

Lecture

March 19, 2014

11.8 Turbine and Pump Efficiency

Turbine: $\left[\eta_T = \frac{\text{shaft output power}}{\text{ideal power}} = \frac{P_{out}}{P_i} \right]$

P_{out} : real power output of a turbine shaft

P_i : ideal power if there were no losses

PUMP: $\left[\eta_p = \frac{\text{ideal power}}{\text{shaft input power}} = \frac{P_i}{P_{in}} \right]$

P_i : ideally, only this much power would be required if there were no losses in:

- the pump
- surrounding pump system

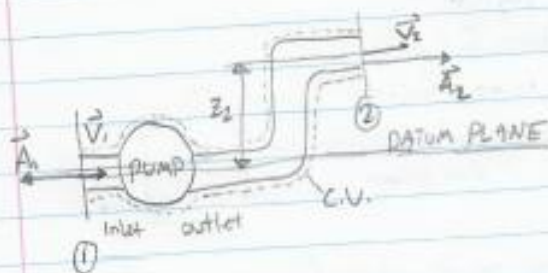
P_{in} : real power input to the pump shaft (must be larger than P_i b/c of losses)

Note: efficiency (η_T or η_p) is always less than 1.0 or 100%

Example: A pump delivers $0.3 \frac{m^3}{s}$ of water. The suction (PUMP) (inlet) pipe has a diameter of 0.25 m and the static pressure at the inlet is -25 kPa(g). The discharge (outlet) pipe has a diameter of 0.2 m and a pressure of 700 kPa(g). It is located 10 m above the suction pipe.

- what is the ideal pumping power, P_i ?
- what is the efficiency of the pump if 310 kW of power is required to drive it?

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Given: $Q = 0.3 \text{ m}^3/\text{s}$

$d_1 = 0.25 \text{ m}$

$d_2 = 0.2 \text{ m}$

$P_1 = -25 \text{ kPa(g)} = -25 \cdot 10^3 \text{ Pa(g)}$

$P_2 = 700 \text{ kPa(g)} = 700 \cdot 10^3 \text{ Pa(g)}$

$z_2 = 10 \text{ m}$

$z_1 = 0 \text{ m}$

Find: $P_p = ?$

$z_p = ?$ for $P_{in} = 310 \text{ kW}$

Solution:

a. $P_p = ?$

First, calculate V_1 & V_2 :

$$V_1 = \frac{Q}{A_1} = \frac{0.3}{\frac{\pi d_1^2}{4}} = \frac{0.3}{\frac{\pi (0.25)^2}{4}} = 6.11 \text{ m/s}$$

$$V_2 = \frac{Q}{A_2} = \frac{0.3}{\frac{\pi d_2^2}{4}} = \frac{0.3}{\frac{\pi (0.2)^2}{4}} = 9.55 \text{ m/s}$$

Now apply SFEE betw ① & ②

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + z_2 + \frac{W_p}{\dot{m}g} + H_L$$

$$\rho_1 = \rho_2 = \rho \text{ (assume incompressible)}$$

For P_i , \dot{w} no losses, $H_L = 0$

$$P_i = \dot{w}_s = \frac{1}{g} \left(\frac{P_1 - P_2}{\rho} + \frac{V_1^2 - V_2^2}{2} + 0 - z_2 g \right) \cdot g \dot{m}$$

$$\dot{w}_s = \frac{\dot{m}}{\rho} \left(\frac{P_1 - P_2}{\rho} - \frac{V_1^2 - V_2^2}{2} - z_2 g \right)$$

