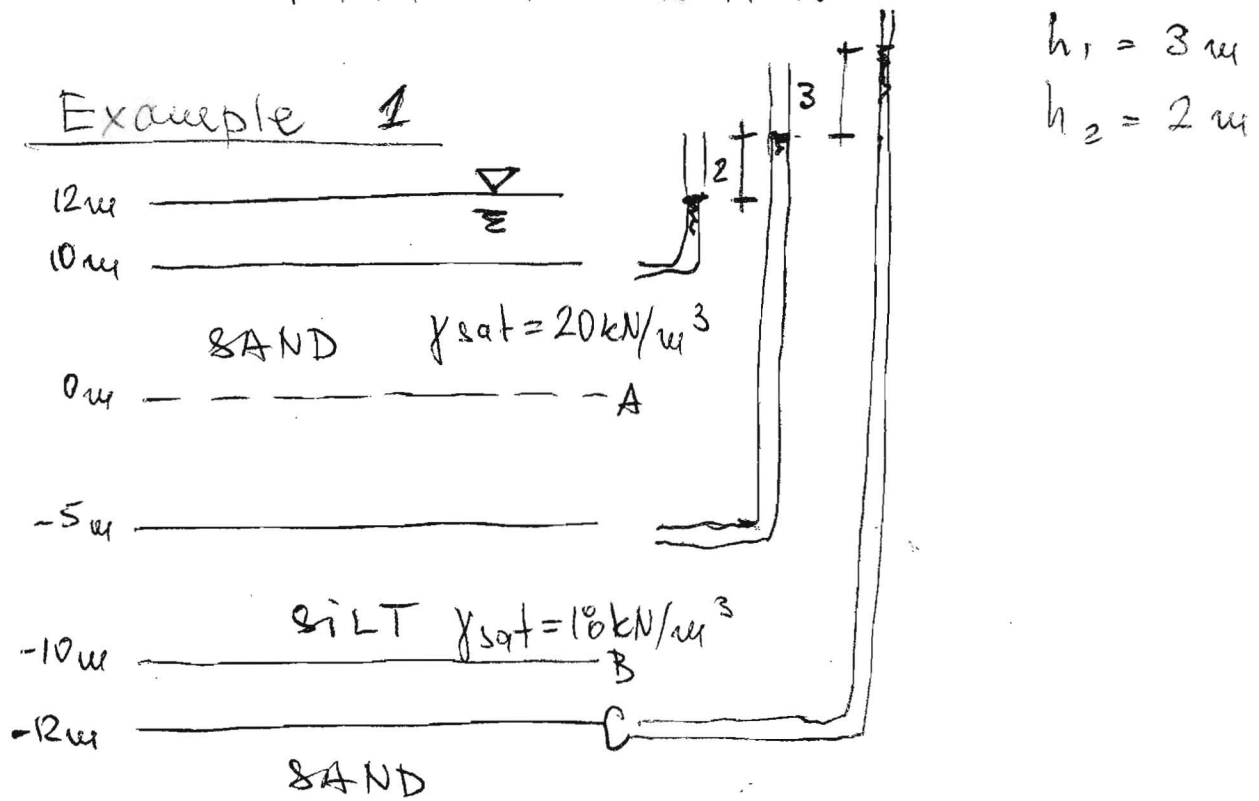


CEG 3109. Soil Mechanics  
Midterm Review



Solution

@ Point C ( $z = -12 \text{ m}$ )

$$\sigma_c = (12 - 10) \gamma_w + (10 - (-5)) \gamma_{sat}(\text{sand}) + [(-5) - (-12)] \gamma_{sat}(\text{silt})$$

$$\sigma_c = 2 \times 9.81 + 15 \times 20 + 7 \times 18 = \underline{445.62 \text{ kN/m}^2}$$

$$u_c = [12 - (-12)] \gamma_w + (3 + 2) \gamma_w = 24 \times 9.81 + 5 \times 9.81 = \underline{284.49 \text{ kN/m}^2}$$

$$\sigma'_c = \sigma_c - u_c = 445.62 - 284.49 = \underline{161.13 \text{ kN/m}^2}$$

@ Point B ( $z = -10 \text{ m}$ )

$$\sigma_B = (12 - 10) \gamma_w + [10 - (-5)] \gamma_{sat}(\text{sand}) + [(-5) - (-10)] \gamma_{sat}(\text{silt})$$

$$\sigma_B = 2 \times 9.81 + 15 \times 20 + 5 \times 18 = \underline{409.62 \text{ kN/m}^2}$$

$$u_B = [12 - (-10)] \gamma_w + (2) \gamma_w + \underbrace{\left\{ \frac{3}{[-5] - [-12]} \right\}}_i \underbrace{\{ [(-5) - (-10)] \}}_z \gamma_w$$

$$u_B = 22 \times \gamma_w + 2 \gamma_w + \left( \frac{3}{7} \right) (5) \gamma_w$$

$$u_B = 22 \times 9.81 + 2 \times 9.81 + 2.14 \times 9.81 = \underline{256.43 \text{ kN/m}^2}$$

$$\sigma_B' = \sigma_B - u_B = 409.62 - 256.43 = \underline{153.19 \text{ kN/m}^2}$$

