

**CONCORDIA UNIVERSITY**  
**FACULTY OF ENGINEERING AND COMPUTER SCIENCE**  
**ENGR 372/4 sec. Y FUNDAMENTALS OF CONTROL SYSTEMS**

Mid-Term

Instructor: Dr. H. Hong

Date: March 9, 2000

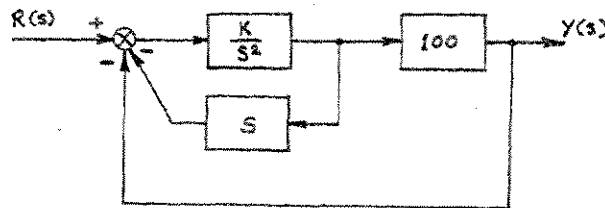
Answer all three (3) questions. Closed book exam. Total time: 1 hour 15 minutes

Problem 1. →23; Problem 2. →7; Problem 3. →5; = 35 marks total.

**Problem 1.** [ a→1, b→7, c→3, d→2, e→1, f→3, g→3, h→3 = 23 marks ]

A negative feedback control system has a block diagram as shown below.

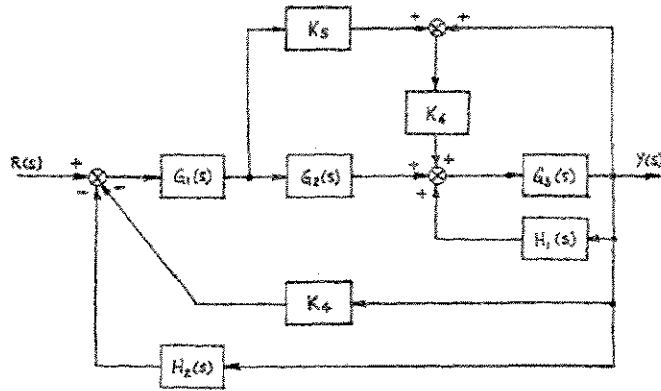
- (a) Determine the closed-loop transfer function  $T(s) = Y(s)/R(s)$ .
- (b) For a unit step input, find the value for the gain  $K$  so that the system has 20% overshoot.  
What is the natural frequency  $\omega_n$  of the system?  
What is the settling time  $T_s$  of the system?
- (c) Sketch the closed-loop poles on the  $s$ -plane. Clearly indicate  $\omega_n$  (natural frequency) and  $\theta$  (angular representation of the damping ratio  $\zeta$ ), and their numerical values, on the figure.
- (d) Using the Routh-Hurwitz stability criterion determine the range of gain  $K$  for the system to be stable?
- (e) What is the "type number" of the system?
- (f) For a unit step input, determine the position error constant  $K_p$ , and the steady-state error.  
Show all mathematical steps leading to your answer.
- (g) For a unit ramp input, determine the velocity error constant  $K_v$ , and the steady-state error.  
Show all mathematical steps leading to your answer.
- (h) For a unit acceleration input, determine the acceleration error constant  $K_a$ , and the steady-state error.  
Show all mathematical steps leading to your answer.



Problem 2. [ a→1½, b→5½ = 7 marks ]

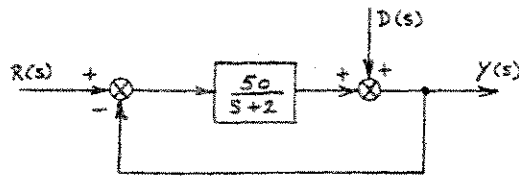
For the system represented in the block diagram below, find:

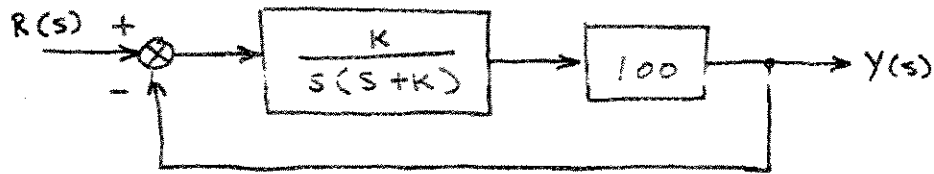
- (a) the signal flow graph representation.
- (b) the transfer function  $T(s) = Y(s)/R(s)$ , by using (only) Mason's signal-flow gain formula.



Problem 3. [ 5 marks ]

For the system shown below find the total steady-state error due to a unit step input  $R(s)$  and a unit step disturbance  $D(s)$ .



