

**SOLUTION**

1. In the 4-mesh, 5-node network shown in Fig.1, it is required to find the power P dissipated in the  $3\ \Omega$  resistor connected between nodes 2 & 3.
- (a) You are expected to choose only between mesh- or node- analysis methods. State the more efficient method of the two that you would use to obtain the required result. Explain the reason for your choice. **[Do not use Source Transformation, Thevenin/Norton or Superposition !]**.
- (b) Using the chosen method, solve the problem of finding P, clearly explaining each procedural step, before doing the associated calculation.
- (c) How would your answer to (a) above change, if the two ideal voltage sources were replaced with ideal current sources ?

( 2 + 6 + 2 marks)

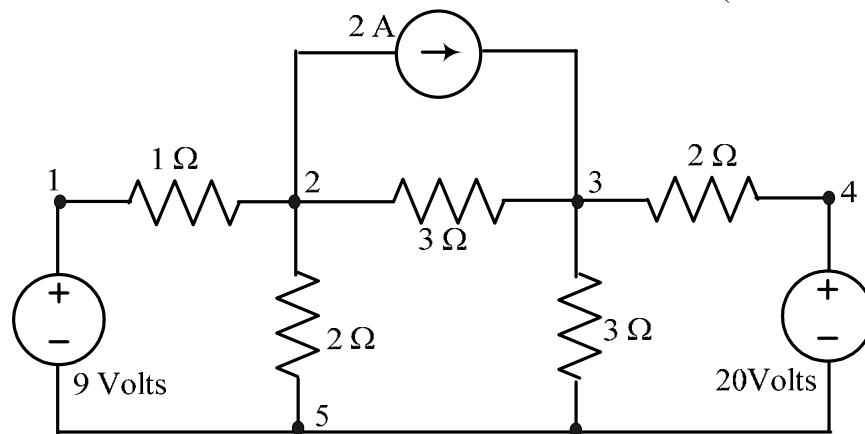


Figure 1

Solution:

(a) In order to find P , we require the voltage across the resistor ( $V_{23}$  or  $V_{32}$ ) or the current through it ( $I_{23}$  or  $I_{32}$ ). Since there are 2 voltage constraints and 1 current constraint, Mesh Analysis will require 3 mesh equations (lower 3 meshes) , and Node Analysis will require 2 nodal equations (nodes 2 & 3 with 5 as ground.)

Nodal analysis is preferable since it requires the lesser number of equations.

(b) Using Node 5 as the ground , the nodal equations at nodes 2 and 3 are, respectively,:

$$\frac{V_2 - 9}{1} + \frac{V_2 - V_3}{3} + \frac{V_2}{2} + 2 = 0 \quad \text{or} \quad 11V_2 - 2V_3 = 42$$

and 
$$\frac{V_3 - V_2}{3} + \frac{V_3}{3} + \frac{V_3 - 20}{2} - 2 = 0 \quad \text{or} \quad -2V_2 + 7V_3 = 72$$

Solving ,

**SOLUTION**

$$V_2 = \frac{(42)(7) - (72)(-2)}{(11)(7) - (-2)(-2)} = \frac{438}{73} = \underline{6 \text{ volts}}$$

$$\text{and } V_3 = \frac{(11)(72) - (-2)(42)}{(11)(7) - (-2)(-2)} = \frac{876}{73} = \underline{12 \text{ volts}}$$

From the above node voltages  $V_{32} = V_3 - V_2 = 12 - 6 = 6 \text{ volts}$

$$\text{and } P = (V_{32})^2 / R = (6)^2 / 3 = 36 / 3 = \underline{12 \text{ Watts}}$$

(c) If the 2 ideal voltage sources are replaced by ideal current sources, there will be 3 current constraints and mesh analysis will require only 1 mesh equation (for the central mesh), whereas nodal analysis (with 5 as ground) will require 2 equations at nodes 2 & 3.. Clearly, MA will then be the preferred method of analysis.

**SOLUTION**

2. For the op-amp circuit shown in Figure 2, (a) write the nodal equations at nodes 1 & 2, (b) determine voltage  $v_o$  and currents  $i_f$  and  $i_o$ .  
(2 + 2 + 2 + 2 + 2 marks)

