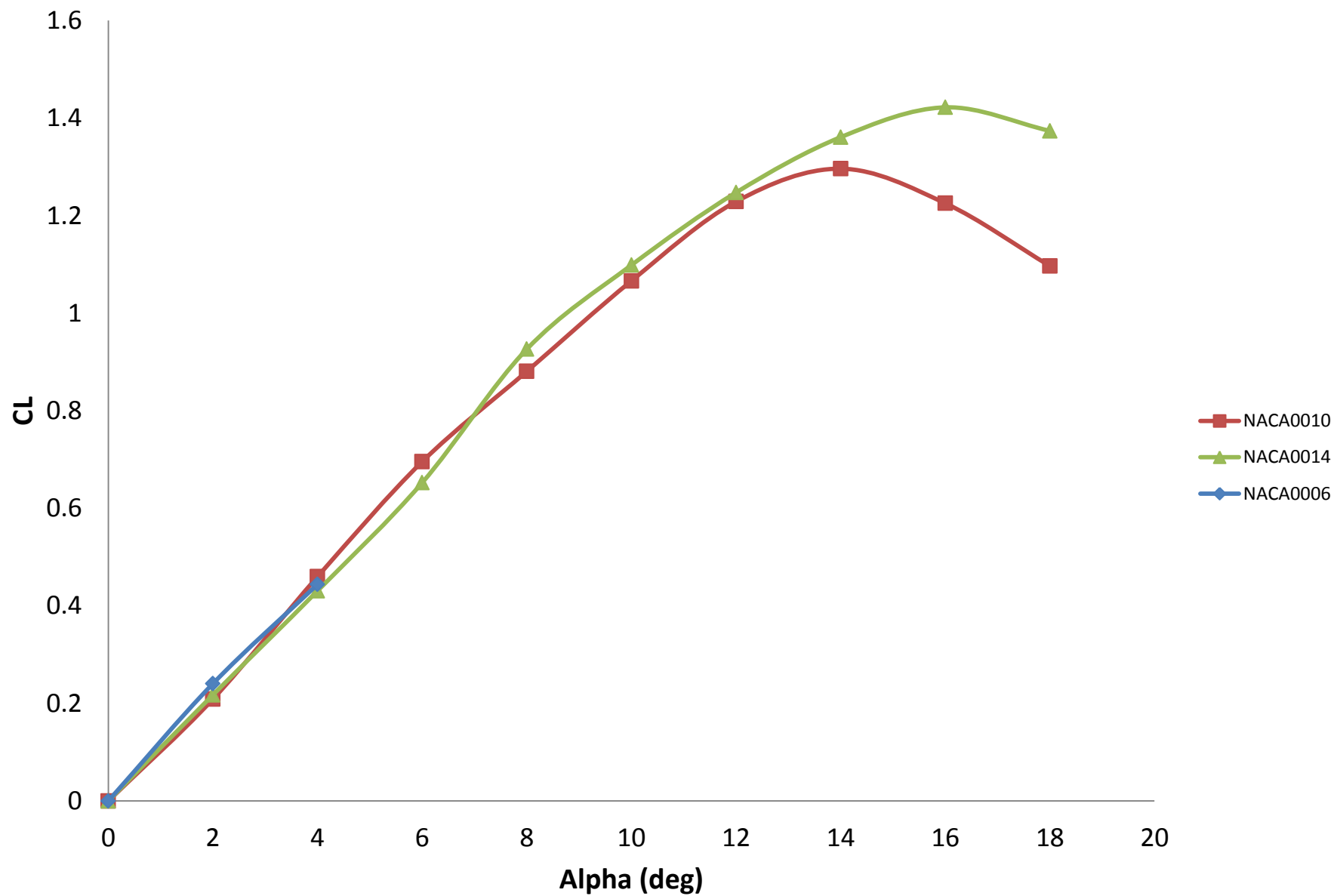
* Fig 3. C_L vs. C_D (for the same Re)