Problem # 1

$$\text{inner loop} \Rightarrow \frac{K/s^2}{1 + s(K/s^2)} = \frac{K}{s^2 + Ks} = \frac{K}{s(s+K)}$$

$$a) \quad \frac{Y(s)}{R(s)} = \frac{G}{1+G} = \frac{\frac{100K}{s(s+K)}}{1 + \frac{100K}{s(s+K)}} = \frac{100K}{s^2 + Ks + 100K}$$

b) From the characteristic equation

$$s^2 + Ks + 100K = s^2 + 2\xi\omega_n s + \omega_n^2 = 0$$

$$\omega_n = \sqrt{100K} \quad \text{----- (equation 1)}$$

$$2\xi\omega_n = 2\xi\sqrt{100K} = K \quad \text{----- (equation 2)}$$

given: 20% overshoot

$$P.O. = 100 \exp\left[\frac{-\xi\pi}{\sqrt{1-\xi^2}}\right]$$

$$\frac{-\xi\pi}{\sqrt{1-\xi^2}} = \ln\left(\frac{20}{100}\right) = -1.6094$$

$$1 - \xi^2 = 3.8102 \xi^2$$

$$\therefore \xi = 0.4559$$

From equation 2

$$2\xi\sqrt{100K} = K$$

$$4\xi^2(100K) = K^2$$

$$\therefore K = 400\xi^2 = 400(0.4559)^2$$

$$K = 83.1379$$

From equation 1

$$\omega_n = \sqrt{100K} = \sqrt{100 \times 83.1379}$$

$$\omega_n = 91.18 \text{ rad/sec}$$

$$\therefore s^2 + Ks + 100K = s^2 + 83.1379s + 8313.7924$$

$$T_s = \frac{4}{\xi\omega_n} = \frac{4}{(0.4559)(91.18)}$$

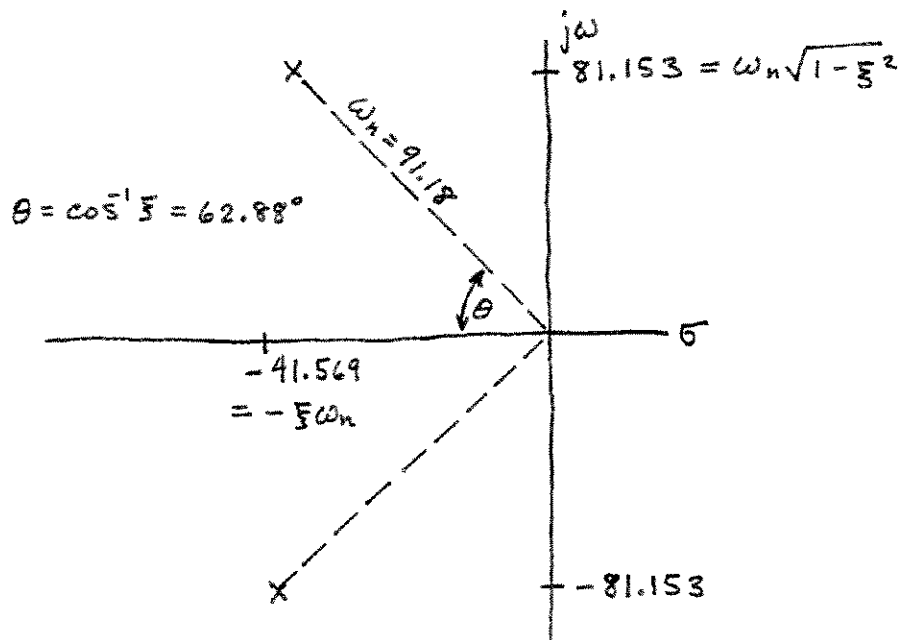
$$T_s = 0.0962 \text{ sec.}$$

$$c) \quad s^2 + 83.1379s + 8313.7924 = 0$$

$$s_1, s_2 = \frac{-83.1379 \pm \sqrt{(83.1379)^2 - 4(8313.7924)}}{2}$$

$$= \frac{-83.1379 \pm 162.3061}{2}$$

$$s_1, s_2 = -41.569 \pm j81.153$$



d) From the Routh-Hurwitz Stability Criterion

$$s^2 + ks + 100k = 0$$

$$\begin{array}{l|ll} s^2 & 1 & 100k \\ s^1 & k & 0 \\ s^0 & 100k & \end{array}$$

from row  $s^1$ ,  $k > 0$  for the system to be stable.

e) From the reduced block diagram, in unity feedback form, the system is "type 1".

$$f) e_{ss} = \frac{1}{1 + K_p} \quad \text{for } R(s) = \frac{A}{s} = \frac{1}{s}$$

$$K_p = \lim_{s \rightarrow 0} G(s) \quad \text{where } G(s) = \frac{100k}{s(s+k)}$$

$$= \lim_{s \rightarrow 0} \left[ \frac{100k}{s(s+k)} \right]$$

$$K_p = \infty$$

$$\therefore e_{ss} = \frac{1}{1 + \infty} = 0$$

$$g) e_{ss} = \frac{1}{K_v} \quad \text{for } R(s) = \frac{A}{s^2} = \frac{1}{s^2}$$

$$K_v = \lim_{s \rightarrow 0} s G(s) \quad \text{where } G(s) = \frac{100K}{s(s+K)}$$