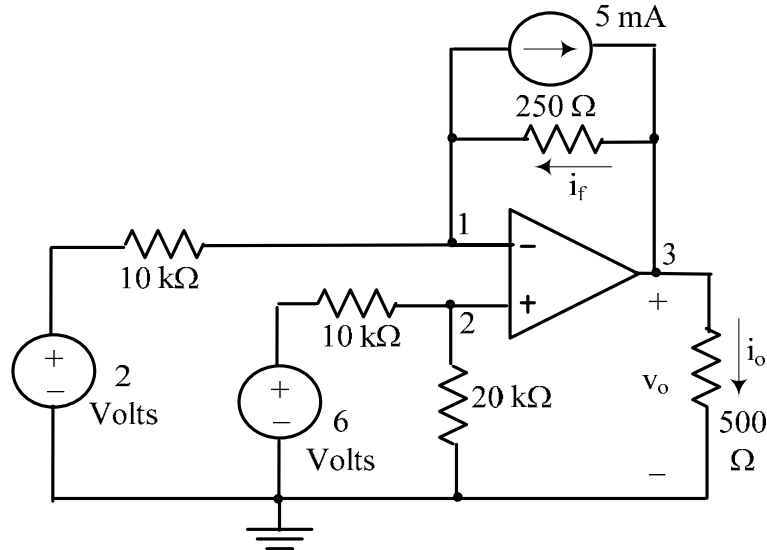


Figure 2

Solution: (a) With currents in **mA**,

$$\text{At Node 1, } \frac{v_1 - 2}{10} + \frac{v_1 - v_3}{0.25} + 5 = 0, \quad v_3 = v_o \quad \text{and} \quad v_1 = v_2$$

$$\text{At Node 2, } \frac{v_2 - 6}{10} + \frac{v_2}{20} = 0,$$

(b) From the Node 2 equation (or by voltage division),

$$v_1 = v_2 = 6 \left[ \frac{20}{30} \right] = 4 \text{ volts.}$$

Substitution for  $v_1$  in the Node 1 equation yields:

$$\frac{4 - 2}{10} + \frac{4 - v_o}{0.25} + 5 = 0 \quad \text{or} \quad 2 + 40(4 - v_o) + 50 = 0 \quad \text{or} \quad v_o = \underline{5.3 \text{ volts}}$$

$$i_f = (v_o - 4)/0.25 \text{ mA} = 1.3/0.25 = \underline{5.2 \text{ mA}}$$

$$i_o = v_o/0.5 \text{ mA} = 5.3/0.5 = \underline{10.6 \text{ mA}}$$

**SOLUTION**

3. The network to the left of terminals a-b , in Figure 3, is to be suddenly connected to the initially uncharged capacitor by means of the normally-open switch S .

- (a) With the switch S open, determine [Hint: Consider using Mesh Analysis]
  - (i) the open-circuit voltage  $v_{ab}(oc)$  across terminals a-b
  - (ii) the current  $i_{ab}(sc)$  that would flow between terminals a-b if these terminals are short circuited
  - (iii) the Thevenin equivalent circuit or the Norton equivalent circuit with respect to terminals a-b
- (b) If the switch S is closed at time  $t = 0$ , determine the capacitor voltage  $v(t)$ ,  $t > 0$ .

( 2 + 2 + 2 + 4 marks)

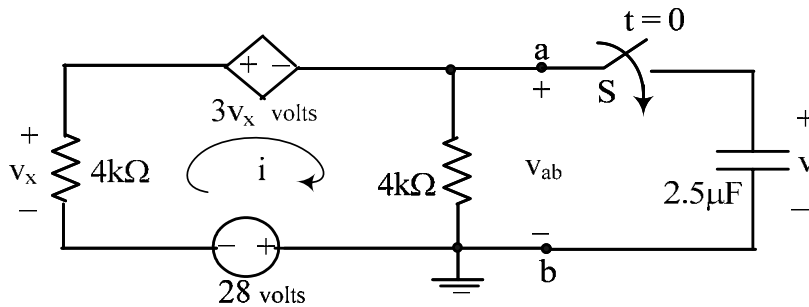


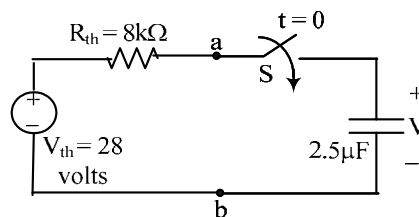
Figure 3

Solution: (a)

(i) Using current  $i$  (mA) ,  $v_x = -4i$  volts &  $v_{ab}(oc) = v_{th} = 4i$  volts  
 KVL with a-b OC :  $28 - (-4i) + 3(-4i) + 4i = 0$  or  $i = 28/4 = 7$  mA ,  
 $v_{ab}(oc) = v_{th} = 4i = \underline{28 \text{ volts}}$

(ii) KVL with a-b SC [  $i = i_{ab}(sc) = i_N$  ]:  
 $28 - (-4i) + 3(-4i) = 0$  or  $i_{ab}(sc) = i_N = 28/8 = \underline{3.5 \text{ mA}}$   
 $R_{Th} = V_{ab}(oc) / i_{ab}(sc) = 28/3.5m = \underline{8 \text{ k}\Omega}$

(iii) (The TEC connected to the switched C is :