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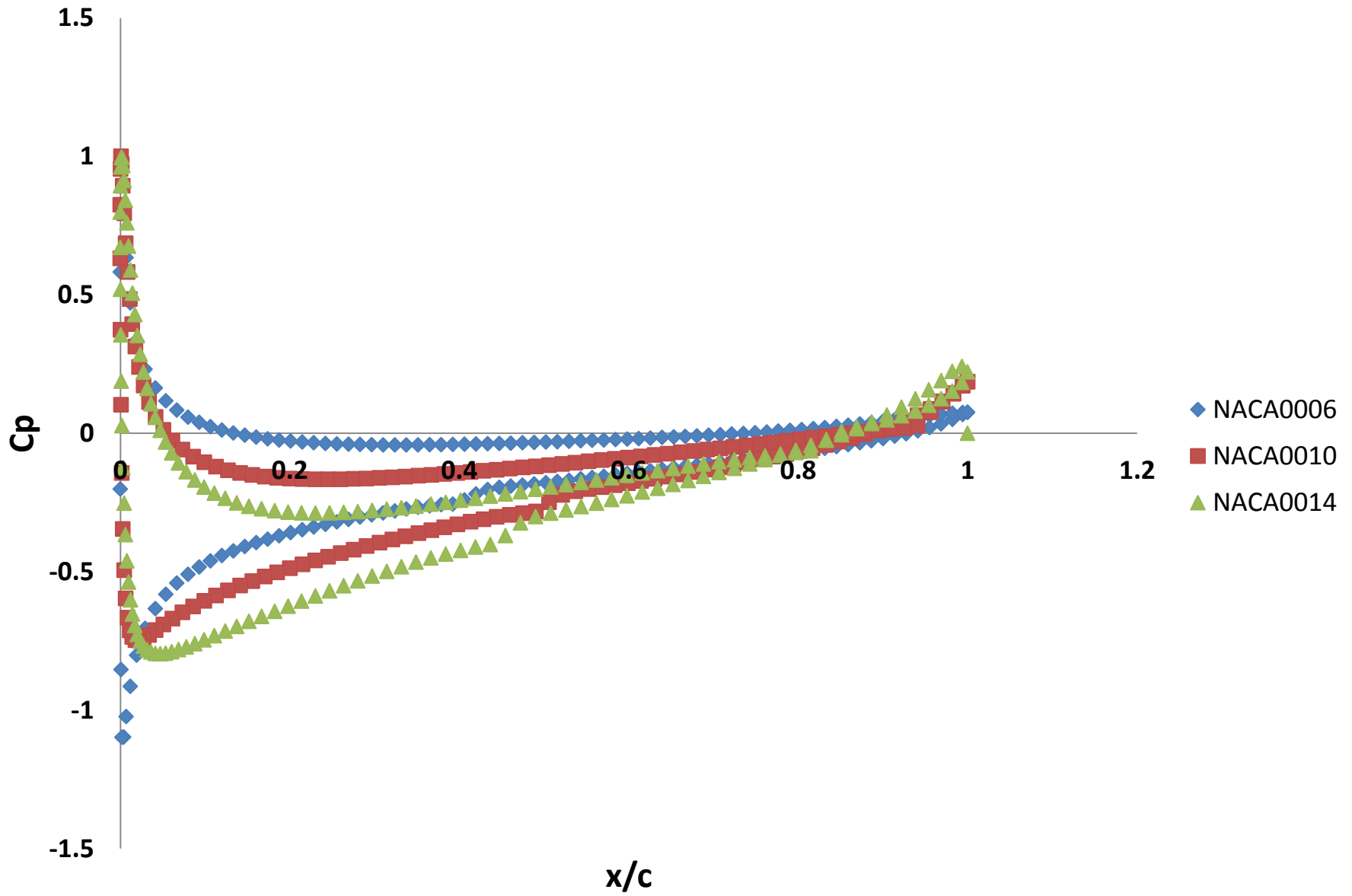


→ This figure shows that the larger lift coefficients are obtained for smaller drag coefficients with the airfoil ~~is~~ NACA 0014 (the larger thickness) compared to NACA 0010, which is preferred.

CL vs. alpha



Cp vs. x/c



CD vs. CL

