

Concordia University
Department of Electrical and
Computer Engineering

ELEC-331

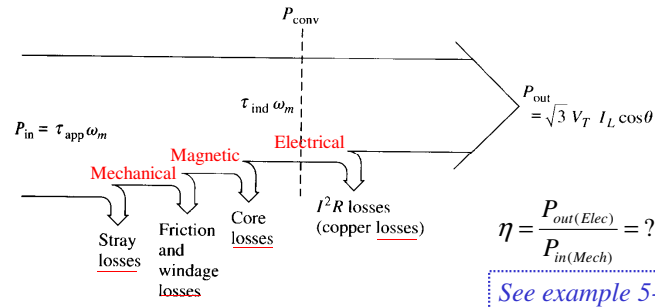
Lecture 9

Synchronous generators (5.6-5.9) and
motors (6.1-6.2)

Outline of the lecture

- Power & torque in synchronous generators
- Measuring SG parameters
- Frequency and voltage control of SG
- Effects of load variations (voltage regulation) for isolated generators.
- Frequency and active power characteristics
- Voltage and reactive power characteristics
- Parallel operation with infinite bus with control of P_{inj} and of Q_{inj} .

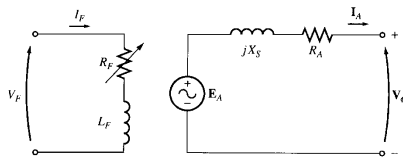
Power & torque in sync. generators



$P = \tau \omega$
 $P_{conv} = \tau_{ind} \omega = 3E_A I_A \cos \gamma, \quad \gamma = \angle E_A - \angle I_A$
Electrical side.

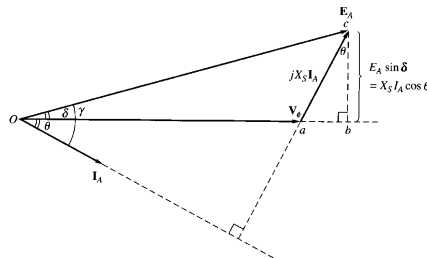
$P_{out} = P_{conv} - P_{cu} = 3V_\phi I_A \cos \theta, \quad \theta = \angle V_\phi - \angle I_A$
Recall the model...

Power & torque in sync. generators



Neglecting R_A :

$$V_\phi = E_A - jX_S I_A$$



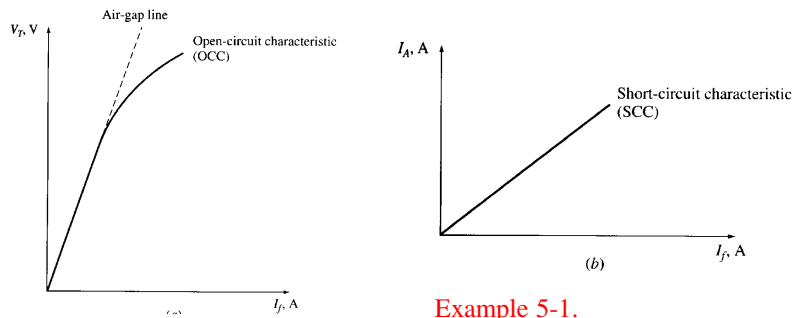
$$P_{out} = 3V_\phi I_A \cos \phi = \frac{3V_\phi E_A \sin \delta}{X_S}$$

where, $\delta = \angle E_A - \angle V_\phi$ (power angle)

- Speed (and frequency) is assumed to be constant. **What happens to δ when P_{out} increases while E_A and V_ϕ remain constant?**

Measuring SG parameters

- Main parameters: $I_F \times E_A$ relationship, X_S and R_A .
- Open-circuit test $\rightarrow E_A = V_T$.
- Short-circuit test $\rightarrow Z_S = \sqrt{R_A^2 + X_S^2} = \frac{V_{\phi,oc}}{I_A}$ $X_S \cong \frac{V_{\phi,oc}}{I_A}$
- DC voltage test in a **Y-connected** armature (stator) $\rightarrow 2R_A = \frac{V_{DC}}{I_{DC}}$



Example 5-1.