② Point A ( $z = 0 \text{ m}$ )

$$\sigma_A = (12 - 10) \gamma_w + (10 - 0) \gamma_{\text{sat(sand)}}$$

$$\sigma_A = 2 \times 9.81 + 10 \times 20 = \underline{219.62 \text{ kN/m}^2}$$

$$u_A = [12 - (0)] \gamma_w + \underbrace{\left\{ \frac{2}{[10 - (-5)]} \right\}}_i \underbrace{\{ (10 - 0) \}}_z \gamma_w$$

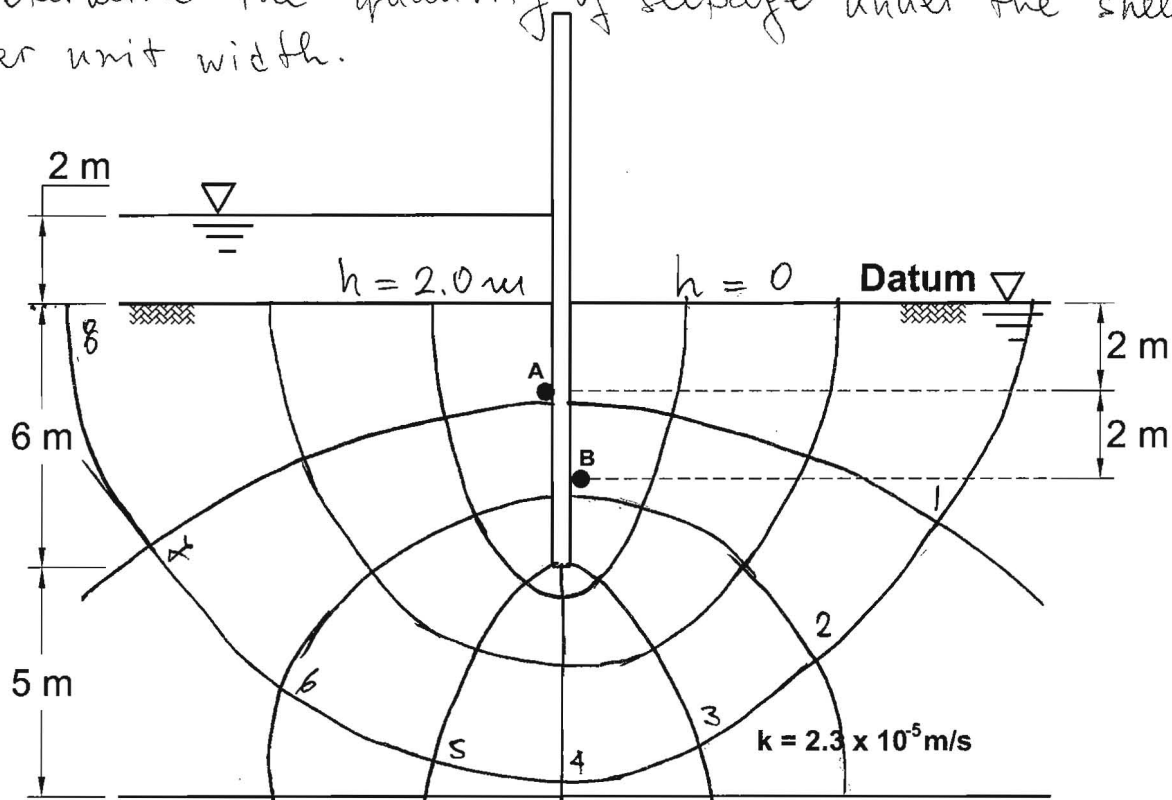
$$u_A = 12 \gamma_w + \left( \frac{2}{15} \right) (10) \gamma_w = 12 \times 9.81 + 1.33 \times 9.81 = \underline{130.80 \text{ kN/m}^2}$$

$$\sigma_A' = \sigma_A - u_A = 219.62 - 130.80 = \underline{88.82 \text{ kN/m}^2}$$

**Q2**

For a sheet piling shown below calculate the effective stress at point A and B ( $\gamma_{\text{sat}} = 20 \text{ kN/m}^3$ ).

Determine the quantity of seepage under the sheet piling per unit width.