(b)  $\tau = (8000)(2.5\mu) = 20$  msec  $V(t) = Ae^{-50t} + 28$  ,  $V(0) = 0 = A + 28$ , or  $A = -28$   
 Hence  $V(t) = \underline{28 [1 - e^{-50t}]}$  volts

**SOLUTION**

4. For the RLC circuit shown in Figure 4,  $L = 360 \text{ mH}$ ,  $C = 100 \mu\text{F}$
- Obtain the governing differential equation for the voltage  $v(t)$ .
  - Find the value of  $R$  which will result in a critically-damped natural response .
  - If  $R = 30 \Omega$  obtain the natural response  $v(t)$ ,  $t > 0$  if  $v(0) = 3 \text{ Volts}$  and  $i(0) = 0.2 \text{ A}$ . (4 + 2 + 4 marks)

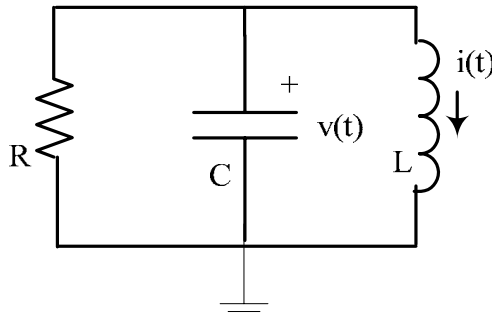


Figure 4

Solution: (a) KCL :  $\frac{v}{R} + C \frac{dv}{dt} + i = 0$  , KVL:  $L \frac{di}{dt} - v = 0$

To obtain the differential equation in  $v$  , obtain  $di/dt$  from the KCL equation and substitute into the KVL equation.

$$\text{ie } L \left[ -\frac{1}{R} \frac{dv}{dt} - C \frac{d^2v}{dt^2} - v \right] = 0 \quad \text{or} \quad \frac{d^2v}{dt^2} + \frac{1}{CR} \frac{dv}{dt} + \frac{1}{LC} v = 0$$

$$\alpha = \frac{1}{2CR} \quad , \quad \omega_n^2 = \frac{1}{LC} = \frac{1}{36(10)^{-6}} \quad (\text{or } \omega_n = 166.667 \text{ rad/s})$$

(b) For critical damping  $\alpha = \omega_n$  or  $R = \frac{1}{2} \sqrt{\frac{L}{C}} = 60/2 = \underline{30 \Omega}$

(c) For  $R = 30 \Omega$ ,  $v(t) = [A_1 + A_2 t] e^{-166.7t} + 0$   
 $v(0) = 3 = [A_1 + 0] 1 + 0$  or  $A_1 = 3$

From the KCL equation  $3/30 + 100(10)^{-6} \frac{dv}{dt}(0) + 0.2 = 0$

$$\text{or } \frac{dv}{dt}(0) = -0.3 / 100(10)^{-6} = -3000$$

Therefore  $-166.667A_1 + A_2 = -3000$  or  $A_2 = -2500$

$$v(t) = \underline{[3 - 2500t] e^{-166.7t}} \text{ volts}$$

**SOLUTION**

5. An AC circuit operating at a radian frequency  $\omega = 4$  rad/sec is shown (in the time domain) in Figure 5.

(a) Draw the phasor domain equivalent circuit and determine the phasor current  $I_1$

(b) Hence determine the voltage  $v_b(t)$  in the form

$$v_b(t) = V \cos(\omega t \pm \phi), \text{ volts} \quad (4 + 4 + 2 \text{ marks})$$

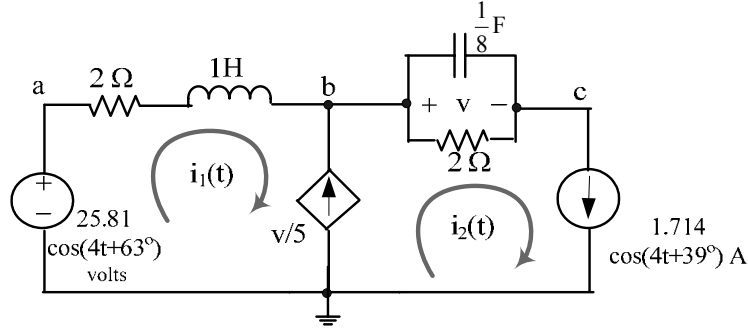
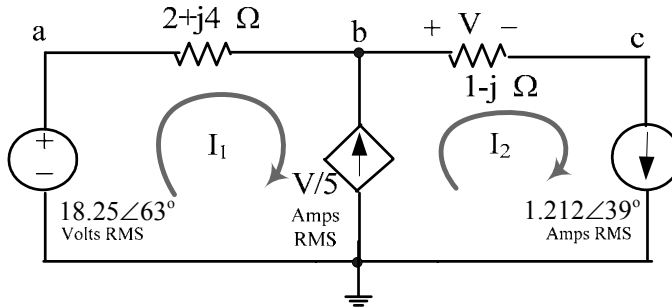