Frequency and voltage control/regulation of synchronous generators

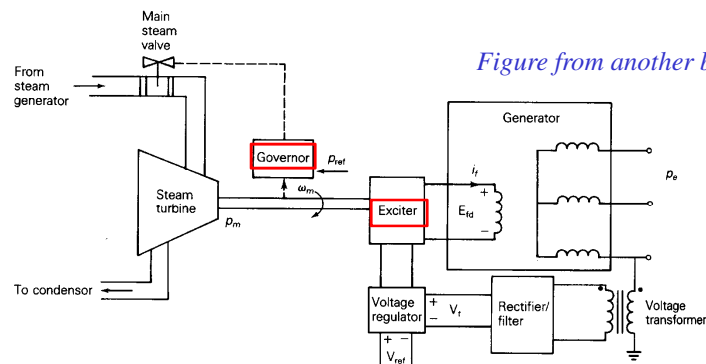


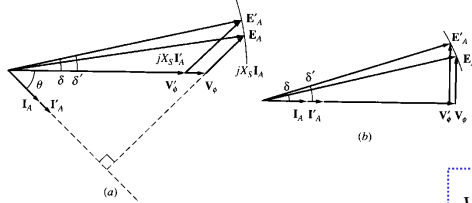
Figure from another book.

Figure 11.1 Voltage regulator and turbine-governor controls for a steam-turbine generator

The **Governor** increases the flow of steam to increase the shaft speed.
 The **Exciter** increases i_f to increase the output voltage of the generator.

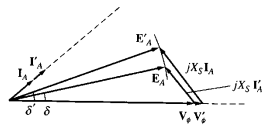
Effects of the load on a synchronous generator operating alone (*islanded*)

- For E_A constant, if the load (current) changes, the voltage drop across X_S and V_ϕ also change $\rightarrow V_\phi = E_A - jX_S I_A$



What about the power angle (δ)?

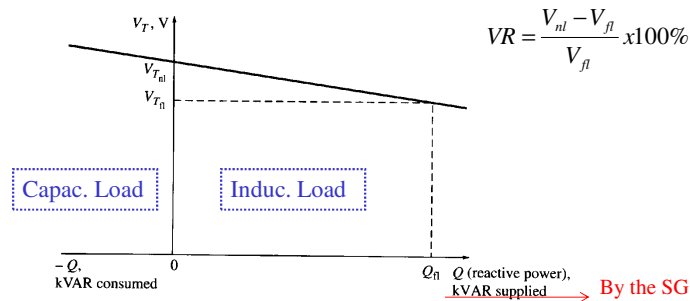
$$VR = \frac{V_{nl} - V_{fl}}{V_{fl}} \times 100\%$$



- How can V_ϕ be regulated? By varying I_F . *Ex. 5-2 & tutorial*

Voltage x reactive power characteristics

- Represents the effect of the demanded reactive power on the voltage terminal. Inductive loads have positive while capacitive have negative VR

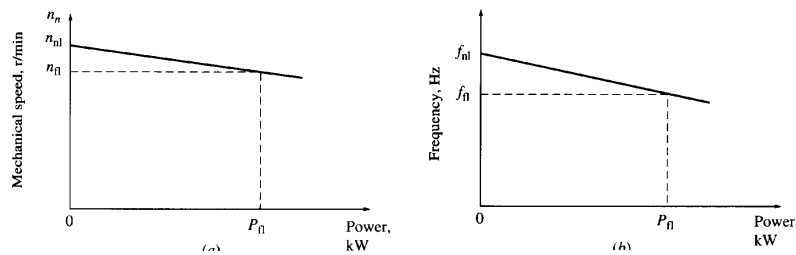


$$VR = \frac{V_{nl} - V_{fl}}{V_{fl}} \times 100\%$$

Frequency x active power characteristics

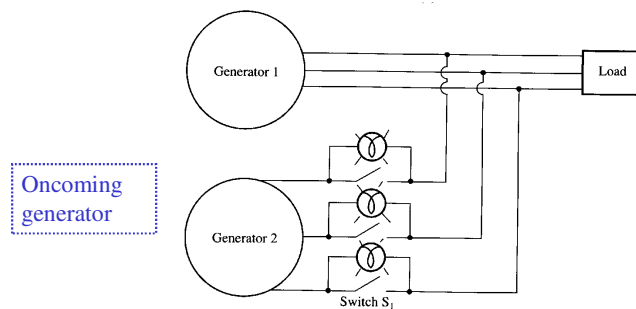
- Load (**active power**) variations result in small frequency variations due to a governor's action (droop factor/control)
- “Droop control” facilitates the operation of generators (of similar size) in parallel. (See example 5.6!)

$$SD = \frac{n_{nl} - n_{fl}}{n_{fl}} \approx 3\% \quad f_e = \frac{n_m P}{120} \quad P = sp(f_{nl} - f_{sys}), sp(\text{kW/Hz})$$



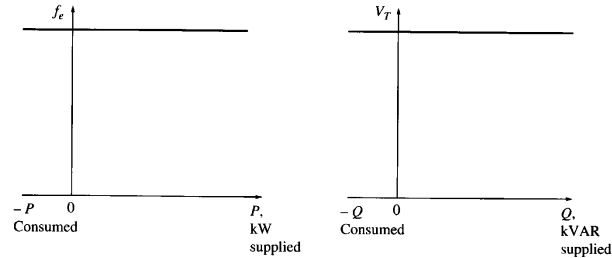
Parallel operation of AC generators

- Conditions: 1) Equal voltage level, 2) phase sequence and 3) phase angle and frequency (after connection).
- Detecting phase sequence and when the voltages of the 2 generators are in-phase...



