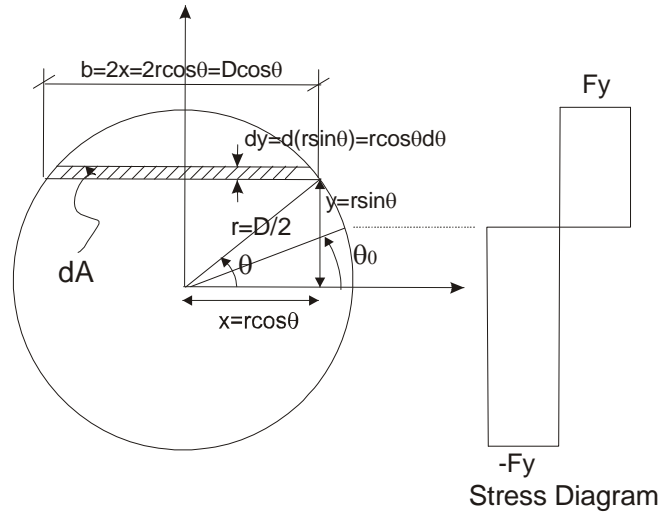


**CVG 4143-STRUCTURAL STEEL II**  
**ASSIGNMENT 2-Beam Columns**

**Plastic Interaction Relations for a solid circular section of diameter D**



$$\text{Element of Area } dA = bdy = (D \cos \theta) d \left( \frac{D}{2} \sin \theta \right) = \left( \frac{D^2}{2} \cos^2 \theta \right) d\theta$$

The element of area  $dA$  has to sweep the whole cross-section. This is accomplished by varying  $\theta$  from  $-\pi/2$  to  $+\pi/2$

Stress distribution

$$\sigma = -F_y \quad -\pi/2 \leq \theta \leq \theta_0$$

$$+F_y \quad \theta_0 \leq \theta \leq +\pi/2$$

The tensile axial force is the summation (or integration) of the longitudinal stresses over the cross-section.

$$P = \int_A \sigma dA = \int_{\theta=-\pi/2}^{\theta=\pi/2} \sigma \left( \frac{D^2}{2} \cos^2 \theta \right) d\theta = - \int_{\theta=-\pi/2}^{\theta=\theta_0} F_y \frac{D^2}{2} (\cos^2 \theta) d\theta + \int_{\theta=\theta_0}^{\theta=\pi/2} F_y \frac{D^2}{2} (\cos^2 \theta) d\theta \quad (1)$$

Note:

$$\int \cos^2 \theta d\theta = \int \frac{1}{2} (1 + \cos 2\theta) d\theta = \frac{\theta}{2} + \frac{\sin 2\theta}{4} + C \quad (2)$$

From Eq. 2, by substituting into Eq. 1., we get

$$P = -F_y \frac{D^2}{2} \left[ \theta_0 + \frac{\sin 2\theta_0}{2} \right] = -F_y \frac{D^2}{2} [\theta_0 + \sin \theta_0 \cos \theta_0] \quad (3)$$

The bending moment is the summation of the moments due to the longitudinal stresses over the cross-section.

$$M = \int_A \sigma y dA = \int_{\theta=-\frac{\pi}{2}}^{\theta=\frac{\pi}{2}} \sigma \left( \frac{D^2}{2} \cos^2 \theta \right) \underbrace{\left( \frac{D}{2} \sin \theta \right)}_{\text{moment arm}} d\theta \quad (4)$$

$$= - \int_{\theta=-\frac{\pi}{2}}^{\theta=\theta_0} F_y \left( \frac{D^2}{2} \cos^2 \theta \right) \left( \frac{D}{2} \sin \theta \right) d\theta + \int_{\theta=\theta_0}^{\theta=\frac{\pi}{2}} F_y \left( \frac{D^2}{2} \cos^2 \theta \right) \left( \frac{D}{2} \sin \theta \right) d\theta$$

We note since the stress  $\sigma$  has a stepwise definition, the integral in Eq. has to be split into two integrals.

Note:

$$\int \cos^2 \theta \sin \theta d\theta = -\frac{\cos^3 \theta}{3} + C \quad (5)$$

From Eq. 5, by substituting into Eq. 4., we get

$$M = \frac{1}{6} F_y D^3 \cos^3 \theta_0 \quad (6)$$

From Eq. 6,

$$\begin{aligned} \cos \theta_0 &= \left( \frac{6M}{F_y D^3} \right)^{1/3}, \quad \theta_0 = \cos^{-1} \left( \frac{6M}{F_y D^3} \right)^{1/3}, \\ \sin \theta_0 &= \sqrt{1 - \cos^2 \theta_0} = \sqrt{1 - \left( \frac{6M}{F_y D^3} \right)^{2/3}} \end{aligned} \quad (7)$$