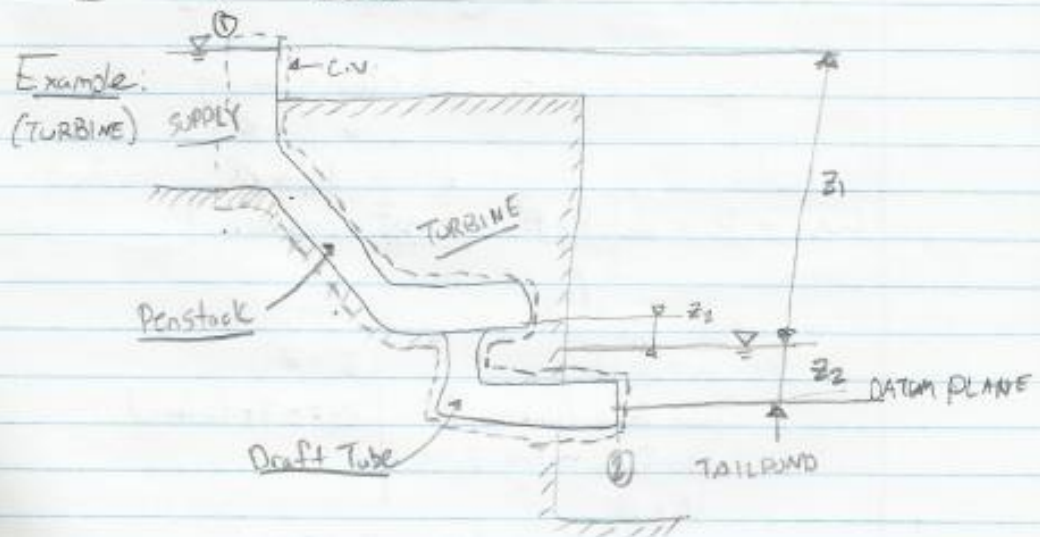
$$\dot{w}_s = 1000 \cdot 0.3 \left(\frac{-25 \cdot 10^3 - 700 \cdot 10^3}{10^3} + \frac{6.11^2 - 9.55^2}{2} - 10 \cdot 9.81 \right) =$$

$$P_i = \dot{w}_s = -255,010 \text{ W} = -255 \text{ kW}$$

Note: \ominus sign means that this is indeed a pump and not a turbine

b, $\eta_p = ?$ for $P_{in} = 310 \text{ kW}$

$$\eta_p = \frac{P_i}{P_w} = \frac{255 \text{ kW}}{310 \text{ kW}} = 0.823 \approx 82.3\%$$



210 m³/s of water pass through a hydroelectric turbine whose efficiency is 95%. The water level in the supply is $z_1 = 100\text{m}$ above the tailwater pond. The draft tube inlet and exit areas are $47\text{m}^2 (=A_1)$ and $94\text{m}^2 (=A_2)$.

a) neglect losses in the penstock, what shaft power is delivered by the turbine?

b) what shaft power is delivered by the turbine if head loss in the penstock is $H_L = 2.5\text{m}$?

c) for the conditions of a) what is the static pressure at the turbine exit/draft tube inlet plane, if this lies 2m above the tailpond level?

a) SFEE btwn ① & ②

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + z_2 + \frac{W_s}{\rho g} + H_L \quad | \quad = (g \cdot m)$$

and assuming

$$\rho_1 = \rho_2 = \rho$$

$H_L = 0$ in penstock

$$W_s = P_i = \dot{m} \left[\frac{P_1 - P_2}{\rho} + \frac{V_1^2 - V_2^2}{2} + (z_1 - z_2)g \right]$$

$$\dot{m} = \rho \cdot Q$$

$P_1 = P_{atm}$ (unknown)

$$P_2 = P_{atm} - \rho g z_2$$

$$V_1 = 0$$

$$V_2 = \frac{Q}{A_2} = \frac{210}{94} = 2.23 \text{ m/s}$$

$$z_1 = 0$$

$$z_2 = -z_2 \text{ (unknown)}$$

$$W_s = P_i = 1,000 \cdot 210 \left[\frac{P_{atm} - P_{atm} - \rho \cdot g \cdot z_2}{f} + \frac{0.25^2}{2} + g \cdot (100 - z_1) \right]$$

$$= \dots 205.9 \cdot 10^9 = 206 \text{ MW}$$

This is the ideal power, the real power will be less by

$$\eta_T = \frac{P_{out}}{P_i} \Rightarrow P_{out} = \eta_T \cdot P_i = 0.95 \cdot 206 = 195.7 \text{ MW}$$

b) Same as a) but w $h_L = 2.5 \text{ m}$

$$P_i = P_{h_L} - h_L \rho g = \dots = 200.8 \text{ MW}$$

c. Bernoulli btwn ① and ②: $P_{real} = 0.95 \cdot 200.8 = 190.8 \text{ MW}$

$$P_{(g)} = -27.12 \text{ KR (g)}$$