$$= \lim_{s \rightarrow 0} s \left[ \frac{100K}{s(s+K)} \right]$$

$$K_v = 100$$

$$\therefore e_{ss} = \frac{1}{100}$$

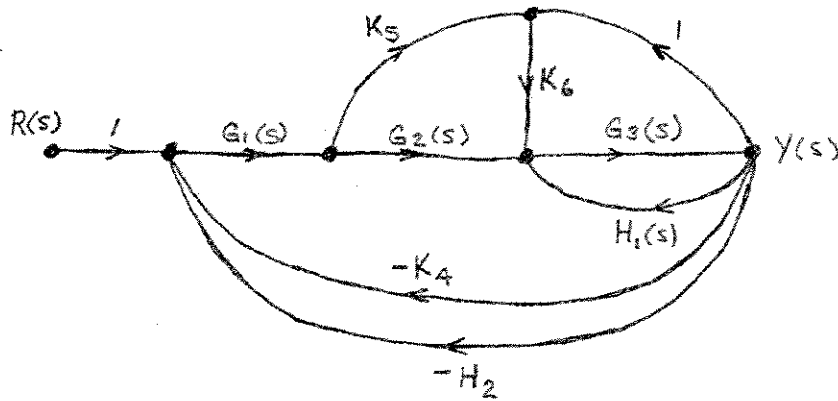
$$h) e_{ss} = \frac{1}{K_a} \quad \text{for } R(s) = \frac{A}{s^3} = \frac{1}{s^3} \quad (At^2/2)$$

$$K_a = \lim_{s \rightarrow 0} s^2 G(s) \quad \text{where } G(s) = \frac{100K}{s(s+K)}$$

$$= \lim_{s \rightarrow 0} s^2 \left[ \frac{100K}{s(s+K)} \right]$$

$$K_a = 0$$

$$e_{ss} = \frac{1}{0} = \infty, \quad \text{system cannot track a parabola input}$$



$$L_1 = G_3 K_6$$

$$L_2 = G_3 H_1$$

$$L_3 = -G_1 G_2 G_3 K_4$$

$$L_4 = -G_1 G_2 G_3 H_2$$

$$L_5 = -G_1 K_5 K_6 G_3 K_4$$

$$L_6 = -G_1 K_5 K_6 G_3 H_2$$

$$P_1 = G_1 G_2 G_3$$

$$P_2 = G_1 K_5 K_6 G_3$$

$$\Delta = 1 - (L_1 + L_2 + L_3 + L_4 + L_5 + L_6)$$

$$= 1 - G_3 K_6 - G_3 H_1 + G_1 G_2 G_3 K_4 + G_1 G_2 G_3 H_2 + G_1 K_5 K_6 G_3 K_4 + G_1 K_5 K_6 G_3 H_2$$

$$= 1 - G_3 (K_6 + H_1) + G_1 G_2 G_3 (K_4 + H_2) + G_1 K_5 K_6 G_3 (K_4 + H_2)$$

$$\Delta = 1 - G_3 (K_6 + H_1) + G_1 G_3 (K_4 + H_2) (G_2 + K_5 K_6)$$

$$\Delta_1 = 1 \quad P_1 \Delta_1 = G_1 G_2 G_3$$

$$\Delta_2 = 1 \quad P_2 \Delta_2 = G_1 K_6 K_5 G_3$$

$$P_1 \Delta_1 + P_2 \Delta_2 = G_1 G_3 (G_2 + K_5 K_6)$$

$$\frac{Y(s)}{R(s)} = \frac{G_1 G_3 (G_2 + K_5 K_6)}{1 - G_3 (K_6 + H_1) + G_1 G_3 (K_4 + H_2) (G_2 + K_5 K_6)}$$

Problem # 3

$$E(s) = E_R(s) + E_D(s)$$

$$E_R(s) = \frac{1}{1 + \frac{50}{s+2}} \cdot R(s) = \frac{s+2}{s+52} \cdot \frac{1}{s}$$

$$E_D(s) = \frac{-1}{1 + \frac{50}{s+2}} \cdot D(s) = -\frac{s+2}{s+52} \cdot \frac{1}{s}$$

$$e_{ss} = \lim_{s \rightarrow 0} s E(s) = \lim_{s \rightarrow 0} s [E_R(s) + E_D(s)]$$

$$= \lim_{s \rightarrow 0} s \left[ \frac{s+2}{s+52} - \frac{s+2}{s+52} \right] \frac{1}{s}$$

$$= 0$$

OR

$$\frac{Y_R}{R} = \frac{\frac{50}{s+2}}{1 + \frac{50}{s+2}} = \frac{50}{s+52}$$

$$\text{steady state } Y_R = \lim_{s \rightarrow 0} s \left[ \frac{50}{s+52} \right] \frac{1}{s} = \frac{50}{52}$$

$$\frac{Y_D}{D} = \frac{1}{1 + \frac{50}{s+2}} = \frac{s+2}{s+52}$$

$$\text{steady state } Y_D = \lim_{s \rightarrow 0} s \left[ \frac{s+2}{s+52} \right] \frac{1}{s} = \frac{2}{52}$$

$$Y = Y_R + Y_D = \frac{50}{52} + \frac{2}{52} = 1$$

$$e_{ss} = R - Y = 1 - 1 = 0$$

1.80

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DEPARTMENT OF MECHANICAL AND INDUSTRIAL ENGINEERING  
MECH 371/4 sec. X FUNDAMENTALS OF CONTROL SYSTEMS

Mid-Term

Instructor: H. Hoog

Date: March 4, 2003

Answer all four (4) questions. Closed book exam. Total time: 1 hour 15 minutes

For all questions:

Clearly show all equations and mathematical steps.