Figure 5

Solution: (a)  $Z_{ab} = 2 + j(4)(1) = 2 + j4$  ohms =  $4.47 \angle 63.43^\circ$

and  $Z_{bc} = 2 \text{ P } [ -j / (4)(1/8) ] = 2 \text{ P } (-j2) = -j 4 / (2-j2) = -j2(1-j) = 1-j$  ohms  
 $= 1.414 \angle -45^\circ$

The phasor equivalent circuit is shown below



Ohm's Law :  $V = Z_{bc}I_2 = 1.414 \angle -45^\circ (1.212 \angle 39^\circ) = 1.714 \angle -6^\circ$  volts (2.424pk)

And  $I_2 - I_1 = V/5$

Hence  $I_1 = I_2 - V/5 = 1.212 \angle 39^\circ - 0.343 \angle -6^\circ$   
 $= 0.942 + j 0.763 - 0.341 + j 0.036 = 0.6 + j 0.799$   
 $= 1 \angle 53.1^\circ$  (1.414 pk)

(b) KVL:  $V_b = 18.25 \angle 63^\circ - (2+j4)I_1 = 18.25 \angle 63^\circ - 4.47 \angle 116.53^\circ$   
 $\approx 8.285 + j 16.26 + 1.99 - j 4 = 10.275 + j 12.26$   
 $= 15.996 \angle 50^\circ \approx 16 \angle 50^\circ$  vRMS (22.62 pk)

Hence  $v_b(t) = 16 \cos(4t + 50^\circ)$  volts RMS  
 $= 22.62 \cos(4t + 50^\circ)$  volts peak

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6. The circuit of Figure 6 shows a series RLC load connected to an AC source whose a voltage is 972 volt RMS at a radian frequency of 2765 radians/sec. Determine :
- the power-factor of the load , also stating whether the PF is lagging or leading
  - the RMS current delivered by the source
  - the average power  $P$  and the reactive power  $Q$  in the load
  - A capacitor  $C$  is to be connected in parallel with the load (as shown, by closing the switch  $S$ ) in order to change the overall load PF to 0.71 lagging. Determine the required value of  $C$  .

(3 + 1 + 2 + 4 marks)

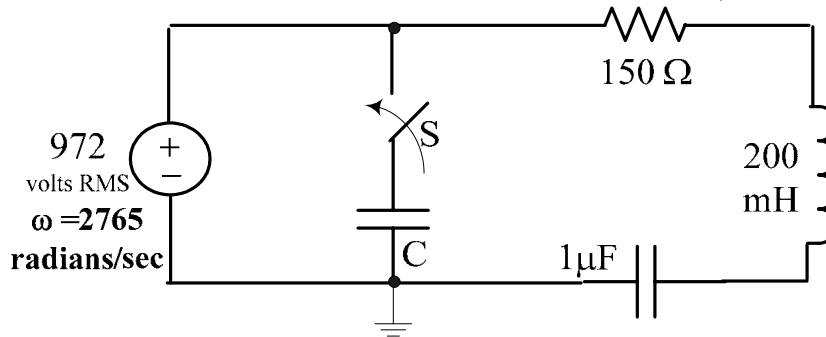


Figure 6

Solution: (a) The load impedance  $Z_L = 150 + j(2765)(0.2) - j / 2765(10)^{-6}$   
 $= 150 + j553 - j 361.7$   
 $= 150 + j191.3 = 243.1 \angle 51.9^\circ$

The load power factor is  $\cos 51.9^\circ = \underline{0.617 \text{ lagging}}$   
 (lagging, since the impedance angle is positive)

(b) The RMS current delivered by the source  $= 972/243.1 = 3.998 \text{ A} \approx \underline{4 \text{ A}}$

(c) Average power  $P = I^2 \text{Re } Z_L \approx 16 (150) = \underline{2.4 \text{ kW}}$   
 Reactive power  $Q = I^2 \text{Im } Z_L \approx 16 (191.3) \approx \underline{3.06 \text{ kvar}}$

(d) For a PF = 0.71 lagging ,  $\theta = \cos^{-1}(0.71) = 44.77^\circ$  and  $\tan\theta = 0.9918$

$$Q_{\text{new}} = P \tan\theta_{\text{new}} = 2400(0.9918) = 2380.4 \text{ var}$$

$$\text{I.e } \Delta Q = 2380.4 - 3060 = -679.6 = -\omega CV^2$$

$$\text{or } C = 679.6 / (2765)(972)^2 \approx \underline{0.26 \mu\text{F}}$$