Solution:

Total Head Loss:  $H = 2 - 0 = 2 \text{ m}$

Number of equipotential drops;  $N_d = 8$

$$\Delta h = \frac{2}{8} = 0.25 \text{ m}$$

Number of flow channels;  $N_f = 3.2$

Pore water pressure at point A ( $z = -2 \text{ m}$ )

Total head:  $2 - 0.8 \times \Delta h = 2 - 0.8 \times 0.25 = 1.8 \text{ m}$

$h_{p_A}$  Pressure head = Total - Elevation head =  $1.8 - (-2) = 3.8 \text{ m}$

$$u_A = h_{p(A)} \times \gamma_w = 3.8 \times 9.81 = 37.28 \text{ kN/m}^2$$

## Mid-term Review

### Example 2 - Cont

Pore water pressure at point B ( $z = -4 \text{ m}$ )

$$\text{Total head} = 2 - 6.2 \times 1.2 = 0.45 \text{ m}$$

$h_{pB}$  = pressure head = Total head - elevation head

$$h_{pB} = 0.45 - (-4) = 4.45 \text{ m}$$

$$u_B = h_{pB} \times \gamma_w = 4.45 \times 9.81 = 43.65 \text{ kN/m}^2$$

Calculating Stresses at A and B

$$\sigma_A = 2 \times \gamma_w + 2 \times \gamma_{\text{sat}} = 2 \times 9.81 + 2 \times 20 = 59.62 \text{ kN/m}^2$$

$$u_A = 37.28 \text{ kN/m}^2$$

$$\sigma'_A = \sigma_A - u_A = 59.62 - 37.28 = 22.34 \text{ kN/m}^2$$

$$\sigma_B = (2 + 2) \gamma_{\text{sat}} = 4 \times 20 = 80 \text{ kN/m}^2$$

$$u_B = 43.65 \text{ kN/m}^2$$

$$\sigma'_B = \sigma_B - u_B = 80 - 43.65 = 36.35 \text{ kN/m}^2$$

Quantity of seepage:

$$q = kH \left( \frac{N_f}{N_d} \right) \quad (\text{/width})$$

$$q = (2.3 \times 10^{-5}) (2) \left( \frac{3.2}{8} \right) = 1.84 \times 10^{-5} \text{ m}^3/\text{s} \quad (\text{/width})$$

## Mid-term Review

### Example 3

$$e_0(\text{sand}) = 0.76$$

$$w(\text{clay}) = 38\%$$

$$H_0(\text{clay}) = 2.0 \text{ m}$$

$$OCR = 1.5$$

$$C_c = 0.3$$

$$C_s = 0.05$$

$$G_s = 2.7$$

### Solution

- 1) Calculate  $\sigma_0'$  and  $e_0$  at the middle of the clay layer:

Sand

$$\gamma_d = \frac{G_s}{1+e_0} \gamma_w = \frac{2.7}{1+0.76} \times 9.81 = 15.05 \text{ kN/m}^3$$

$$\gamma_{\text{sat}} = \left( \frac{G_s + e_0}{1+e_0} \right) \gamma_w = \left( \frac{2.7 + 0.76}{1+0.76} \right) \times 9.81 = 19.3 \text{ kN/m}^3$$

Clay: Below water table, assume  $S = 100\%$

$$e_0 = w G_s = 0.38 \times 2.7 = 1.026 = 1.03$$

$$\gamma_{\text{sat}} = \left( \frac{G_s + e_0}{1+e_0} \right) \gamma_w = \left( \frac{2.7 + 1.03}{1+1.03} \right) \times 9.81 = 18.03 \text{ kN/m}^3$$

- 2) Calculate in-situ stress in the middle of clay

$$\sigma_0 = 3 \times 15.05 + 7.4 \times 19.3 + 1.0 \times 18.03 = 206.0 \text{ kN/m}^2$$

$$u_0 = (7.4 + 1.0) \times 9.81 = 82.40 \text{ kN/m}^2$$

$$\sigma_0' = \sigma_0 - u_0 = 206.0 - 82.40 = 123.6 \text{ kN/m}^2$$

$$\Delta \sigma = 140 \text{ kPa}$$

3) Final effective stress in the middle of clay,  $\sigma_1'$

$$\sigma_1' = \sigma_0' + \Delta \sigma = 123.6 + 140 = 263.6 \text{ kN/m}^2$$

4) Determine the preconsolidation pressure,  $\sigma_p'$

$$OCR = \frac{\sigma_p'}{\sigma_0'}$$

$$\sigma_p' = \sigma_0' \times OCR = 123.6 \times 1.5 = 185.4 \text{ kN/m}^2$$

5) Compare in-situ, preconsolidation and final effective stresses!

$$\sigma_0' = 123.6 < \sigma_p' = 185.4 < \sigma_1' = 263.6 \text{ kN/m}^2$$

6) Calculate Consolidation Settlement

$$S_c = \frac{C_s}{1+e_0} H_0 \log \left( \frac{\sigma_p'}{\sigma_0'} \right) + \frac{C_c}{1+e_0} H_0 \log \left( \frac{\sigma_1'}{\sigma_p'} \right)$$

$$S_c = \frac{0.05}{1+1.03} \times 2 \log \left( \frac{185.4}{123.6} \right) + \frac{0.3}{1+1.03} \times 2 \log \left( \frac{263.6}{185.4} \right)$$

$$S_c = 0.0087 + 0.045 = 0.054 \text{ m} = \underline{54 \text{ mm}}$$