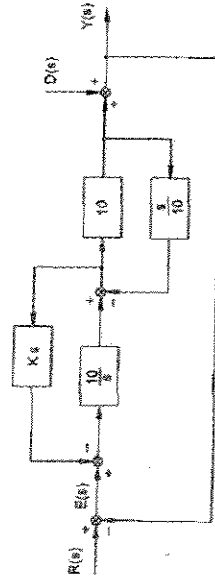
Answers without mathematical steps will be given a mark of zero.

Problem 1. → 23; Problem 2. → 10; Problem 3. → 10; Problem 4. → 12 = 55 marks total.

Problem 1. [ 1 → 3, 2 → 2, 3 → 6, 4 → 4, 5 → 6, 6 → 2 = 23 marks ]

A negative feedback control system has a block diagram as shown below.

- (1) Draw the signal flow graph for the system.
- (2) Determine the closed-loop transfer function  $T(s) = Y(s)/R(s)$ .
- (3) For a unit step input, find the value for the gain  $K$  so that the system has 20% overshoot. What is the natural frequency  $\omega_n$  of the system? What is the settling time  $T_s$  of the system?
- (4) Sketch the closed-loop poles on the  $s$ -plane. Clearly indicate  $\omega_n$  (natural frequency),  $\omega_d$  (damped natural frequency), and  $\theta$  (angular representation of the damping ratio  $\zeta$ ), and their numerical values, on the figure.
- (5) Find the total steady-state response due to a unit step input  $R(s)$  and a unit step disturbance  $D(s)$ .
- (6) Determine the sensitivity of the transfer function  $T(s)$  with respect to gain  $K$ , i.e.  $S_K^T$



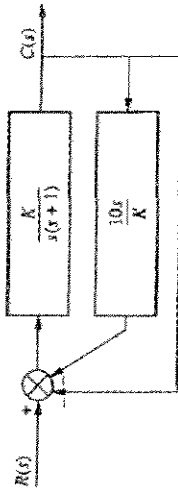
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Problem 2. [ 10 marks ]

For the feedback control system shown below:

- (1) Determine the type number of the system.
- (2) Using the concept of system type number, determine the steady state error to a unit step input.
- (3) Using the concept of system type number, determine the steady state error to a unit ramp input.
- (4) Using the concept of system type number, determine the steady state error to a unit parabola input.



Problem 3. [ 10 marks ]

Using the Routh-Hurwitz test, determine the stability of the closed-loop transfer function:

$$T(s) = \frac{10}{s^3 + 7s^2 + 6s^3 + 42s^2 + 8s + 36}$$

Determine, if any,

- (1) the marginally stable roots, and their numerical values.
- (2) the total number of unstable roots.

HINT: The negative number  $-4$  is a vector written as  $-4 + 0j$  or as  $4e^{j180^\circ}$ .

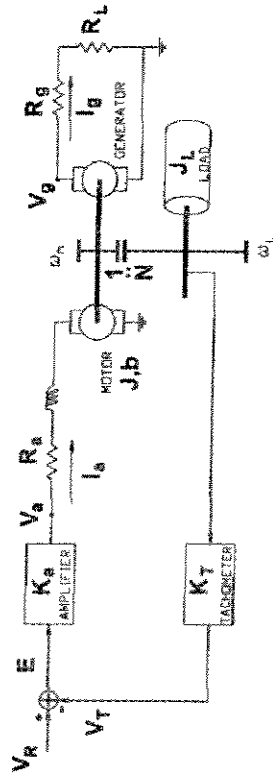
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**Problem 4. [ 12 marks ]**

A permanent magnet DC-motor drives a rotational load through a speed reduction gear ratio. The motor also directly drives a generator that supplies current to a resistive load. The load speed is measured by a tachometer for velocity feedback control. The error between the reference and tachometer voltage drives an amplifier that supplies power to the armature of the DC-motor.

Draw the block diagram for the feedback control system shown in the schematic diagram below. Provide justification to any assumptions made.



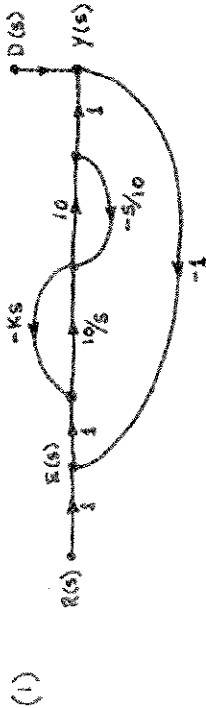
Given equations with respect to schematic diagram:

- $E(s) = V_R(s) - V_T(s)$  error = reference voltage minus tachometer voltage
- $V_T(s) = K_T \omega_L(s)$  tachometer voltage = tachometer gain times load speed
- $V_e(s) = K_a E(s)$  amplifier gain times error voltage
- $V_a(s) = K_a I_a(s) + V_g(s)$  amplifier (or armature) voltage = armature resistance times armature current plus back EMF [armature inductance neglected]
- $V_g(s) = K_g \omega_m(s)$  back EMF = back EMF gain times motor speed
- $T_m(s) = T(s) - T_d(s)$  torque driving motor = motor generated torque less torque driving disturbances
- $T_m(s) = J \dot{\omega}_m(s) + b \omega_m$  torque driving motor = armature inertia times motor speed plus damping times motor speed
- $T_d(s) = T_d(s) + T_g(s)$  disturbance torque = torque driving inertia load plus torque driving generator