From Eqs. (7), substitute into Eq. 3 to obtain the interaction equation:

$$P = \frac{F_y D^2}{2} \left[ \cos^{-1} \left( \frac{6M}{F_y D^3} \right)^{1/3} + \left( \frac{6M}{F_y D^3} \right)^{1/3} \sqrt{1 - \left( \frac{6M}{F_y D^3} \right)^{2/3}} \right] \quad (8)$$

Limiting Cases:

1. When  $\theta_0 = \pm \frac{\pi}{2}$ , the stress distribution corresponds to the case of pure axial force.

Equations 3 and 6 yield the expressions  $P = \pm \frac{\pi D^2}{2} F_y = \pm A F_y = \pm P_y$  (maximum axial yield resistance), and  $M = 0$  (zero bending resistance since the section is fully utilized in providing the maximum axial resistance).

2. When  $\theta_0 = 0$ ,  $M = \frac{D^3}{6} F_y = \underbrace{Z}_{\text{plastic modulus}} F_y = M_p$  (maximum bending resistance) and  $P = 0$  (no axial resistance since the section is fully utilized in providing the bending resistance)

Normalization:

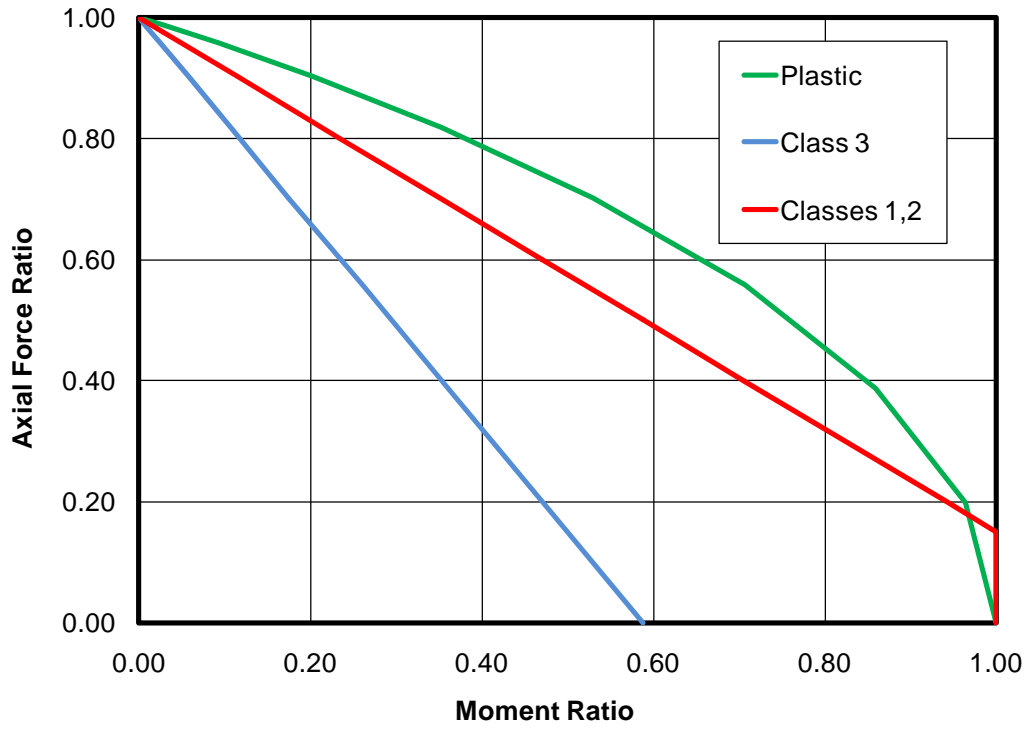
Divide both sides of Eq. 8 by  $P_y$ , we obtain

$$\frac{P}{P_y} = \frac{F_y D^2}{2 P_y} \left[ \cos^{-1} \left( \frac{6M}{F_y D^3} \right)^{1/3} + \left( \frac{6M}{F_y D^3} \right)^{1/3} \sqrt{1 - \left( \frac{6M}{F_y D^3} \right)^{2/3}} \right] \quad (9)$$

By using the expressions  $P_y = A F_y$  and  $M_p = \frac{D^3}{6} F_y$  derived under limiting cases, we obtain the following non-dimensional form of the interaction equation.

$$\frac{P}{P_y} = \pm \frac{2}{\pi} \left[ \cos^{-1} \left( \frac{M}{M_p} \right)^{1/3} + \left( \frac{M}{M_p} \right)^{1/3} \sqrt{1 - \left( \frac{M}{M_p} \right)^{2/3}} \right] \quad (10)$$

The above equation can be plotted by assuming ratios  $M / M_p$  and determining the corresponding  $P / P_y$



Plastic Interaction Relation for Solid Circular Section