Parallel operation with an infinite bus

- An infinite bus has a flat frequency and voltage profiles.
- It can consume or supply any amount of P and Q.
- The speed of a SG connected to an infinite bus is fixed.



- P_{inj} is controlled by the governor (P_{Mec})

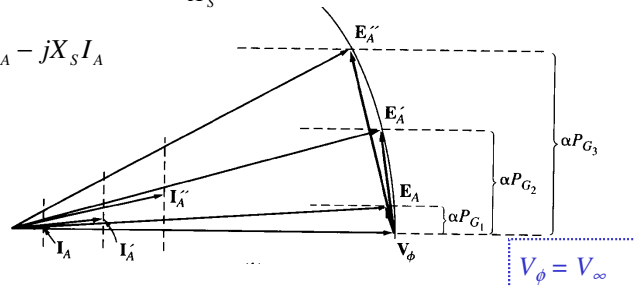
$$P_{inj} = P_{Mec} - P_{losses}, \quad P_{inj} = \frac{3E_A V_\infty \sin \delta}{X_S}, \quad \delta = \angle E_A - \angle V_\infty, (V_\infty = V_\phi)$$

Varying the injected active power (P_{inj})

- P_{inj} is controlled by the governor's set point (P_{Mec})

$$P_{inj} = P_{Mec} - P_{losses} \quad P_{inj} = \frac{3E_A V_\infty \sin \delta}{X_S}, \quad \delta = \angle E_A - \angle V_\infty, (V_\infty = V_\phi)$$

$$V_\phi = E_A - jX_S I_A$$

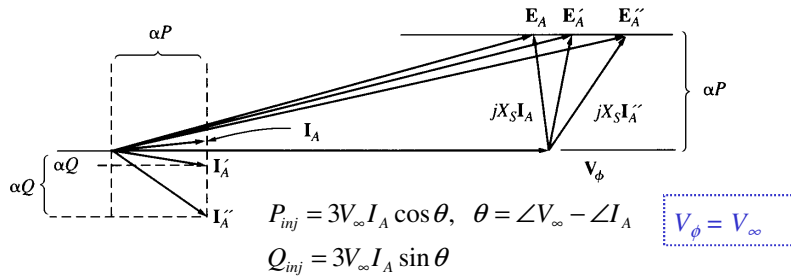


- $\delta \uparrow$. Since $E_A = \text{const}$, Q also $\uparrow Q = 3V_\infty I_A \sin \theta$, $\theta = \angle V_\phi - \angle I_A$

In this case, the generator now supplies or absorbs Q?

Varying the injected reactive power (Q)

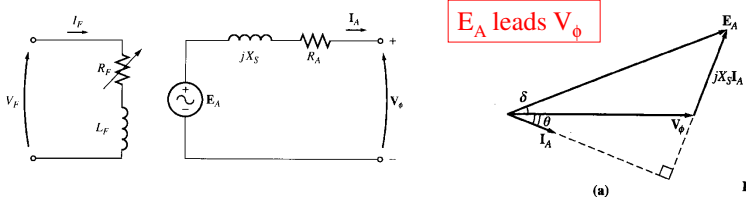
- This is done by varying the exciter's set point (I_F) and E_A .
- It is assumed that the governor's set point (P_{Mec}) remains constant ($P_{inj} = \text{const}$). When $I_F \uparrow$, $E_A \uparrow$, θ and Q_{inj} change.



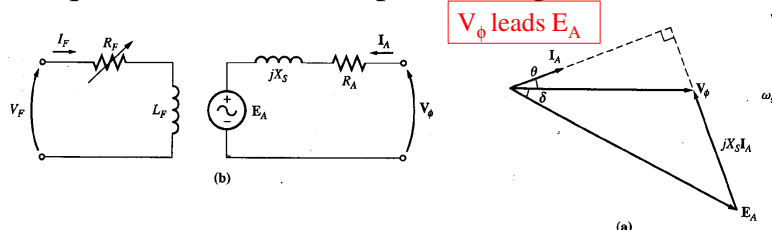
When does the generator supply Q? ... absorb Q?