Equations that must be derived from schematic diagram:

- $\omega_L(s) = ??$  load speed  $\omega_L(s) \Rightarrow$  motor speed  $\omega_m(s)$  with gear reduction. Let gear ratio be  $N > 1$
- $T_d(s) = ??$  load torque  $T_d(s) \Rightarrow$  rotational load inertia  $J_L$ ; omit damping;
- $V_g(s) = ??$  load angular acceleration  $\dot{\omega}_m(s)$ ; gear ratio  $N > 1$
- $V_a(s) = ??$  generator voltage  $V_g(s) \Rightarrow$  generator voltage gain  $K_g$ ; generator (or motor) speed  $\omega_m(s)$
- $I_a(s) = ??$  generator current  $I_g(s) \Rightarrow$  generator armature resistance  $R_g$ ; resistive load  $R_L$ ; generator voltage  $V_g(s)$ ; neglect generator inductance
- $T_m(s) = ??$  generator torque  $T_g(s) \Rightarrow$  generator constant  $K_g$
- $I_e(s) = ??$  generator current  $I_g(s)$

Problem # 1



$$(1) \quad T(s) = \frac{Y(s)}{R(s)} = \frac{(\frac{10}{s})(10)}{1 - (-[Ks][\frac{10}{s}] - [10][\frac{10}{s}] - [\frac{10}{s}][10])}$$

$$T(s) = \frac{10^3/s}{1 + 10K + s + \frac{10^3}{s}}$$

$$T(s) = \frac{100}{s^2 + s(10K+1) + 100}$$

$$(2) \quad s^2 + s(10K+1) + 100 = s^2 + 2\zeta\omega_n s + \omega_n^2$$

$$\omega_n = 10 \text{ rad/sec}$$

$$2\zeta\omega_n = 10K+1$$

$$P.O. = 20 = 100 \exp\left[\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}\right]$$

$$\ln\left[\frac{20}{100}\right] = -\frac{\zeta\pi}{\sqrt{1-\zeta^2}} = -1.6094$$

(1/6)

$$1 - \zeta^2 = 3.8104 \zeta^2$$

$$\therefore \zeta = 0.4559$$

$$K = \frac{2\zeta\omega_n - 1}{10} = \frac{(2)(0.4559)(10) - 1}{10}$$

$$K = 0.8119$$

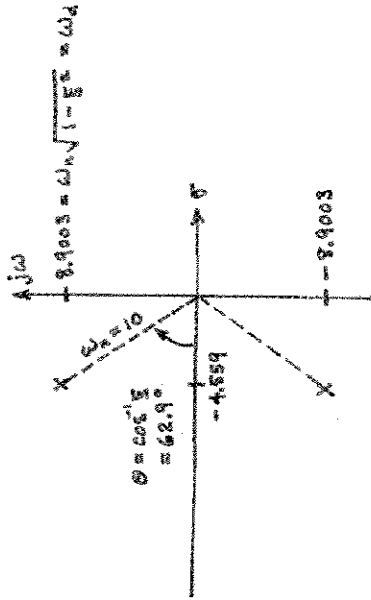
$$T_s = \frac{4}{\zeta\omega_n} = \frac{4}{(0.4559)(10)}$$

$$T_d = 0.8774 \text{ sec.}$$

$$(4) \quad s^2 + 9.1185s + 100$$

$$= \frac{-9.118 \pm \sqrt{(9.118)^2 - 4 \times 100}}{2} = \frac{-9.118 \pm 17.8006j}{2}$$

$$s_1, s_2 = -4.559 \pm 8.9003j$$



(2/6)

$$(5) Y(s) = T_1 R(s) + T_2 D(s)$$

$$T_1 = \frac{100}{s^2 + s(10K+1) + 100}$$

$$T_2 = \frac{1 \cdot (1+10K+s)}{1+10K+s + \frac{100}{s}} = \frac{s(1+10K+s)}{s^2 + s(10K+1) + 100}$$

for  $R(s) = \frac{1}{s}$  and  $D(s) = \frac{1}{s}$

$$y(\infty) = \lim_{s \rightarrow 0} s \left[ \frac{100}{s^2 + s(10K+1) + 100} \right] \cdot \frac{1}{s} + \lim_{s \rightarrow 0} s \left[ \frac{s(1+10K+s)}{s^2 + s(10K+1) + 100} \right] \cdot \frac{1}{s}$$

$$Y(\infty) = 1 + 0 = 1$$

$$(6) S_K^T = \frac{\partial T}{\partial K} \cdot \frac{K}{T}$$

$$\frac{\partial T}{\partial K} = - \frac{10S}{[s^2 + s(10K+1) + 100]^2}$$

$$S_K^T = \frac{-10S}{[s^2 + s(10K+1) + 100]^2} \cdot K \cdot \frac{[s^2 + s(10K+1) + 100]}{100}$$

$$S_K^T = \frac{-KS}{10[s^2 + s(10K+1) + 100]}$$

(3/6)

Problem #2

Reduce inner loop

$$\frac{\frac{K}{s(s+1)}}{1 + \left( \frac{K}{s(s+1)} \right) \left( \frac{10s}{K} \right)}$$

$$= \frac{K}{s(s+1) + 10KS} = \frac{K}{s[s + 10K + 1]}$$



(1) Type 1 system,  $G(s) = \frac{K}{s(s+10K+1)}$

(2)  $K_P = \lim_{s \rightarrow 0} G(s) = \infty$

$$e_{ss} = \frac{1}{1+K_P} = \frac{1}{1+\infty} = 0$$

(3)  $K_V = \lim_{s \rightarrow 0} sG(s) = \frac{K}{10K+1}$

$$e_{ss} = \frac{1}{K_V} = \frac{10K+1}{K}$$

(4)  $K_A = \lim_{s \rightarrow 0} s^2 G(s) = 0$

$$e_{ss} = \frac{1}{K_A} = \frac{1}{0} = \infty, \text{ i.e. cannot track acceleration input}$$

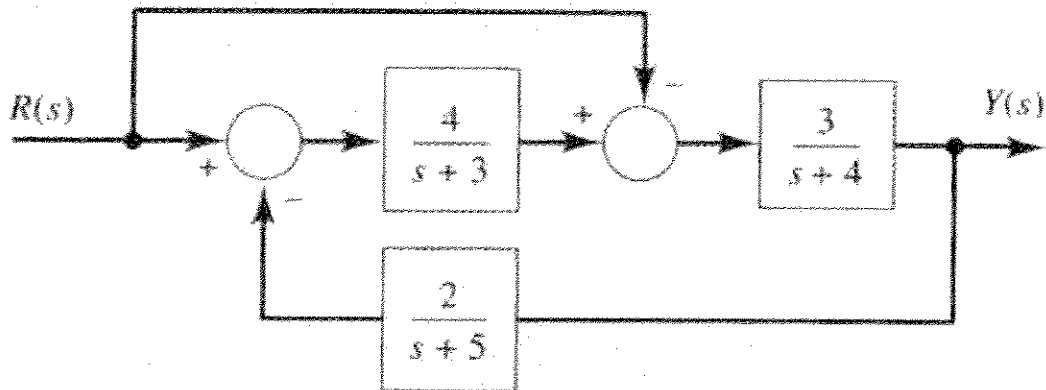
(4/6)



**Problem #1** (  $a = 3$ ,  $b = 5$ ,  $c = 5$ ,  $d1 = 4$ ,  $d2 = 3 \rightarrow \rightarrow 20$  marks )

For the system block diagram given below:

- Draw the signal flow graph for the system.
- Determine the overall transfer function  $\frac{Y(s)}{R(s)} = G(s)$ .
- Determine the type number of the system.
- Using the method of system type number as determined from part (3) of the question above, determine:
  - The steady state error due to unit step input.
  - The steady state error due to unit ramp input.