Synchronous generators and motors

- Equivalent circuit and phasor diagram of **SG**

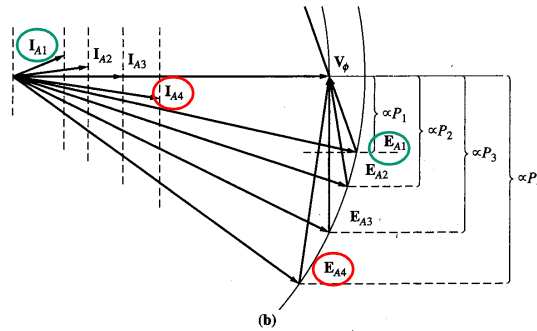


- Equivalent circuit and phasor diagram of **SM**



Effect of varying the load power (P_{Mec})

- It is assumed that the grid voltage and frequency remain constant. Besides I_f and E_A are fixed.

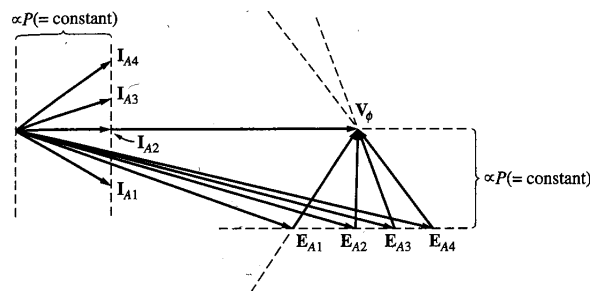


If $P \uparrow$, the power angle (δ) \uparrow .

- What happens to the reactive power of the motor as the active power it draws is increased?

Effect of varying I_f and E_A

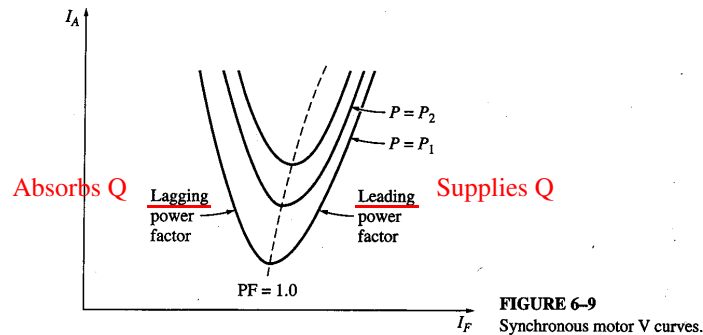
- It is assumed that the grid voltage and frequency remain constant. The load power (P_{Mec}) is fixed.



- What happens to the reactive power of the motor, when for a given P , I_f and E_A increase? Value of E_A for minimum I_A (and unity power factor)?

V curves for synchronous machines

- There is a value of I_f for which the machine operates with UPF (minimum I_A). As I_f increases or decreases, I_A increases. Machine either absorbs or supplies reactive power (Q).



Recall that E_a varies with I_f ...

Phasor diagrams: P and Q control

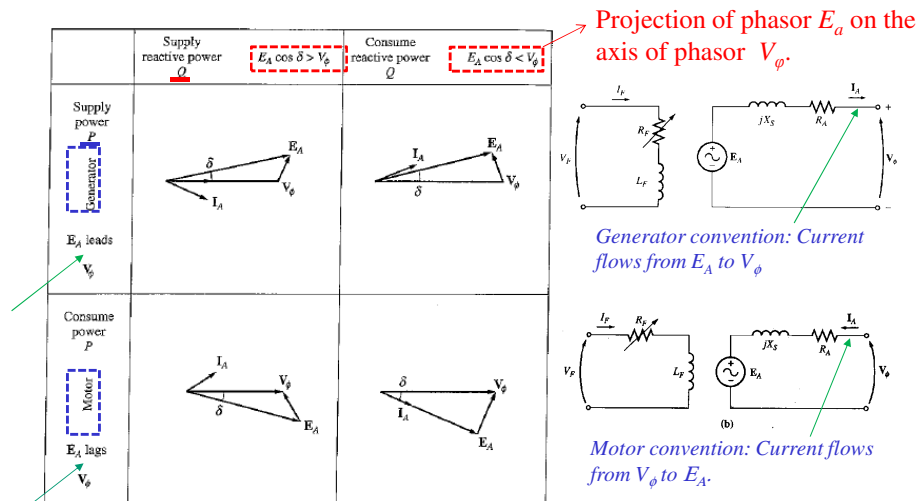


Figure from another book.