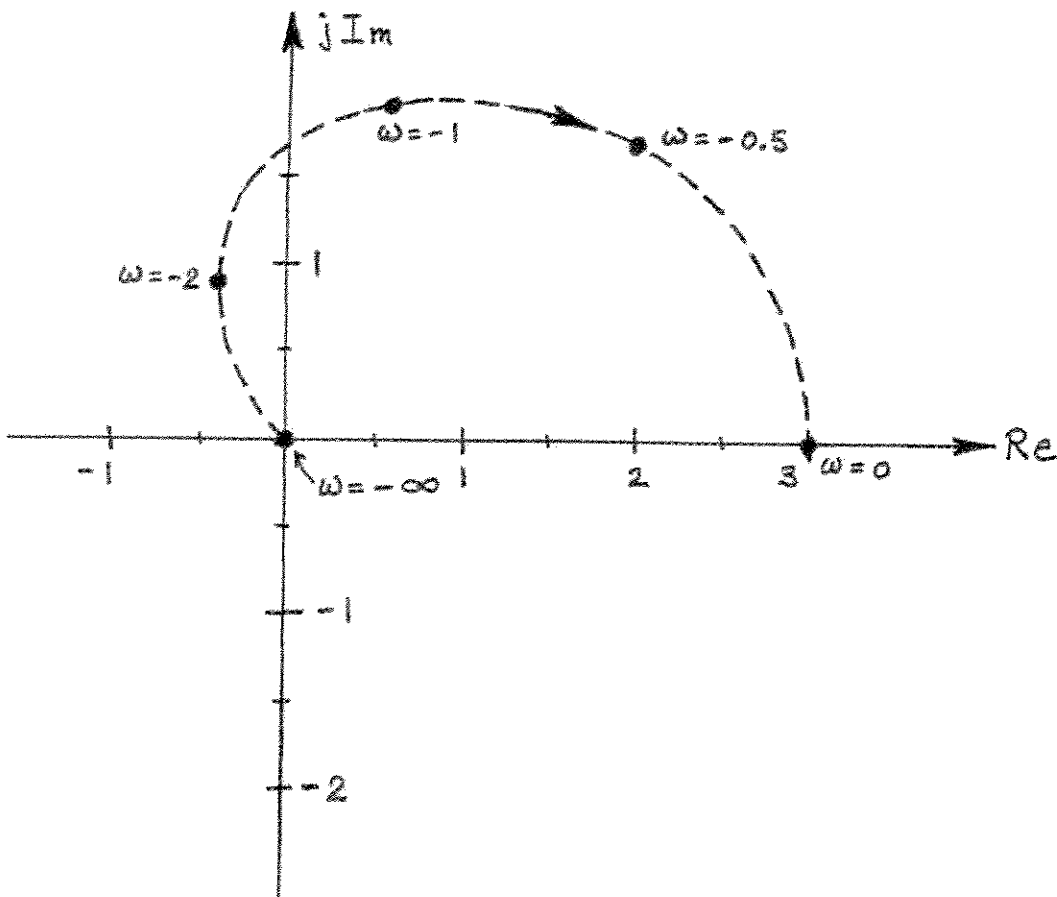


**Problem #2** (  $a = 3$ ,  $b = 2\frac{1}{2} + 2\frac{1}{2}$ ,  $c = 2 \rightarrow \rightarrow \rightarrow 10$  marks )

The open-loop transfer function of a system is given by:

$$GH(s) = \frac{6}{(s+1)(s+2)}$$

- The figure below gives a partial sketch of the Nyquist plot for the system, from  $\omega = 0$  to  $\omega = -\infty$ . Complete the drawing for the sketch of the Nyquist plot. Explain your procedure.
- From the Nyquist plot, estimate the gain margin and the phase margin. Show your procedures clearly.
- Is the closed-loop system stable or unstable? Explain your answer clearly.



**Problem #3** ( Part A:  $a = 3, b = 2 \rightarrow \rightarrow \rightarrow 5$  marks )  
( Part B:  $a = 10, b = 3\frac{1}{2} + 3\frac{1}{2}, c = 3 \rightarrow \rightarrow \rightarrow 20$  marks )

(A) A feedback control system has the following characteristic equation:

$$p(s) = s^4 + 3s^3 + s^2 + 3s + 2$$

- Using the Routh-Hurwitz criterion, determine the stability of the system.
- Is the system stable or unstable? Explain your answer.

(B) The open-loop transfer function for a unity feedback system is:

$$G(s) = \frac{K(s+1)}{s(s-3)}$$

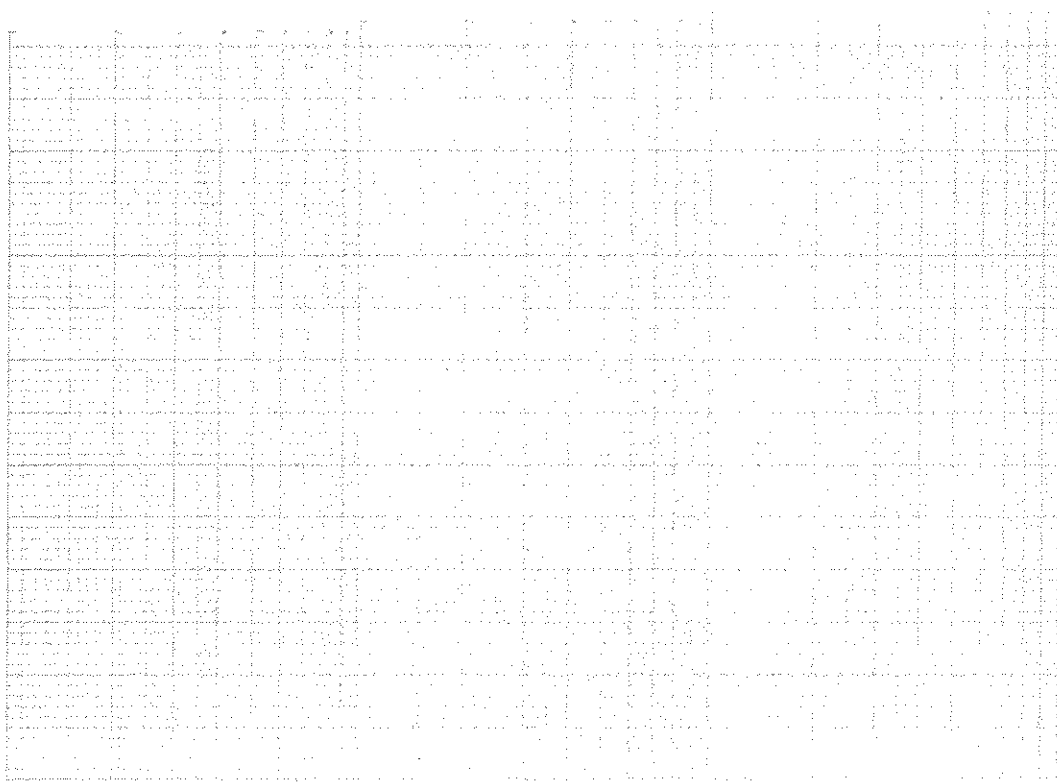
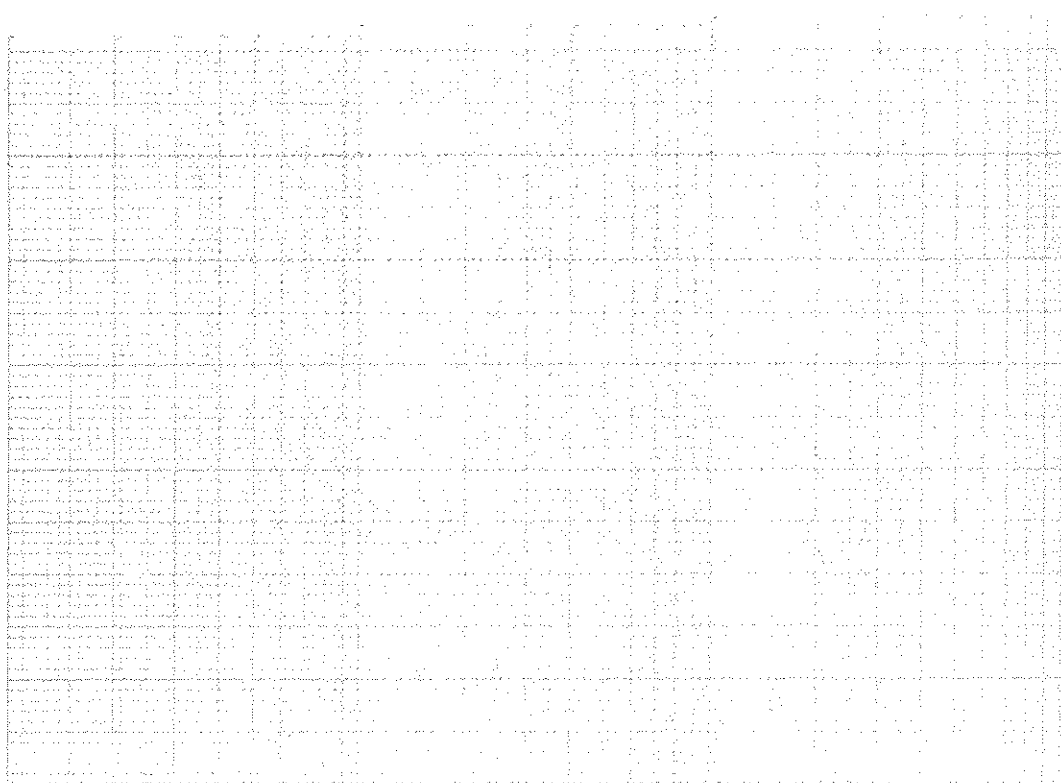
- Draw the root-locus for the closed-loop system, showing all relevant steps and details.
- Show that the closed-loop poles  $s = -2 \pm j\sqrt{3}$  lie on the locus.  
Determine the gain  $K$  at these poles.
- Derive the sensitivity equation of  $G(s)$  with respect to the gain  $K$ . ie: derive  $S_K^G$ .

**Problem #4** ( $a = 10, b_1 = 2+2, b_2 = 2, c_1 = 3, c_2 = 1 \rightarrow \rightarrow \rightarrow 20$  marks )

A unity feedback system has a plant transfer function given by:

$$G_p = \frac{3200}{s(s+4)(s+8)}$$

- On the semi-log paper provided, plot the asymptotic Bode diagram. Show all relevant steps. Indicate the relevant slopes on the diagram.
- (1) From the asymptotic Bode diagram, determine the gain margin and the phase margin. Show these values on the diagram clearly.  
(2) Is the closed loop system stable or unstable? Explain your answer clearly.
- Introduce a constant gain  $K$  controller (ie: proportional controller) to obtain a phase margin of 45 degrees.
  - What is the numerical value of this constant gain  $K$  controller?
  - Draw the block diagram for the complete closed-loop system including the controller.



**Problem #5** ( a = 5, b = 10, c = 2, d = 8 →→→ 25 marks )

A unity negative feedback control system has the plant transfer function given by:

$$G_p = \frac{10}{s(s+1)}$$

Given information:

$$\text{percent overshoot } P.O. = 100e^{-\zeta\pi/\sqrt{1-\zeta^2}}$$

$$\text{time to peak } T_p = \frac{\pi}{\omega_d} = \frac{\pi}{\omega_n\sqrt{1-\zeta^2}}$$

where  $\omega_n$ ,  $\omega_d$  and  $\zeta$  is the system natural frequency, system damped natural frequency, and system damping ratio, respectively.

- Using the root locus method, design a proportional controller so that the system transient response due to a step input  $r(t)$  has exactly 4.3 % overshoot.
- Using the root locus method, design a PD controller so that the system transient response due to a step input  $r(t)$  has exactly 4.3 % overshoot and time to peak  $T_p = 1.047\text{sec}$ .
- Discuss which system designed, either (a) or (b), has better performance due to a step input.
- For the two systems found in parts (a) and (b), determine the steady-state error due to a unit step input and due to a unit ramp input.